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DEPARTEMENT D'ETUDES ET DE RECHERCHES EN
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(RT-OA-63/1685) REPORT ON TESTS OF A CAST
10 AIRFOIL WITH FIXED TRANSITION IN THE T2
TRANSONIC CRYOGENIC WIND TUNNEL WITH
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R.T. OA n° 63/1685 AND (DERAT n° 6/5019 DN) - Août 1985

Rapport d'essais du profil CAST 10 en transition déclenchée,
effectués dans la soufflerie transsonique cryogénique T2 en
présence de parois auto-adaptables.

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Le Chef du DERAT

Le Chef de Groupe
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RESUME D'AUTEUR : Ces essais sont la suite de ceux effectués en transition naturelle et présentés dans le rapport précédent, R.T. OA n° 59/1685 AND (DERAT n° 4/5019 DN) - Mars 1985.				
Un complément a tout d'abord été effectué, pour préciser la position de la transition sur l'extrados du profil, par une exploration longitudinale dans la couche limite (critère de Jones).				
Puis, dans un premier temps, la transition n'a été déclenchée qu'à l'intrados du profil par une bande de carborundum de hauteur 0,045 mm placée à $x/c = 5\%$ (noté T. 1/2 D.), afin de mieux séparer les phénomènes liés à l'intrados et ceux liés à l'extrados en transition naturelle (T.N.).				
Dans une deuxième phase, la transition a été déclenchée normalement sur les deux faces du profil (T.D.), également à $x/c = 5\%$ et $h = 0,045$ mm. Les configurations des essais de la campagne précédente ont été reprises, et les résultats des trois cas (T.N.) (T. 1/2 D.) et (T.D.) sont comparés ; particulièrement en ce qui concerne l'effet du nombre de Reynolds sur les coefficients aérodynamiques du profil.				
On observe le regroupement des valeurs expérimentales vers 20 millions de Reynolds, obtenu par des évolutions différentes suivant les cas considérés.				
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ABSTRACT

This technical report describes the tests on the CAST 10 airfoil in tripped-transition, carried out in the cryogenic and transonic wind-tunnel T2 fitted with self-adaptive walls.

These tests follow those which were performed in natural transition and were presented in a previous note : R.T. OA n° 59/1685 AND (DERAT n° 4/5019 DN) ONERA /CERT - March 1985.

Firstly, a complement was realized to precise the location of the natural transition on the upper surface of the airfoil ; this was done by a longitudinal exploration in the boundary layer (JONES criterion).

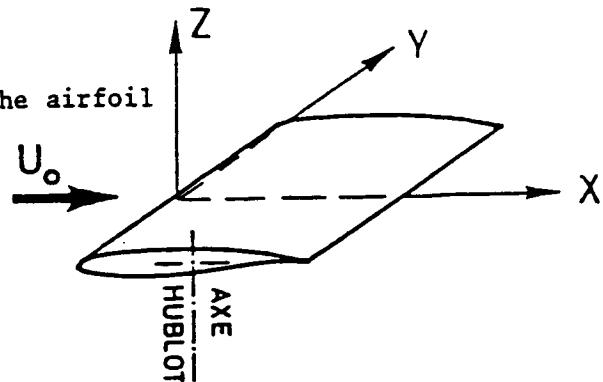
Secondly, in a first stage, the transition was only tripped on the lower surface with a carborundum strip of 0.045 mm height, situated at 5 % of chord (noted T. 1/2 D.). These tests were performed here to separate the phenomena in relation to the lower surface and those in relation to the upper surface which occur in natural transition (T.N.).

In a second stage, the transition was normally tripped on both sides of the profile (T.D.), likewise at $x/c = 5\%$ and $h = 0.045$ mm. The test configurations of the previous serial were experimented again and results obtained in the three cases (T.N.), (T. 1/2 D.) and (T.D.) were compared, in particular those concern with the effect of the Reynolds number on aerodynamic coefficients of the airfoil.

We observe the gathering of the experimental values around 20 millions Reynolds number ; but before this number, the evolutions of the curves in the three cases tested are different.

LIST OF SYMBOLS

c	chord of the airfoil
α	angle of attack
XPH	abscissa of the pressure holes in the top wall
XPB	abscissa of the pressure holes in the bottom wall
XV	abscissa of the jacks
X	
Y	
Z	
NB	iteration number of the test



PRESSESURES

p_{SL}	local static pressure
$p_{ref} = p_S$	upstream static pressure as reference
p_{SS}	static pressure in the wake
DPS =	$p_{SS} - p_{ref}$ (loss in static pressure in the wake)
DPS/PS	relative value of the static pressure in the wake
p_i, p_T	total pressure in the settling chamber
p_{iS}	total pressure in the wake
DPI =	$p_{iS} - p_i$ (loss in total pressure in the wake)
DPI/PI	relative value of the total pressure in the wake (%)
K_p	pressure coefficient

MACH

M_∞	infinite upstream Mach number
M_L	local Mach number of the airfoil calculated from p_{SL}/p_i

TEMPERATURES

TPR	temperature of the airfoil
TPG	temperature in the settling chamber
T_i, T_T	total temperature of the test
T_{iS}	total temperature in the wake
DTI =	$T_{iS} - T_i$ (variation of the total temperature in the wake)
DTI/TI	relative value of the total temperature in the wake
T_W	wall temperature
T_f	skin friction temperature $T_f/T_i = (1 + 0.2 r M^2)/(1 + 0.2 M^2)$

AERODYNAMIC COEFFICIENTS

C_z lift coefficient
C_{xp} pressure drag coefficient
C_{xs} drag coefficient (measured in the wake)
C_m pitching moment coefficient (calculated at 25 % of chord)
R_c Reynolds number of the airfoil chord

Subscripts

p wall
s wake

1 - INTRODUCTION

This study is a part of a collaboration between the ONERA (FRANCE), the DFVLR (GERMANY) and the NASA (USA). The tests will be carried out on the same model of a supercritical airfoil CAST 10 having a chord of 180 mm ; it was designed by DORNIER (GERMANY).

Two series of tests have been made in the cryogenic wind tunnel T2 fitted with self-adaptive walls (ONERA/CERT). The first series concerns only tests in natural transition (T.N.) where particular care has been taken to avoid false tripping ; the results are reported in a previous note /14/.

This technical report is related to the second series of tests where the transition was, at first, tripped only on the lower surface of the airfoil (T.1/2 D.) and, in a second stage, tripped normally on both sides of the profile (T.D.). We used a carborundum strip of 0.045 mm height, situated at 5 % of chord in each case.

The first phase (T.1/2 D.) was accomplished to separate the phenomena which occur, in natural transition, on the lower surface or on the upper surface of the airfoil : displacement of the transition location, changes of the shock position, modifications around the stagnation point, sudden tripping of the transition produced by the overspeed spike near the leading edge, etc. Some controls were executed in the T.1/2 D. case to verify the transition location on the upper surface which depends on the configuration (Mach number, angle of attack), on the Reynolds number of the test and on the wall temperature. The results are well fitted with those in natural transition (T.N.).

The second phase (T.D.) describes the normal operation of the airfoil. These tests are easier to perform than the previous ones ; problems involved by the surface state disappear.

The test procedure is exactly the same as in the first series ; all details will be found in the previous note /14/. The wind tunnel T2 and its model conditioning, the profile equipment, the test apparatus (probing system, visualizations), the adaptive walls and their use, the run process, the data acquisition and analysis will not be described again.

Here, the configurations tested are the same to be compared in the three cases (T.N.), (T.1/2 D.), (T.D.). The Mach number distributions along the profile and wakes are drawn systematically as function of α , M_0 and R_c . Likewise, the aerodynamic coefficients are plotted versus α , M_0 or R_c . Comparisons of the various evolutions are made ; we observe in particular the gathering of the curves around 20 millions Reynolds number ; however, the effect of the Reynolds is not the same in natural transition (T.N.) or in tripped transition (T.D.). At lower Reynolds number, the evolutions of the curves are greatly different and the aerodynamic efficiency is not on the same order.

The explanations of the curve evolutions and comparisons with boundary layer computations will be given in a third report /15/.

2 - GENERAL PRESENTATION OF THE TESTS

This series of tests is subdivided in three groups :

- a complement in natural transition (T.N.),
- the transition tripping on the lower surface (T.1/2 D.),
- the transition tripped on each side of the airfoil (T.D.).

In each category, the tests are classified in tables (Fig. 2, 4, 5) where the angle of attack, the Mach number and the Reynolds number are apparent. Furthermore, all the tests are listed in the order of their run number in tables (Fig. 1, 3, 6, 7) which recapitulate the results and the general conditions of the runs. Some of them do not have the C_D or the C_L values as they were judged invalid.

The complement in natural transition precise the location of the transition by a longitudinal exploration of a pitot tube inside the boundary layer (JONES's criterion). This was done at low Reynolds number ($R_c = 4 \cdot 10^6$) and unique Mach number ($M_o = 0.73$) for angles of attack from $- 1^\circ$ to $+ 0.25^\circ$ (Fig. 1).

In "half-tripping transition" (T.1/2 D.), four Mach numbers (0.7, 0.73, 0.765, 0.783) and angles of attack going from $- 2^\circ$ to $+ 2^\circ$ were tested at low Reynolds number ($R_c = 4 \cdot 10^6$) (Table : Fig. 2). The Reynolds effect was experimented in two cases and a wall temperature effect was tested in the same conditions as presented in natural transition /14/.

The tests carried out in tripped transition (T.D.) are presented on tables (Fig. 4 and 5), in the same way. The effect of the Reynolds number has been studied for six configurations and compared with the curves obtained in natural transition. Furthermore, the drag divergence was observed for two Reynolds numbers : $4 \cdot 10^6$ and $25 \cdot 10^6$, at $+ 0.25^\circ$ angle of attack.

It can be noticed from the tables that there is considerable cross-checking between the various tests at different Mach numbers, angles of attack, Reynolds numbers. In some cases, the run has been repeated several times to check the repeatability of the tests ; the precision of the results can be seen on the aerodynamic coefficients presented in the lists (Fig. 3, 6, 7).

We give in appendix listings of main tests ; each sheet corresponds to the last iteration of the runs presented. The values of the Mach numbers on the test section walls, on the airfoil, as well as the temperatures of the model can be found there. They are classified in the order of their run number.

3 - COMPLEMENT OF THE PREVIOUS TEST IN NATURAL TRANSITION :

Transition detection by a JONES's criterion

The longitudinal exploration of the boundary layer is performed with the system described on the figure 8. The pitot tube and the pressure transducer are mounted on the sting normally used at T2 /14/ ; the longitudinal moving is controlled by a step-motor. The probe has a backward movement of 66.5 mm ; the displacement is tangential to the upper surface and the setting out abscissa can be chosen.

The first control consists of observing the influence of the probe on the Mach distribution along the profile (Fig. 9). Then, the five configurations tested are presented on figures 10 to 14, where the transition location detected by oil visualization is also indicated.

We can correlate the Mach number evolution recorded at iso-height inside the boundary layer to the "bump" seen on the Mach distribution along the profile /14/ and to the oil visualization. The transition location has been plotted figure 15 ; the JONES criterion indicates the beginning and the end of the transition area, which gives a useful information.

4 - TRANSITION TRIPPED ONLY ON THE LOWER SURFACE (T.1/2 D.)

4.1. Control of the Reynolds number effect and wall temperature effect on the transition location detected on the upper surface

The run 232 corresponds to a thermal effect produced by a cold model exposed to a room temperature flow. We can verify on figure 16 that the transition location on the upper side is situated at the same place as in natural transition /14/ ; of course, this result was expected, but we find again the same lift coefficient, which shows the main contribution of the upper surface in these cases.

We have also controlled the transition location as function of Reynolds number, figure 16 ; here, the results fit well with the natural transition curve.

4.2. Mach number distributions on the airfoil and wakes

The Mach number distributions along the profile and the wakes are drawn, at the smallest Reynolds number ($R_c = 4,10^6$), for various upstream Mach numbers M_0 (fig. 17 to 28) ; each illustration corresponds to an angle of attack going from -2° to $+2^\circ$.

Conversely, they are drawn on figures 29 to 36 in relation to the angle of attack for each Mach number tested.

The third series of illustrations shows the influence of Reynolds number in the two configurations experimented here ($M_0 = 0.73$, $\alpha = -0.25^\circ$), ($M_0 = 0.76$, $\alpha = +0.25^\circ$) (figures 37 to 40).

4.3. Aerodynamic coefficients

The lift (C_L), drag (C_D) and pitching moment (C_M) coefficients are pointed in figures 41 to 43 versus Mach number for the lowest Reynolds number.

The values of these coefficients determined from the preceding curves for 4 Mach numbers (0.7, 0.73, 0.765, 0.785) have been reported in relation to the angle of attack on the figures 44 to 46.

At last, the polar C_L (C_D) was traced for three Mach numbers (fig. 47).

These curves must be compared to those obtained in natural transition /14/ ; they are more regular and the drag coefficient higher for positive angles of attack. Comparisons will be made later for 0.765 Mach number.

5 - TRANSITION TRIPPED ON THE UPPER AND LOWER SURFACE

In the T.D. case, the transition was tripped on both sides of the airfoil with a carborundum strip of 0.045 mm height, situated at $x/c = 5\%$. The test configurations have been seen previously on tables 4 and 5.

5.1. Mach number distributions on the airfoil and wakes

The curves are presented here in the same way as before ; the first series of illustrations concerns the smallest Reynolds number ($R_c = 4 \cdot 10^6$) for various upstream Mach numbers (figures 48 to 63) ; each plate is at a given angle of attack.

The Mach distributions and wakes are drawn too, for a given Mach number (0.7, 0.73 and 0.765), as function of the angle of attack going from -2° to $+4^\circ$ (figures 64 to 71).

The third series (figures 72 to 83) shows the influence of Reynolds number in the six configurations tested here ; they are a selection of cases experimented in natural transition /14/. We observe the backward displacement of the shock as the Reynolds increases, just the opposite of what we have observed in the previous series of tests (T.N.) /14/.

5.2. Aerodynamic coefficients

The aerodynamic coefficients (C_L , C_D and C_M) calculated at low Reynolds number ($R_c = 4 \cdot 10^6$) are pointed, in figures 87 to 89, in terms of angle of attack. The polar C_L (C_D) has been drawn too (figure 90).

Considerable modifications were produced by the transition tripping /14/. The total drags are higher, the lifts and pitching moments lower ; the curves are much more regular.

The drag divergence was determined for $+0.25^\circ$ and two Reynolds numbers : $R_c = 4 \cdot 10^6$ and $26 \cdot 10^6$ (figures 91 and 92). The curves obtained in T.D. case are completely different from those obtained in T.N. for the same run parameters.

The comparisons and explanations will be given in the third report /15/.

6 - EFFECT OF THE REYNOLDS NUMBER

The curves will be presented here comparatively for the three basis cases : T.N., T.1/2 D. and T.D..

6.1. Mach number distributions on the airfoil and wakes

When the laminar bubble exists on the lower surface in natural transition ($R_c < 10 \cdot 10^6$), it does not exist in the two other cases ; but the greatest differences are on the upper surface for the transition tripped on both sides (T.D.) (figures 93 to 98). The shape of the wakes is also affected.

At higher Reynolds numbers (figures 99 to 101), the differences are smaller ; this indicates the forward moving of the natural transition.

6.2. Aerodynamic coefficients

Comparison is made on figures 102 to 104 for the upstream infinite Mach number $M_\infty = 0.765$. The lift and drag coefficients are plotted versus angle of attack for the smallest Reynolds number (figures 102, 103), where the differences in natural and tripped transition are obvious. The polar for the $21 \cdot 10^6$ Reynolds number is drawn too (figure 104) ; in this case, we obtain the same curve ; details will be found in the following series of illustrations.

The aerodynamic coefficients (C_D , C_L and C_M) are traced in relation to the Reynolds number for the six configurations tested in tripped transition (T.D.) (figures 105 to 122). The next table recapitulates the configurations experimented :

α M_∞	- 2°	- 1°	- 0.25°	+ 0.25°	+ 1°	+ 2°
0.7					0 ■	
0.73		0	0 ▲ ■			
0.76				0 ▲ ■	0 ■	
0.765	0 ■			0.		0 ■

0 T.N. ▲ T.1/2 D. ■ T.D.

At low Reynolds numbers, the total drags in T.D. are higher, the lifts and pitching moments are lower. The values obtained in T.1/2 D. are situated either between the two other groups (T.N. and T.D.) or near the natural transition case. Explanations must be seen on the Mach number distributions along the profile ; it depends on the transition location on the lower surface /15/.

At higher Reynolds numbers (between 10 and 20 millions according to the configuration examined), we observe the gathering of the three curves (T.N., T.1/2 D. and T.D.). This indicates again the forward moving of the natural transition with the increase in Reynolds number ; in addition, the height of the carborundum strip is well adapted to the boundary layer thickness ; it produces no overthickening.

Lastly, the curves corresponding to the tripped transition are smoother.

7 - CONCLUSION

This report describes the tests performed in tripped transition on the CAST 10 airfoil ; it is the continuation of the previous note about the natural transition. Remember that a considerable effort has been made to avoid false tripping ; the transition was natural until at least 8 million Reynolds. Furthermore, a number of cross-checks allowed the estimation of the transition location.

We added a testing aid for the detection of the transition by a JONES criterion which fits well with the other means ; but it gives also useful information about the beginning and the end of the boundary layer transition.

The cross-checking with the previous tests is excellent ; this gives confidence in the comparisons made here. Indisputably, the aerodynamic testing in tripped transition is much easier than for the previous one, although this CAST 10 airfoil is particularly sensitive to the flow parameters around its computation point.

The tests in "half tripped" transition (only on the lower surface) were performed to separate the phenomena which occur on the upper surface from those occurring on the lower surface. Indeed, the curve shapes of the aerodynamic coefficients which seem strange in natural transition are due to transition displacements on both sides of the profile. The Reynolds number effect is not easy to explain because some compensations can occur.

We have observed the gathering of the experimental curves around 20 millions Reynolds number for the three cases T.N., T.1/2 D. and T.D., which indicates the forward movement of the natural transition when the Reynolds number increases. In addition this proves that the height of the carborandum strip is well adapted at the boundary layer thickness ; it produces no overthickening.

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J.F. BREIL

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R.T. OA N° 59/1685 AND (DERAT N° 4/5019 DN) - Mars 1985

/15/

Analyse des résultats obtenus dans la soufflerie T2 sur le profil CAST 10.
R.T. à paraître

L I S T E D E S P L A N C H E S

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- 6 - Tableau des résultats obtenus en T.D.
- 7 - Tableau des résultats obtenus en T.D. (suite).

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- 15 - Repérage de la position de transition : comparaison critère de Jones - visualisation.

ESSAIS EN TRANSITION DECLENCHEE A L'INTRADOS (T. 1/2 D.)

- 16 - Comparaison de résultats T. N. - T. 1/2 D.

VARIATION DU MACH M_∞ à $R_c = 4 \cdot 10^6$

- | | |
|--|--------------------------|
| 17 - Distributions de Mach sur le profil | } $\alpha = - 2^\circ$ |
| 18 - Sondages des sillages | |
| 19 - Distributions de Mach sur le profil | } $\alpha = - 1^\circ$ |
| 20 - Sondages des sillages | |
| 21 - Distributions de Mach sur le profil | } $\alpha = - 0,5^\circ$ |
| 22 - Sondages des sillages | |
| 23 - Distributions de Mach sur le profil | } $\alpha = 0^\circ$ |
| 24 - Sondages des sillages | |
| 25 - Distributions de Mach sur le profil | } $\alpha = 1^\circ$ |
| 26 - Sondages des sillages | |
| 27 - Distributions de Mach sur le profil | } $\alpha = + 2^\circ$ |
| 28 - Sondages des sillages | |

VARIATION D'INCIDENCE $R_c = 4 \cdot 10^6$

- | | |
|--|----------------------|
| 29 - Distributions de Mach sur le profil | } $M_\infty = 0,7$ |
| 30 - Sondages des sillages | |
| 31 - Distributions de Mach sur le profil | } $M_\infty = 0,73$ |
| 32 - Sondages des sillages | |
| 33 - Distributions de Mach sur le profil | } $M_\infty = 0,766$ |
| 34 - Sondages des sillages | |
| 35 - Distributions de Mach sur le profil | } $M_\infty = 0,784$ |
| 36 - Sondages des sillages | |

VARIATION DU NOMBRE DE REYNOLDS

- | | |
|--|---------------------------|
| 37 - Distributions de Mach sur le profil | } $\alpha = - 0,25^\circ$ |
| 38 - Sondages des sillages | |

- 39 - Distributions de Mach sur le profil } $\alpha = 0,25^\circ$
40 - Sondages des sillages } $M = 0,76$

COEFFICIENTS AERODYNAMIQUES EN FONCTION DU NOMBRE DE MACH

- 41 - Coefficient de trainée C_{xs} }
42 - Coefficient de portance C_z } $R_C = 4 \cdot 10^6$
43 - Coefficient de moment de tangage C_m }

COEFFICIENTS AERODYNAMIQUES EN FONCTION DE L'INCIDENCE

- 44 - Coefficient de trainée C_{xs} }
45 - Coefficient de portance C_z }
46 - Coefficient de moment de tangage C_m } $R_C = 4 \cdot 10^6$
47 - Polaire C_z (C_x) }

ESSAIS EN TRANSITION DECLENCHEE T.D. - Extrados - Intrados

VARIATION DU MACH M_e à $R_C = 4 \cdot 10^6$

- 48 - Distributions de Mach sur le profil } $\alpha = - 2^\circ$
49 - Sondages des sillages }
50 - Distributions de Mach sur le profil } $\alpha = - 1^\circ$
51 - Sondages des sillages }
52 - Distributions de Mach sur le profil } $\alpha = 0^\circ$
53 - Sondages des sillages }
54 - Distributions de Mach sur le profil } $\alpha = 0,25^\circ$
55 - Sondages des sillages }
56 - Distributions de Mach sur le profil } $\alpha = 1^\circ$
57 - Sondages des sillages }

58 - Distributions de Mach sur le profil	}	$\alpha = 2^\circ$
59 - Sondages des sillages		
60 - Distributions de Mach sur le profil	}	$\alpha = 3^\circ$
61 - Sondages des sillages		
62 - Distributions de Mach sur le profil	}	$\alpha = 4^\circ$
63 - Sondages des sillages		

VARIATION D'INCIDENCE $R_C = 4 \cdot 10^6$

64 - Distributions de Mach sur le profil	}	$M_\infty = 0,7$
65 - Sondages des sillages		
66 - Sondages des sillages (suite)		
67 - Distributions de Mach sur le profil	}	$M_\infty = 0,73$
68 - Sondages des sillages		
69 - Sondages des sillages (suite)		
70 - Distributions de Mach sur le profil	}	$M_\infty = 0,765$
71 - Sondages des sillages		

VARIATION DU NOMBRE DE REYNOLDS

72 - Distributions de Mach sur le profil	}	$\alpha = 1^\circ$
73 - Sondages des sillages		
74 - Distributions de Mach sur le profil	}	$\alpha = - 0,25^\circ$
75 - Sondages des sillages		
76 - Distributions de Mach sur le profil	}	$\alpha = 0,25^\circ$
77 - Sondages des sillages		
78 - Distributions de Mach sur le profil	}	$\alpha = 1^\circ$
79 - Sondages des sillages		
80 - Distributions de Mach sur le profil	}	$\alpha = - 2^\circ$
81 - Sondages des sillages		

82 - Distributions de Mach sur le profil	}	$\alpha = 2^\circ$
83 - Sondages des sillages		$M_\infty = 0,765$

COEFFICIENTS AERODYNAMIQUES EN FONCTION DU NOMBRE DE MACH

84 - Coefficient de trainée C_{xs}	}	$R_C = 4 \cdot 10^6$
85 - Coefficient de portance C_z		
86 - Coefficient de moment de tangage C_m		

COEFFICIENTS AERODYNAMIQUES EN FONCTION DE L'INCIDENCE

87 - Coefficient de trainée C_{xs}	}	$R_C = 4 \cdot 10^6$
88 - Coefficient de portance C_z		
89 - Coefficient de moment de tangage C_m		
90 - Polaire C_z (C_x)		

COEFFICIENTS AERODYNAMIQUES POUR $\alpha = + 0,25$ ET DEUX NOMBRES DE REYNOLDS

91 - Coefficient de trainée C_{xs}
92 - Coefficient de portance C_z

EFFET DU NOMBRE DE REYNOLDS COMPARATIVEMENT T.N. - T. 1/2 D. - T.D.

COMPARAISON T.N., T. 1/2 D., T.D. SUR LE PROFIL ET DANS LE SILLAGE A MEME REYNOLDS

93 - Distributions de Mach sur le profil	}	$M_\infty = 0,73, \alpha = 0,23$
94 - Sondages des sillages		$R_C = 4 \cdot 10^6$
95 - Distributions de Mach sur le profil	}	$M_\infty = 0,76, \alpha = 0,25$
96 - Sondages des sillages		$R_C = 4 \cdot 10^6$
97 - Distributions de Mach sur le profil	}	$M_\infty = 0,76, \alpha = 0,25$
98 - Sondages des sillages		$R_C = 7,8 \cdot 10^6$

99 - Distributions de Mach sur le profil	$M_\infty = 0,76, \alpha = 0,25^\circ$
100 - Sondages des sillages	$R_C = 13 \cdot 10^6$
101 - Distributions de Mach sur le profil	$M_\infty = 0,765, \alpha = 0,25^\circ$
	$R_C = 25 \cdot 10^6$

COMPARAISON T.N., T. 1/2 D., T.D. SUR LES COEFFICIENTS AERODYNAMIQUES

- 102 - Coefficient de trainée C_{xs} ($R_C = 4 \cdot 10^6$)
103 - Coefficient de portance C_z ($R_C = 4 \cdot 10^6$)
104 - Polaire C_z (C_{xs}) ($R_C = 4 \cdot 10^6$ et $21 \cdot 10^6$)

EVOLUTION DES COEFFICIENTS AERODYNAMIQUES EN FONCTION DU REYNOLDS

105 - Coefficient de trainée C_{xs}	$M_\infty = 0,73$
106 - Coefficient de portance C_z	$\alpha = 1^\circ$
107 - Coefficient de moment de tangage C_m	
108 - Coefficient de trainée C_{xs}	$M_\infty = 0,73$
109 - Coefficient de portance C_z	$\alpha = 0,25$
110 - Coefficient de moment de tangage C_m	
111 - Coefficient de trainée C_{xs}	$M_\infty = 0,76$
112 - Coefficient de portance C_z	$\alpha = 0,25^\circ$
113 - Coefficient de moment de tangage C_m	
114 - Coefficient de trainée C_{xs}	$M_\infty = 0,76$
115 - Coefficient de portance C_z	$\alpha = 1^\circ$
116 - Coefficient de moment de tangage C_m	
117 - Coefficient de trainée C_{xs}	$M_\infty = 0,765$
118 - Coefficient de portance C_z	$\alpha = \sim 2^\circ$
119 - Coefficient de moment de tangage C_m	
120 - Coefficient de trainée C_{xs}	$M_\infty = 0,765$
121 - Coefficient de portance C_z	$\alpha = + 2^\circ$
122 - Coefficient de moment de tangage C_m	

TABLEAUX DES ESSAIS

PLANCHES 1 à 7

Complément

T.N.

ESSAI	ALPH	M0	PT (b)	TT OK	RU e+06	NB	CXP	CXS	CZ	CM
AD402	-.25	.7318	1.652	295.	3.9	4	.0043		.391	-.025
AD403	-.25	.7308	1.646	294.	3.9	3	.0055		.385	-.026
AD404	-.25	.7303	1.648	297.	3.8	2	.0051		.392	-.027
AD405	0.00	.7305	1.646	297.	3.8	3	.0049		.402	-.020
AD406	.25	.7300	1.645	297.	3.8	3	.0057		.426	-.066
AD407	.25	.7305	1.643	294.	3.9	3	.0057		.421	-.066
AD408	-1.00	.7324	1.644	296.	3.8	3	.0041		.329	-.084
AD409	-.50	.7334	1.646	294.	3.9	4	.0039		.386	-.083

Déplacement longitudinal d'un pitot
Critère de Jones

TABLEAU DES ESSAIS COMPLEMENTAIRES EN TRANISTION NATURELLE

T. 1/2 D.

PL. 2

$$R_C = 4 \cdot 10^6 \quad P_i = 1,7 \text{ bar} \quad T_i = 296 \text{ K}$$

α	Mach				
	0,7	0,73	0,76	0,765	0,783
+ 2°	216	217			
+ 1°	213	214		215 245	
+0,25°			236 243	235	
0°	206	204		205	224
-0,25°		226 233			
-0,5°	210	211			225
-1°	207 222	221	208	209	223
-2°	218	219		220	

Effet Reynolds

Conditions d' Essai			Mach = 0,73 $\alpha = -0,25^\circ$	Mach = 0,76 $\alpha = +0,25^\circ$
R_C	P_i	T_i		
$4 \cdot 10^6$	1,69	293	226 233	235 236 243
$5,9 \cdot 10^6$	2,5	296	227	
$6,8 \cdot 10^6$	2,9	297	228	239 240 241 242
$7,7 \cdot 10^6$	3,3	297	229	238
$8,9 \cdot 10^6$	2,9	240	230	
$13,8 \cdot 10^6$	1,64	119	231 234	244

Effet T_p/T_f

$$\begin{cases} R_C = 4 \cdot 10^6 \\ M_0 = 0,73 \\ \alpha = -0,25^\circ \end{cases}$$

Essai 232

ESSAI	ALPH	M0	PT (b)	TT OK	RC e+06	NB	CXP	CXS	CZ	CI	
$R_c = 4.10^6$	AD204	0.00	.7294	1.673	294.	3.9	4	.0049	.0084	.418	-.06
	AD205	0.00	.7637	1.727	294.	4.2	4	.0063	.0067	.552	-.096
	AD206	0.00	.6984	1.629	293.	3.7	4	.0043	.0081	.401	-.067
	AD207	-1.00	.7016	1.632	294.	3.7	4	.0029	.0070	.334	-.084
	AD208	-1.00	.7554	1.721	296.	4.1	5	.0044	.0065	.584	-.077
	AD209	-1.00	.7667	1.730	296.	4.1	4	.0057	.0069	.388	-.101
	AD210	-.50	.7011	1.635	296.	3.7	5	.0034	.0077	.355	-.072
	AD211	-.50	.7291	1.674	296.	3.9	4	.0040	.0076	.396	-.081
	AD213	1.00	.6832	1.622	293.	3.7	5	.0054	.0088	.511	-.059
	AD214	1.00	.7345	1.680	295.	4.0	4	.0078	.0093	.608	-.070
	AD215	1.00	.7647	1.730	295.	4.1	4	.0154	.0169	.689	-.099
	AD216	2.00	.6996	1.594	294.	3.6	5	.0101	.0112	.692	-.057
	AD217	2.00	.7324	1.679	296.	3.9	4	.0166	.0165	.798	-.078
	AD218	-2.00	.7010	1.640	295.	3.7	5	.0029	.0063	.197	-.086
	AD219	-2.00	.7321	1.682	296.	3.9	4	.0034	.0063	.212	-.093
	AD220	-2.00	.7667	1.735	297.	4.1	4	.0047	.0073	.228	-.101
	AD221	-1.00	.7320	1.678	293.	4.0	5	.0042	.0067	.361	-.091
	AD222	-1.00	.6991	1.637	294.	3.8	4	.0030	.0072	.332	-.084
	AD223	-1.00	.7821	1.748	295.	4.3	4	.0084	.0095	.389	-.106
	AD224	0.00	.7823	1.749	295.	4.2	4	.0128	.0125	.546	-.107
	AD225	-.50	.7857	1.752	296.	4.3	6	.0104	.0103	.468	-.106
$R_c = 0.25$	AD226	-.25	.7314	1.676	293.	4.0	5	.0043	.0080	.400	-.073
	AD227	-.25	.7346	2.509	296.	5.9	4	.0038	.0081	.394	-.071
	AD228	-.25	.7299	2.900	297.	6.7	4	.0035	.0079	.390	-.071
	AD229	-.25	.7299	3.301	297.	7.6	4	.0035	.0079	.388	-.071
	AD230	-.25	.7299	2.903	240.	8.9	4	.0037	.0082	.374	-.069
	AD231	-.25	.7257	1.637	119.	13.5	4	.0049		.362	-.068
	AD233	-.25	.7280	1.688	293.	4.0	4	.0044	.0078	.387	-.070
	AD234	-.25	.7309	1.627	119.	13.5	4	.0047	.0084	.371	-.069
$R_c = 0.25^*$	AD235	.25	.7634	1.723	293.	4.2	4	.0085	.0078	.591	-.097
	AD236	.25	.7607	1.718	292.	4.2	4	.0076	.0071	.578	-.092
	AD238	.25	.7600	3.292	296.	7.8	4	.0057	.0075	.539	-.081
	AD239	.25	.7598	2.899	296.	6.9	4	.0060	.0079	.571	-.088
	AD240	.25	.7627	2.902	297.	6.9	4	.0061	.0083	.593	-.093
	AD241	.25	.7655	2.900	295.	7.0	4	.0028	.0081	.623	-.103
	AD242	.25	.7598	2.895	296.	6.9	4	.0064	.0070	.599	-.094
	AD243	.25	.7620	1.698	296.	4.1	4	.0079	.0081	.613	-.100
$M_e = 0.76$	AD244	.25	.7622	1.639	119.	14.0	4	.0073	.0094	.496	-.075
	AD245	1.00	.7648	1.698	294.	4.1	4	.0166	.0172	.697	-.102

Essai avec déséquilibre thermique $T_p/T_f \approx 0,87$

ESSAI	ALPH	M0	PT (b)	TT OK	RC e+06	NB	CXP	CXS	CZ	CI
AD232	-.25	.7233	1.668	292.	3.9	4	.0039	.0073	.455	-.082

T. D.

PL. 4

$$R_C = 4 \cdot 10^6 \quad P_i = 1,7 \text{ bar} \quad T_i = 296 \text{ K}$$

α	Mach				
	0,7	0,73	0,76	0,765	> 0,77
+ 4°	266	267			
+ 3°	262	263	265	264	
+ 2°	257	258	261	259 260 319	
+ 1°	248 302	247	303	246	
+ 0,25°	326 328	325 331	291 297 334 293 321		322 323 324
0°	249	250	251		
- 0,25°		271 274 277 278 281 283 287 290 300			
- 1°	268	269		270	
- 2°	255 256	254	252 253	312	

Divergence de Trainée $\alpha = +0,25^\circ$

$R_C \backslash M_o$	0,69 ... 0,71	0,71 ... 0,73	0,73 ... 0,75	0,75 ... 0,77	0,77 ... 0,79
$4 \cdot 10^6$	328	326 331	325 334	291 297 293 321	322 323 324
$25 \cdot 10^6$		336	330	296 332	333 335

TABLEAU DES ESSAIS EN T.D. : $R_C = 4 \times 10^6$

Effet Reynolds

Conditions d'Essai			$M_o=0,765$ $\alpha = -2^\circ$	$M_o=0,73$ $\alpha = -0,25^\circ$	$M_o=0,76$ $\alpha = +0,25^\circ$	$M_o=0,7$ $\alpha = +1^\circ$	$M_o=0,76$ $\alpha = +1^\circ$	$M_o=0,765$ $\alpha = +2^\circ$
R_c	R_i	T_i						
$4 \cdot 10^6$	1,65	295	312	271 274 277 278 281 283 287 290 300	291 293 297 321	248 302	303	259 260 319
$5,9 \cdot 10^6$	2,5	296		272 280	327	307	306	316
$6,7 \cdot 10^6$	2,9	296	313	284	292	304	305	
$7,7 \cdot 10^6$	3,3	296		273	294			
$10,1 \cdot 10^6$	3,3	240		279				318
$11,5 \cdot 10^6$	2	155	314		298	308	309	317
$13,3 \cdot 10^6$	1,6	119		275 276 282	295			
$14,1 \cdot 10^6$	2,5	155		285				
$17,2 \cdot 10^6$	2,9	155			299			
$20,7 \cdot 10^6$	2,5	119	315	288 289 301		310	311	320
$25 \cdot 10^6$	2,9	119			296			
$27,1 \cdot 10^6$	3,3	119		286				

ORIGINAL PAGE IS
OF POOR QUALITY

T.D.

PL. 6

ESSAI	ALPH	M0	PT (b)	TT OK	RC e+06	NB	CXP	CXS	CZ	CM	
AD246	1.00	.7646	1.690	292.	4.1	4	.0131	.0158	.542	-.063	
AD247	1.00	.7320	1.677	293.	4.0	4	.0088	.0114	.505	-.053	
AD248	1.00	.6988	1.599	291.	3.7	4	.0069	.0105	.491	-.053	
AD249	0.00	.6997	1.597	292.	3.7	4	.0048	.0100	.348	-.056	
AD250	0.00	.7300	1.644	293.	3.9	4	.0053	.0104	.349	-.056	
AD251	0.00	.7615	1.680	294.	4.0	4	.0068	.0109	.359	-.056	
AD252	-2.00	.7613	1.680	294.	4.0	4	.0056	.0107	.063	-.062	
AD253	-2.00	.7608	1.685	296.	4.0	4	.0057	.0109	.058	-.061	
AD254	-2.00	.7318	1.647	296.	3.8	4	.0050	.0103	.072	-.061	
AD255	-2.00	.6995	1.562	296.	3.5	4	.0043	.0101	.080	-.061	
AD256	-2.00	.6928	1.592	290.	3.7	4	.0041	.0100	.080	-.060	
AD257	2.00	.7017	1.602	291.	3.7	4	.0100	.0126	.644	-.050	
AD258	2.00	.7306	1.644	293.	3.9	4	.0143	.0169	.692	-.057	
AD259	2.00	.7658	1.691	294.	4.1	4	.0260		.629	-.062	
AD260	2.00	.7656	1.685	294.	4.1	4	.0255	.0342	.636	-.063	
AD261	2.00	.7522	1.667	295.	4.0	4	.0199	.0232	.695	-.065	
AD262	3.00	.7009	1.656	292.	3.8	5	.0196	.0204	.829	-.053	
AD263	3.00	.7296	1.699	293.	4.0	4	.0276	.0300	.840	-.064	
AD264	3.00	.7665	1.741	294.	4.2	4	.0406	.0617	.631	-.051	
AD265	3.00	.7517	1.726	295.	4.1	4	.0363	.0513	.716	-.058	
AD266	4.00	.7021	1.655	296.	3.8	5	.0343	.0339	.948	-.055	
AD267	4.00	.7316	1.697	294.	4.0	4	.0456	.0593	.813	-.054	
AD268	-1.00	.6994	1.588	295.	3.6	4	.0040	.0100	.213	-.059	
AD269	-1.00	.7312	1.630	296.	3.8	4	.0045	.0103	.208	-.059	
AD270	-1.00	.7652	1.683	297.	4.0	4	.0054	.0108	.199	-.058	
<hr/>											
Variation du Reynolds $M_0 = 0.73$ $\alpha = 0.25$	AD271	-.25	.7299	1.634	296.	3.8	5	.0051	.0104	.309	-.056
	AD272	-.25	.7324	2.506	298.	5.8	5	.0045	.0094	.336	-.061
	AD273	-.25	.7271	3.294	298.	7.6	4	.0040	.0089	.350	-.064
	AD274	-.25	.7296	1.643	292.	3.9	4	.0049	.0101	.312	-.057
	AD275	-.25	.7338	1.594	118.	13.4	4	.0051	.0100	.362	-.067
	AD276	-.25	.7293	1.611	120.	13.2	4	.0045	.0097	.363	-.067
	AD277	-.25	.7358	1.638	292.	3.9	4	.0051	.0105	.309	-.056
	AD278	-.25	.7307	1.630	295.	3.8	4	.0051	.0102	.309	-.056
	AD279	-.25	.7273	3.292	240.	10.1	4	.0038	.0085	.361	-.067
	AD280	-.25	.7297	2.497	293.	5.9	4	.0041	.0094	.340	-.061
	AD281	-.25	.7289	1.621	293.	3.8	4	.0049	.0102	.314	-.057
	AD282	-.25	.7302	1.595	119.	13.2	4	.0043	.0094	.360	-.066
	AD283	-.25	.7265	1.621	292.	3.8	4	.0051	.0098	.315	-.057
	AD284	-.25	.7283	2.887	296.	6.7	4	.0042	.0088	.347	-.063
	AD285	-.25	.7329	2.484	155.	14.1	4	.0042	.0079	.381	-.071
	AD286	-.25	.7279	3.272	119.	27.1	4	.0048		.359	-.068
	AD287	-.25	.7271	1.635	292.	3.9	4	.0049	.0099	.310	-.056
	AD288	-.25	.7343	2.491	120.	20.6	4	.0039		.369	-.069
	AD289	-.25	.7313	2.484	120.	20.5	4	.0044		.368	-.068
	AD290	-.25	.7290	1.636	294.	3.8	4	.0052	.0094	.310	-.057

TABLEAU DES RESULTATS OBTENUS EN T.D.

ESSAI	R _{EF}	T ₁₀	P ₁ (h)	T ₁ OK	R _E e+Ra	N _B	C _{EF}	L _{NS}	C _Z	C _U	
$\alpha = -2^\circ$ $M_o = 0.76$ $\alpha = 0.25^\circ$ $M_o = 0.76$	AD291	.25	2610	1.678	295.	4.0	5	.0062	.0105	.349	-.055
	AD292	.25	2594	2.896	297.	6.9	4	.0063	.0095	.444	-.062
	AD293	.25	2598	1.669	292.	4.0	4	.0071	.0105	.349	-.055
	AD294	.25	2598	3.290	296.	7.8	4	.0060	.0093	.405	-.065
	AD295	.25	2594	1.645	120.	13.9	4	.0063	.0096	.466	-.068
	AD296	.25	2603	2.982	120.	25.2	4	.0061	.0094	.428	-.070
	AD297	.25	2567	1.674	292.	4.0	4	.0065	.0105	.392	-.015
	AD298	.25	2595	1.991	154.	11.5	4	.0061	.0092	.423	-.070
	AD299	.25	2589	2.983	155.	17.2	4	.0053	.0082	.491	-.024
$\alpha = -2^\circ$ $M_o = 0.76$ $\alpha = 0.25^\circ$ $M_o = 0.76$	AD300	-.25	2264	1.641	291.	3.9	4	.0052	.0096	.314	-.056
	AD301	-.25	2332	2.493	119.	20.7	4	.0040	.0081	.324	-.069
$\alpha = -2^\circ$ $M_o = 0.76$ $\alpha = 0.25^\circ$ $M_o = 0.76$	AD302	1.00	6980	1.616	294.	3.7	5	.0062	.0100	.429	-.053
	AD303	1.00	7608	1.689	295.	4.1	4	.0119	.0143	.546	-.062
	AD304	1.00	6987	2.888	297.	6.5	4	.0062	.0092	.513	-.059
	AD305	1.00	7587	2.883	297.	6.8	4	.0114	.0134	.588	-.070
	AD306	1.00	7645	2.402	295.	5.8	4	.0128	.0152	.524	-.070
	AD307	1.00	7020	2.398	296.	5.5	4	.0064	.0096	.507	-.056
	AD308	1.00	7012	1.995	154.	11.0	4	.0064	.0085	.534	-.064
	AD309	1.00	7603	2.002	155.	11.6	4	.0122	.0131	.599	-.078
	AD310	1.00	7033	2.496	120.	20.1	4	.0069	.0090	.524	-.062
	AD311	1.00	7638	2.496	119.	21.2	4	.0129	.0136	.597	-.078
$\alpha = -2^\circ$ $M_o = 0.76$	AD312	-2.00	7625	1.689	295.	4.1	5	.0056	.0104	.055	-.062
	AD313	-2.00	7645	2.878	298.	6.8	4	.0049	.0095	.081	-.068
	AD314	-2.00	7715	1.966	156.	11.3	4	.0039	.0087	.105	-.075
	AD315	-2.00	7646	2.473	120.	20.9	4	.0046	.0091	.108	-.075
$\alpha = +2^\circ$ $M_o = 0.76$	AD316	2.00	7696	2.490	295.	6.0	4	.0272	.0365	.640	-.065
	AD317	2.00	7647	1.986	155.	11.5	4	.0265		.705	-.029
	AD318	2.00	7630	1.673	155.	9.7	4	.0257	.0317	.703	-.072
	AD319	2.00	7638	1.692	294.	4.1	4	.0245	.0308	.651	-.065
	AD320	2.00	7669	2.487	120.	21.0	4	.0268	.0350	.692	-.076
$Divergence de Trainée: +0.25^\circ$ $R_c = 4.10$ et $R_c = 25.10$	AD321	.25	2619	1.779	293.	4.3	4	.0070	.0106	.404	-.056
	AD322	.25	2229	1.716	295.	4.2	4	.0079	.0112	.410	-.057
	AD323	.25	2843	1.731	296.	4.2	4	.0101	.0134	.406	-.061
	AD324	.25	2904	1.741	296.	4.2	4	.0121	.0155	.392	-.062
	AD325	.25	2416	1.662	297.	3.9	4	.0063	.0102	.388	-.054
	AD326	.25	2183	1.629	297.	3.7	4	.0057	.0100	.381	-.055
	AD327	.25	2625	2.495	298.	5.9	4	.0071	.0102	.440	-.062
	AD328	.25	7003	1.596	294.	3.7	4	.0052	.0098	.378	-.056
	AD329	.25	2495	2.991	120.	24.9	4	.0245	.0091		
	AD330	.25	2288	1.614	293.	3.8	4	.0060	.0101	.382	-.054
	AD331	.25	2661	2.984	121.	25.0	4	.0070	.0097	.485	-.072
	AD332	.25	2774	2.987	120.	25.3	4	.0086	.0113	.508	-.081
	AD333	.25	2496	1.647	294.	3.9	4	.0048	.0104	.340	-.054
	AD334	.25	2396	2.989	120.	25.7	4	.0140	.0166	.478	-.071
	AD335	.25	2291	2.982	120.	24.5	4	.0060	.0087	.450	-.067

TABLEAU DES RESULTATS OBTENUS EN T.D. (suite)

**COMPLEMENT EN
TRANSITION NATURELLE**

T.N.



PLANCHES 8 à 15



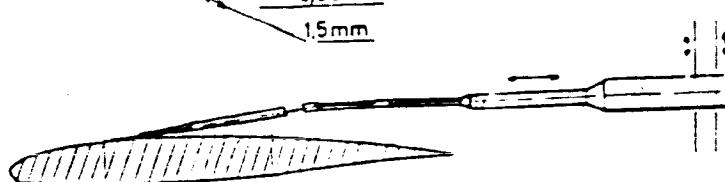
ORIGINAL PAGE IS
OF POOR QUALITY

fente 0.02 mm

$\phi = 1 \text{ mm}$

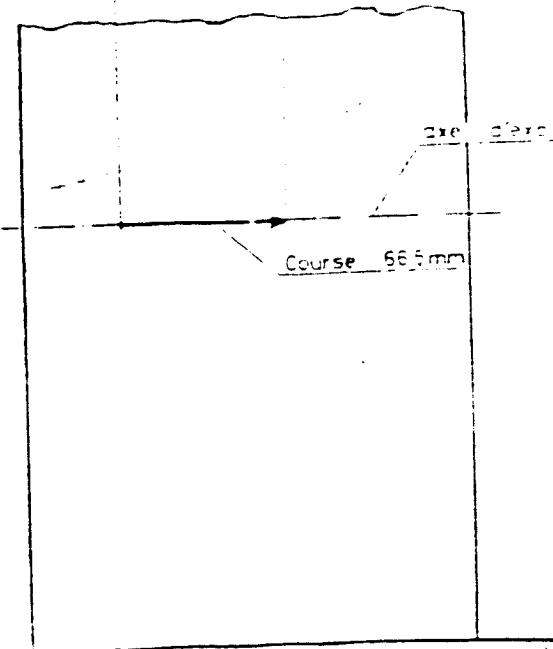
0.05 mm

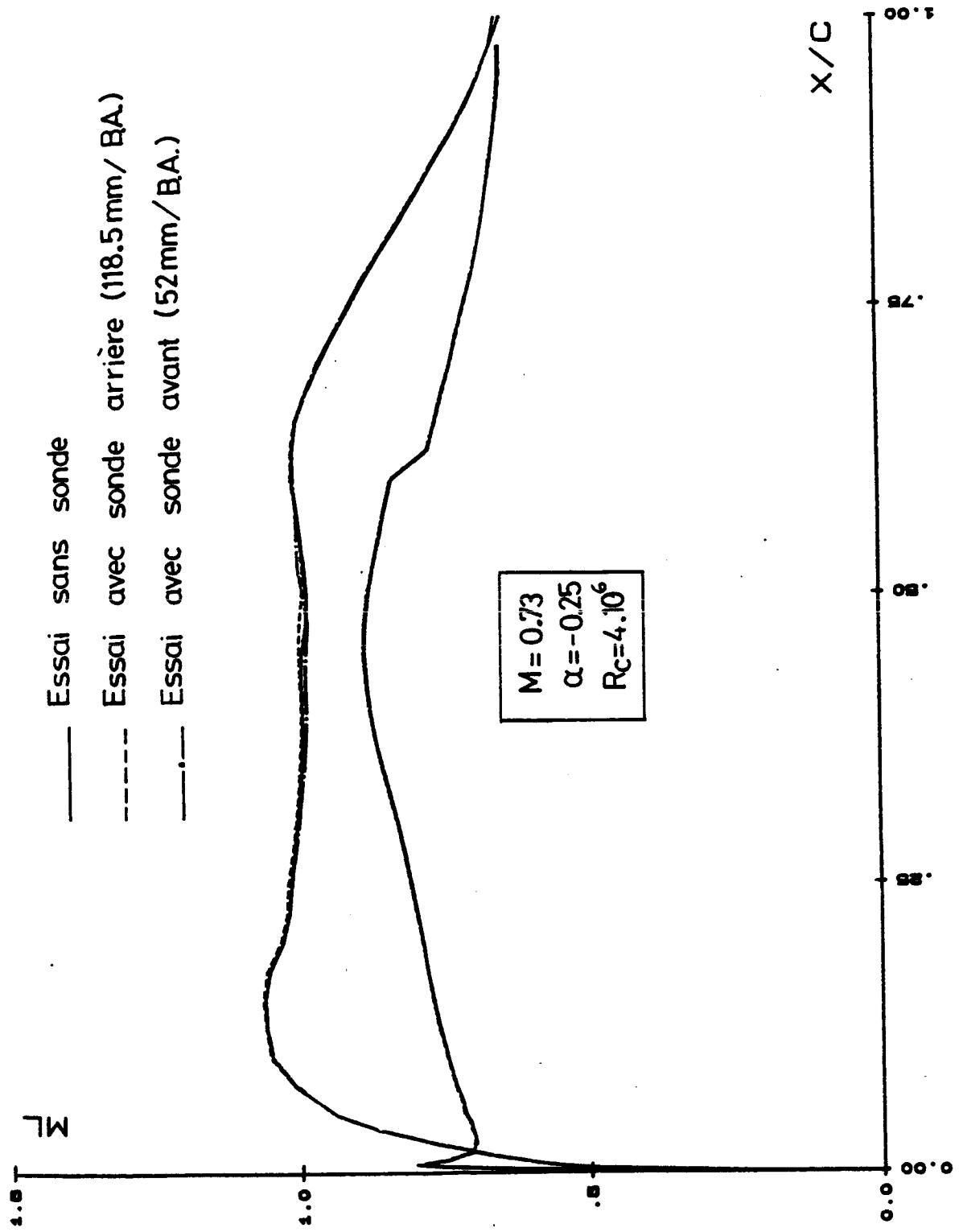
1.5 mm



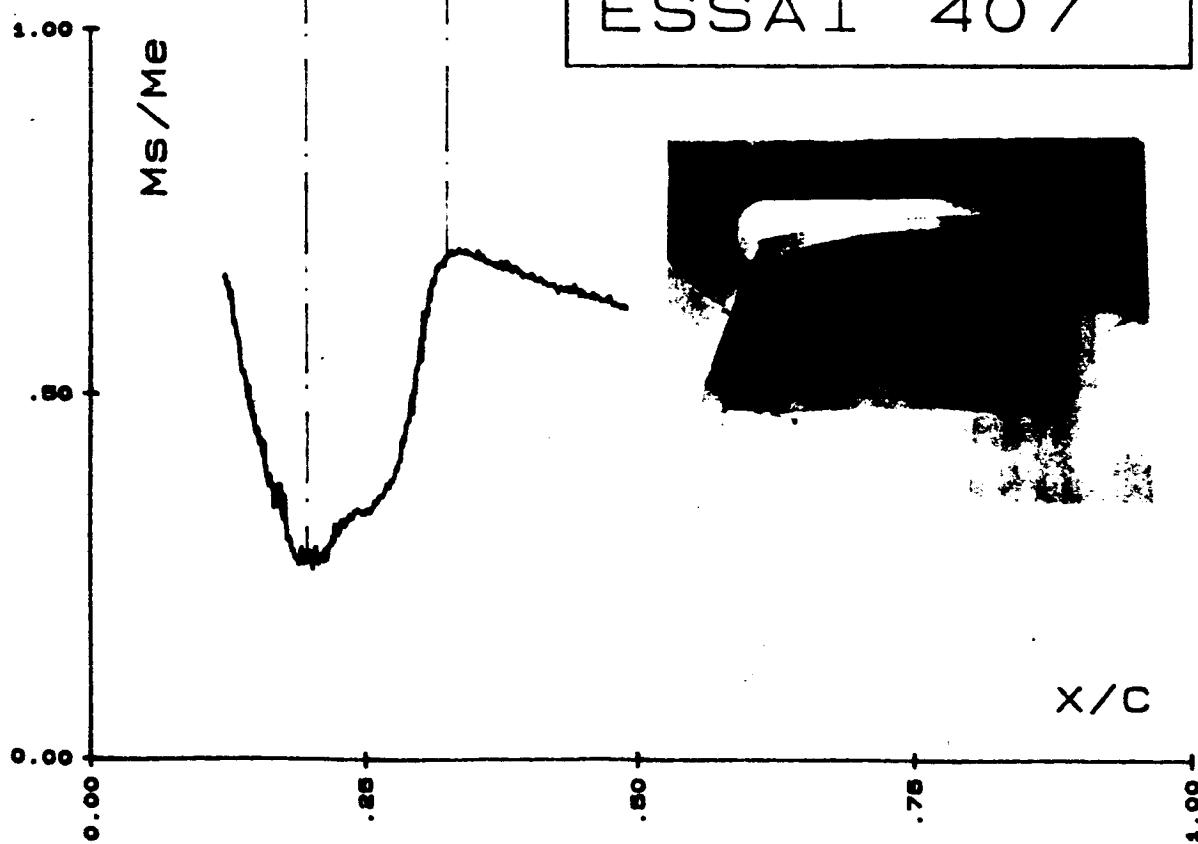
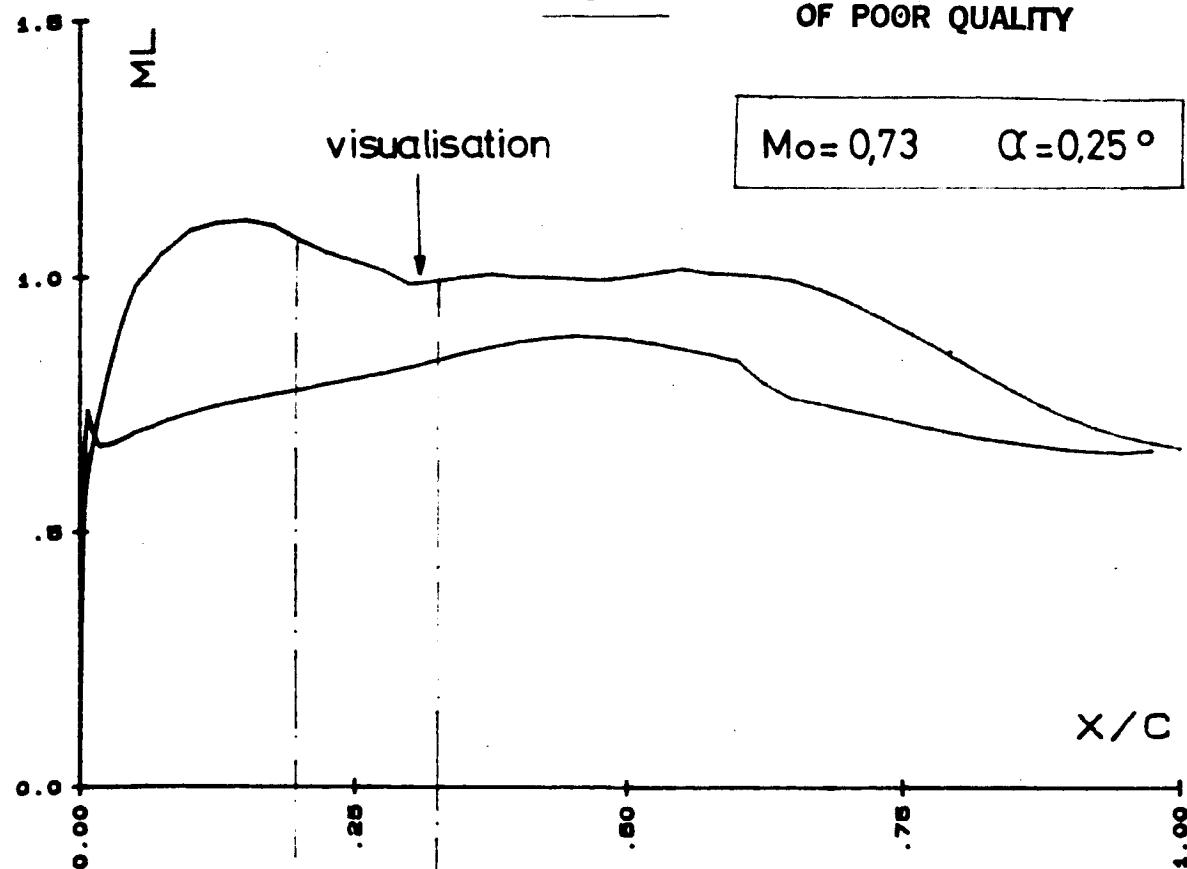
axe d'oscillation

Course 66.5 mm





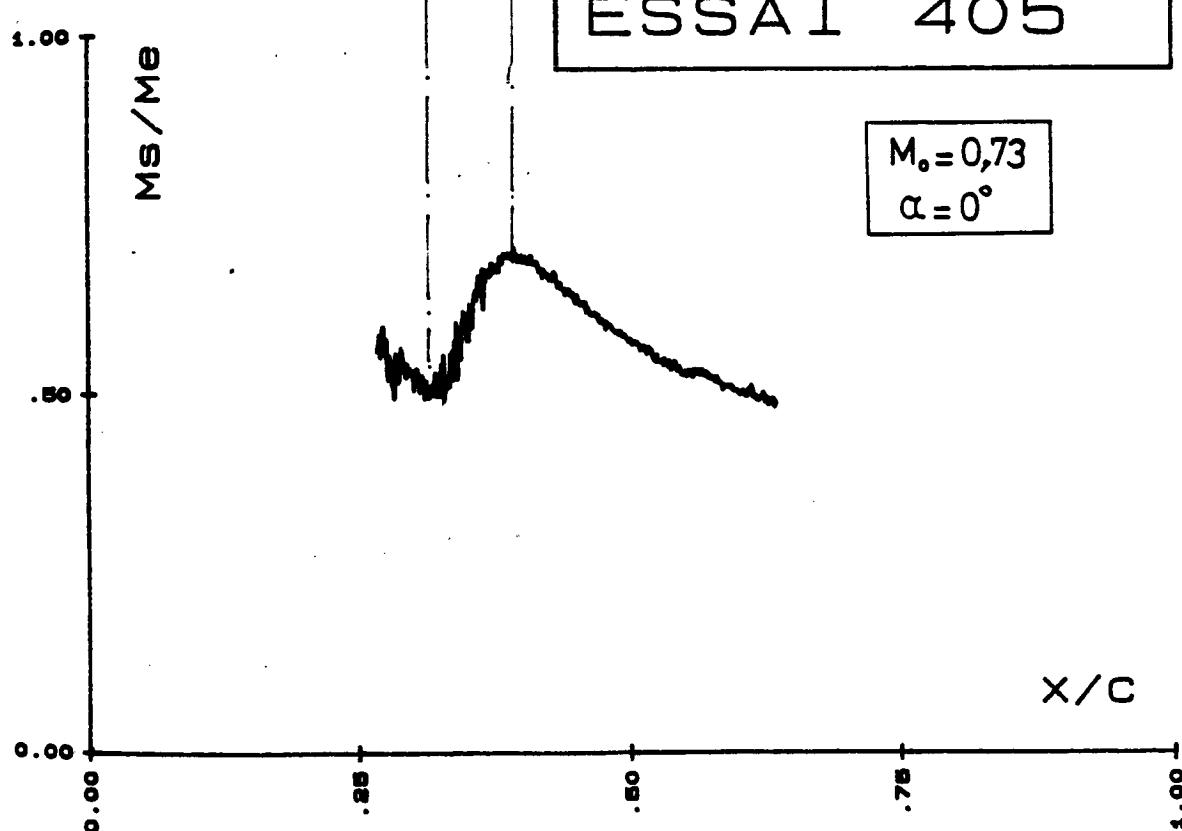
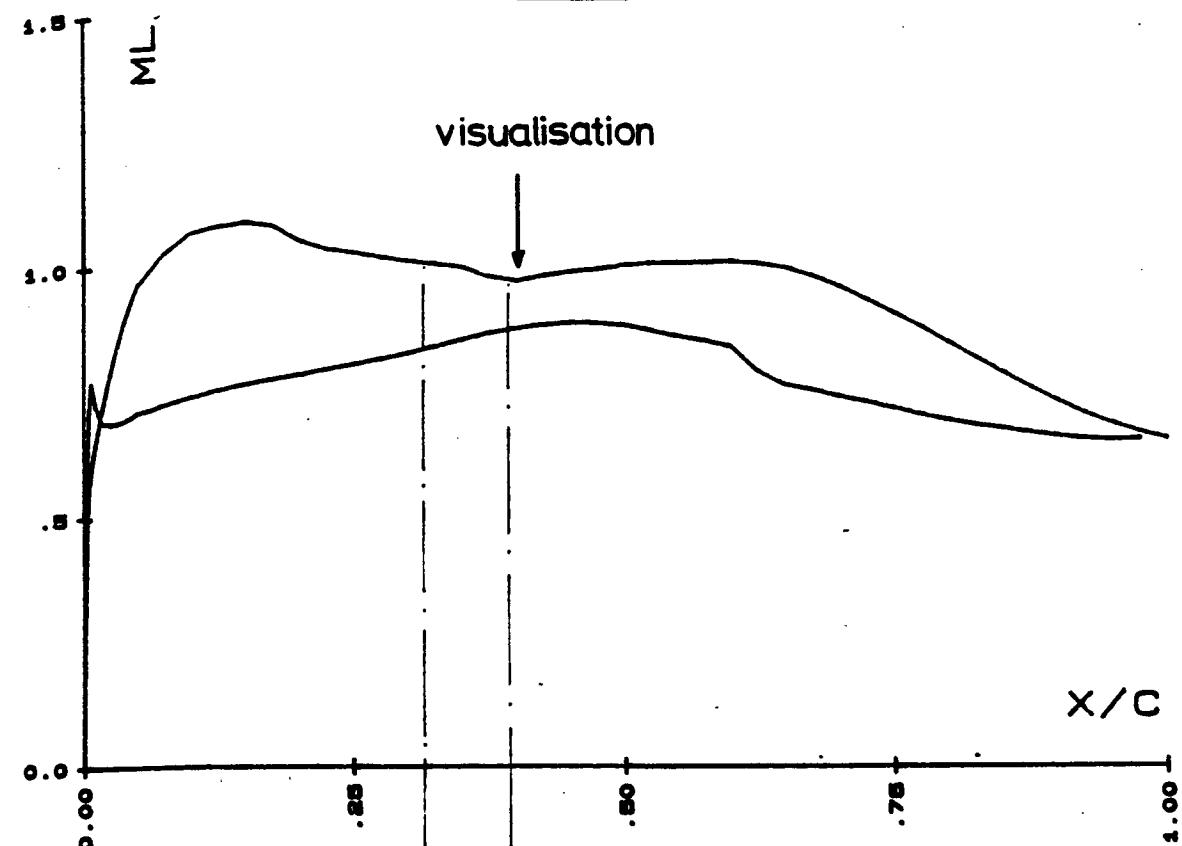
INFLUENCE DE LA PRÉSENCE DE LA SONDE



REPERAGE DE LA POSITION DE TRANSITION PAR SONDE D'ARRET

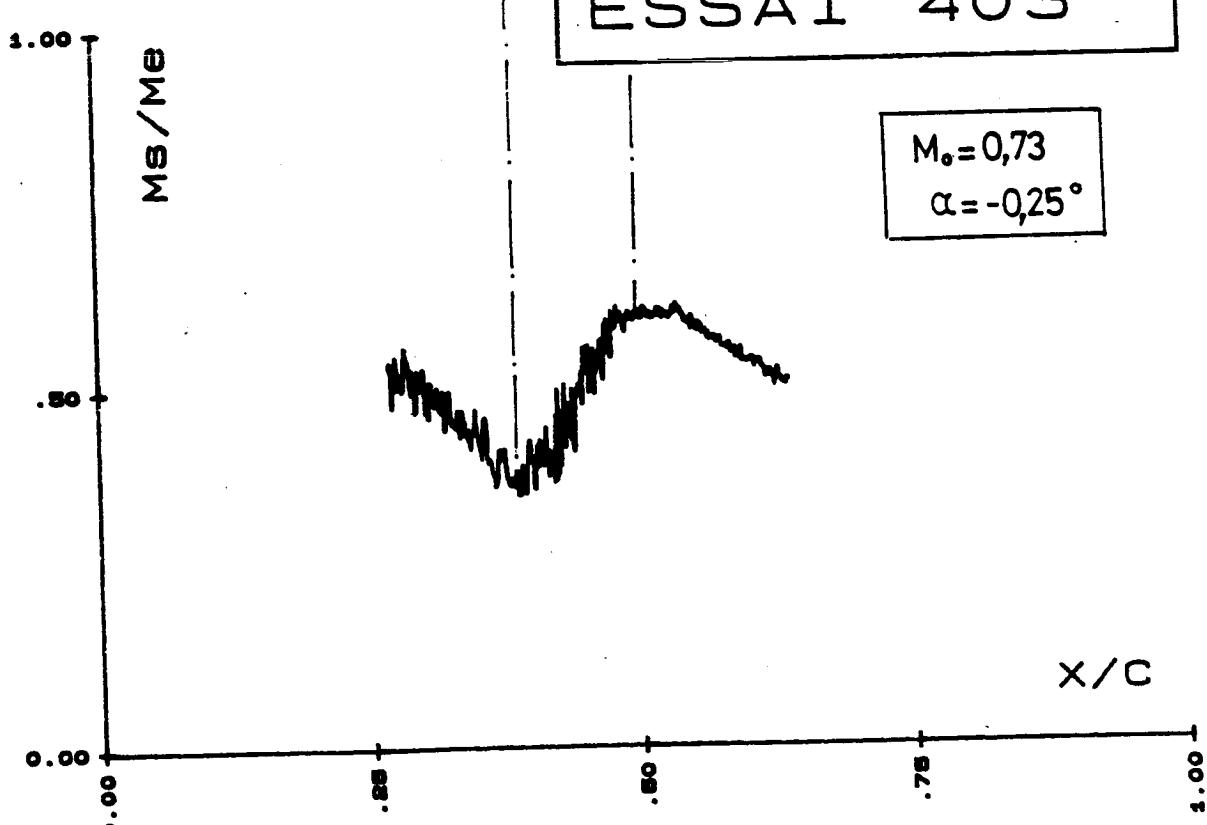
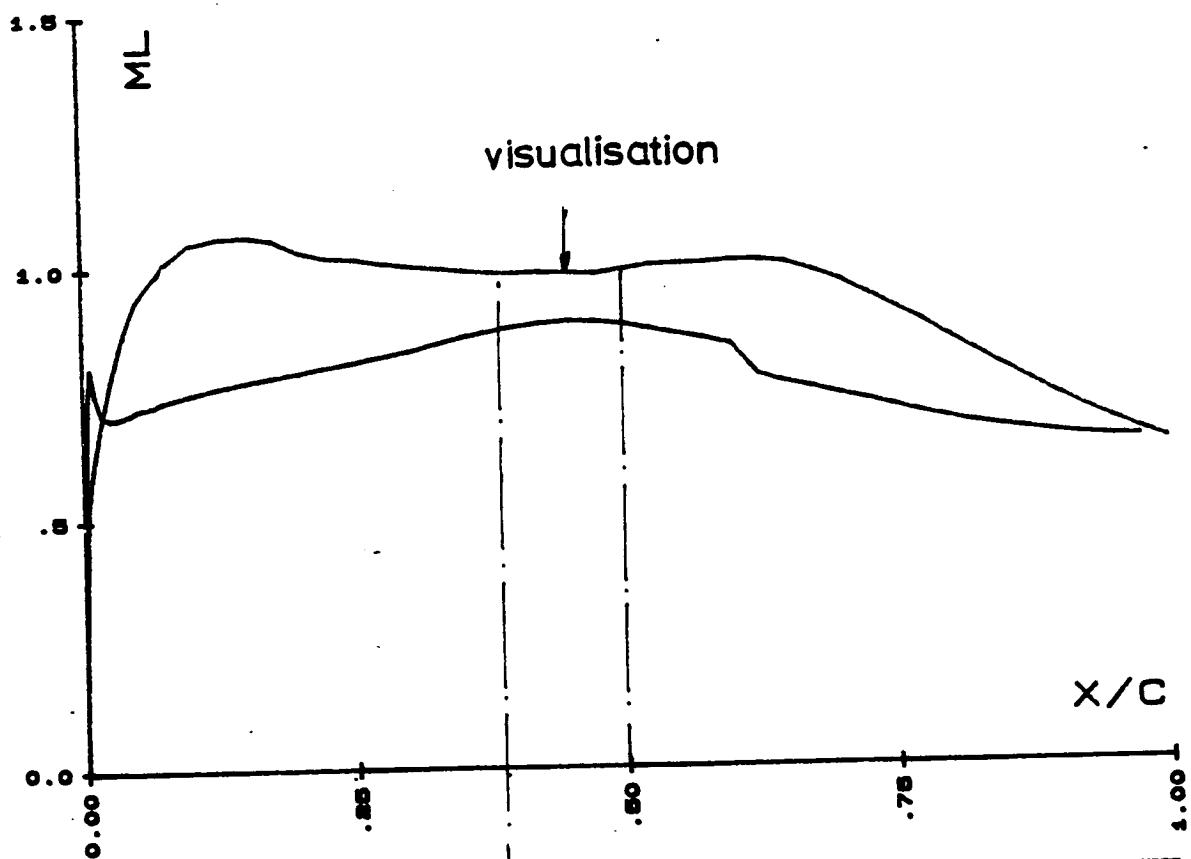
$M_o = 0,73, \quad \alpha = -0,25^\circ$

PL. 11



REPERAGE DE LA POSITION DE TRANSITION PAR SONDE D'ARRET

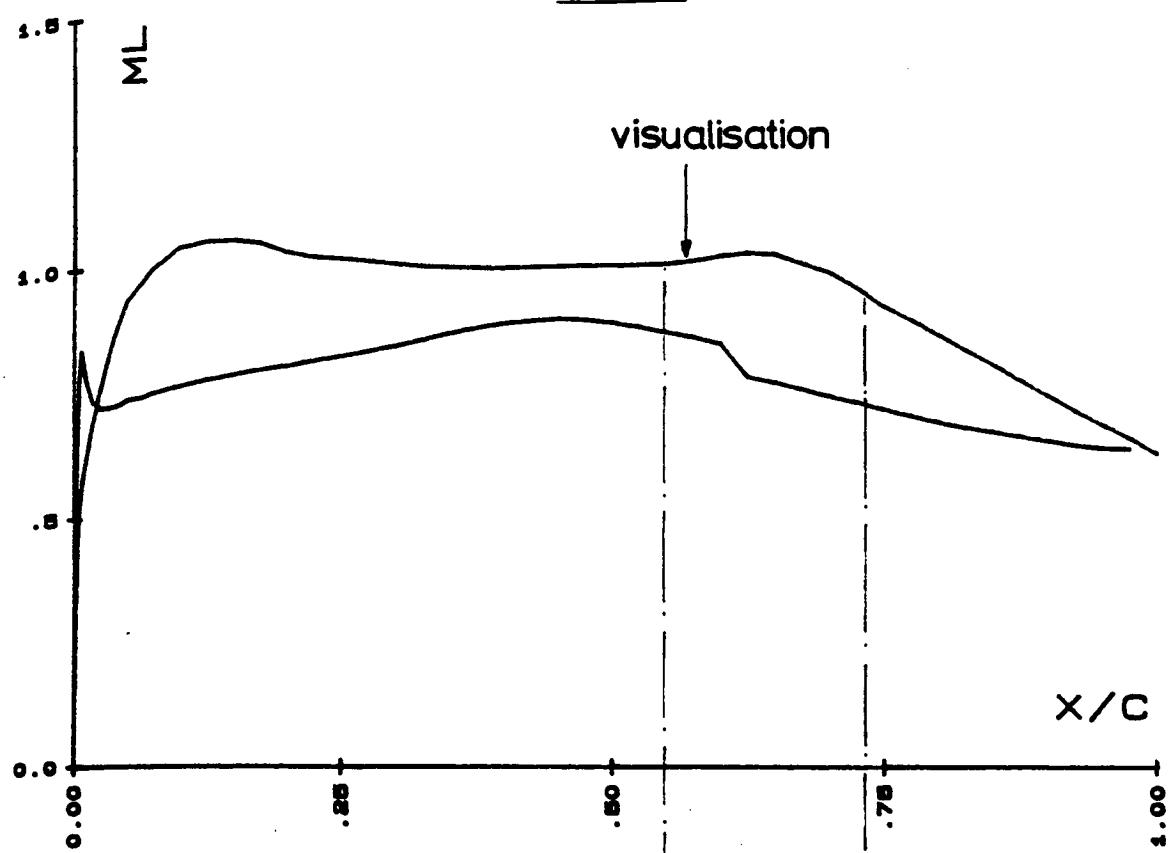
$M_\infty = 0,73 \quad \alpha = 0^\circ$



REPERAGE DE LA POSITION DE TRANSITION PAR SONDE D'ARRET

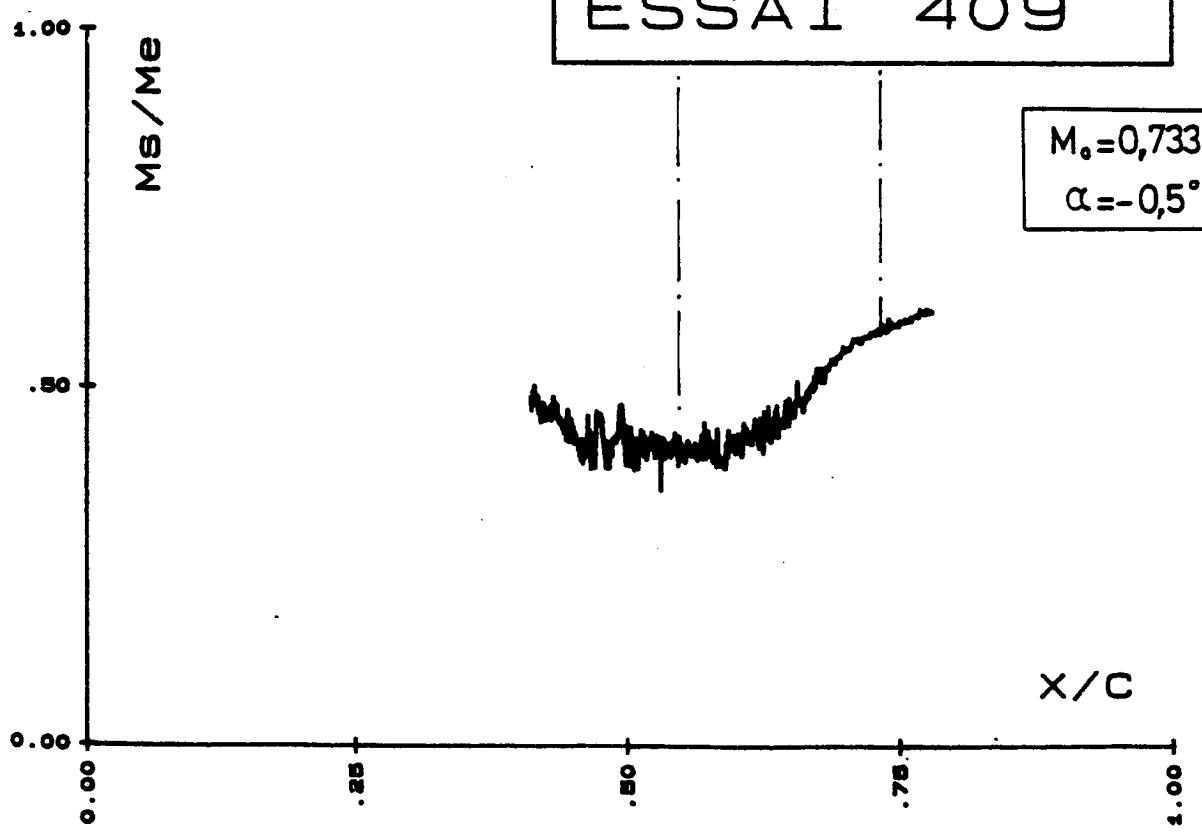
$M_{\infty} = 0,73 \quad \alpha = -0,25^{\circ}$

PL. 13



ESSAI 409

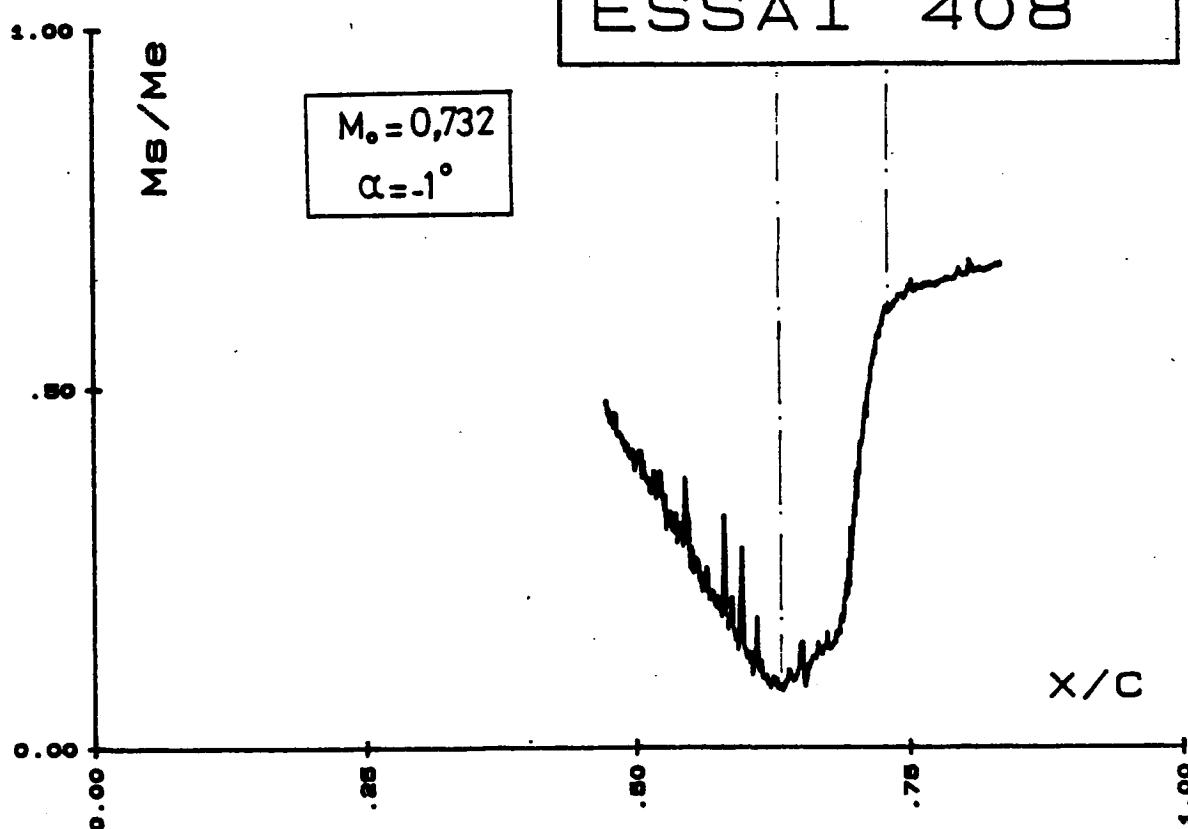
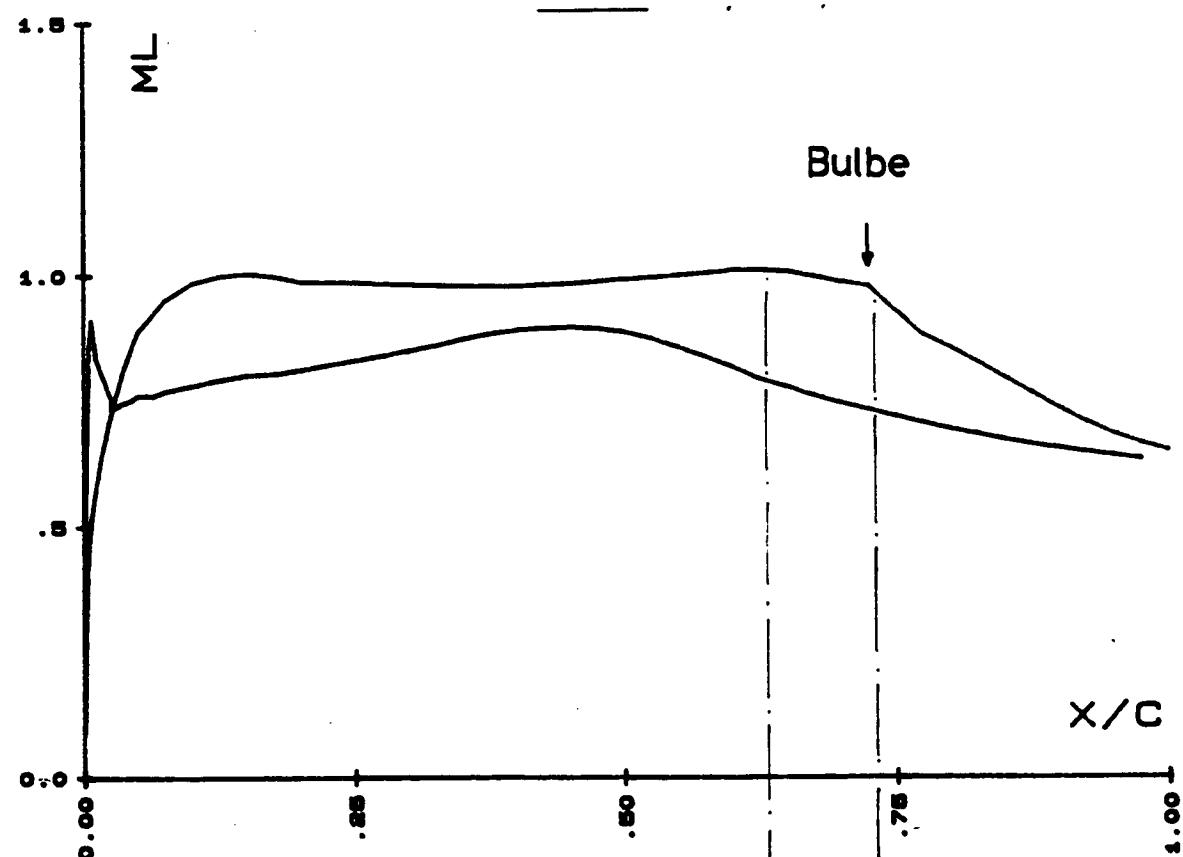
$M_\infty = 0,733$
 $\alpha = -0,5^\circ$



REPERAGE DE LA POSITION DE TRANSITION PAR SONDE D'ARRET

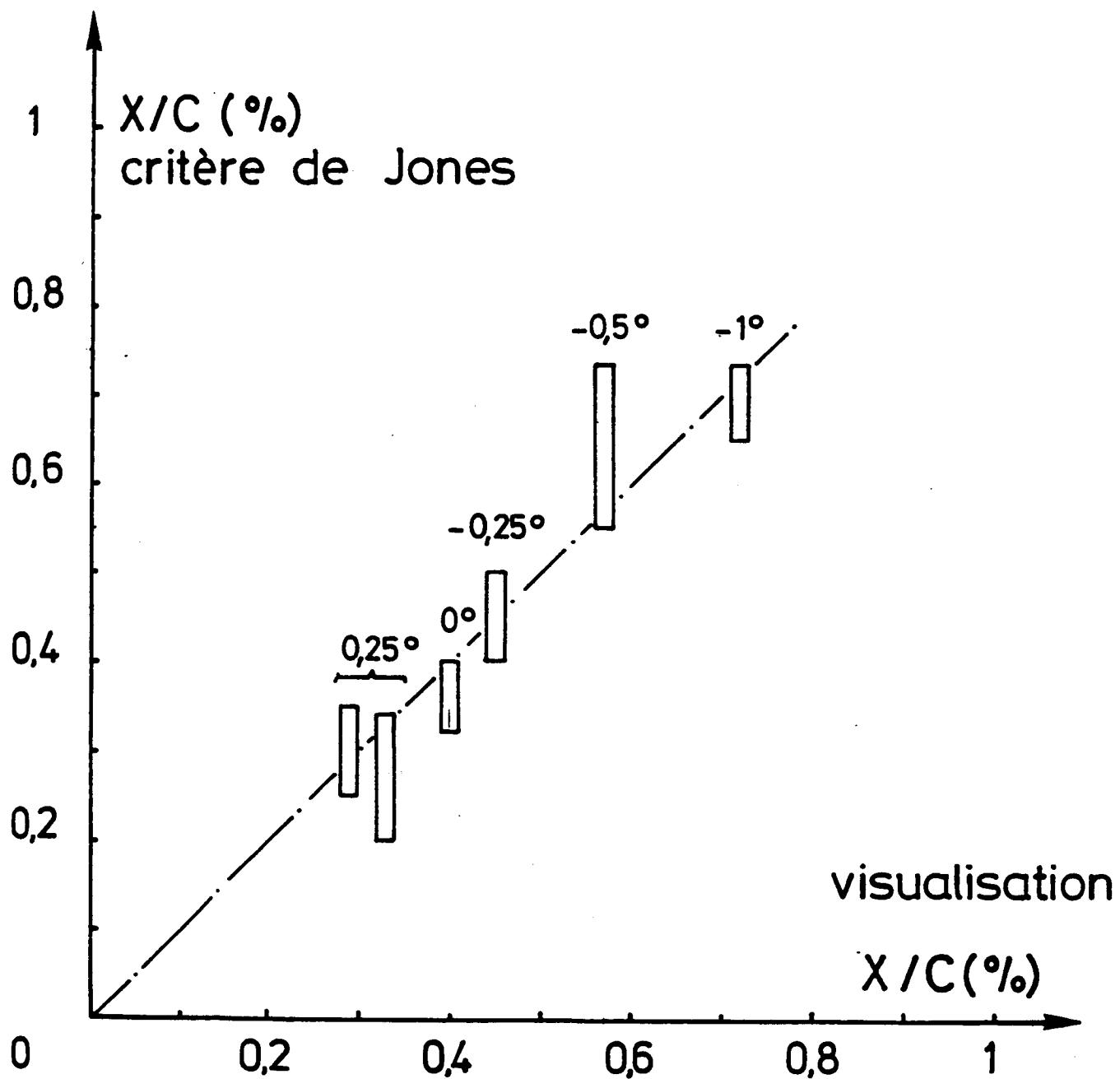
$M_\infty = 0,73 \quad \alpha = -0,5^\circ$

PL. 14



REPERAGE DE LA POSITION DE TRANSITION PAR SONDE D'ARRET

M₈ = 0,73 α = - 1°

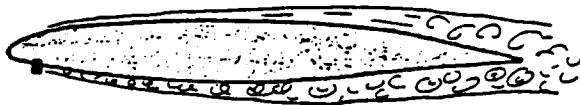


REPERAGE DE LA POSITION DE TRANSITION : COMPARAISON CRITERE
DE JONES - VISUALISATION

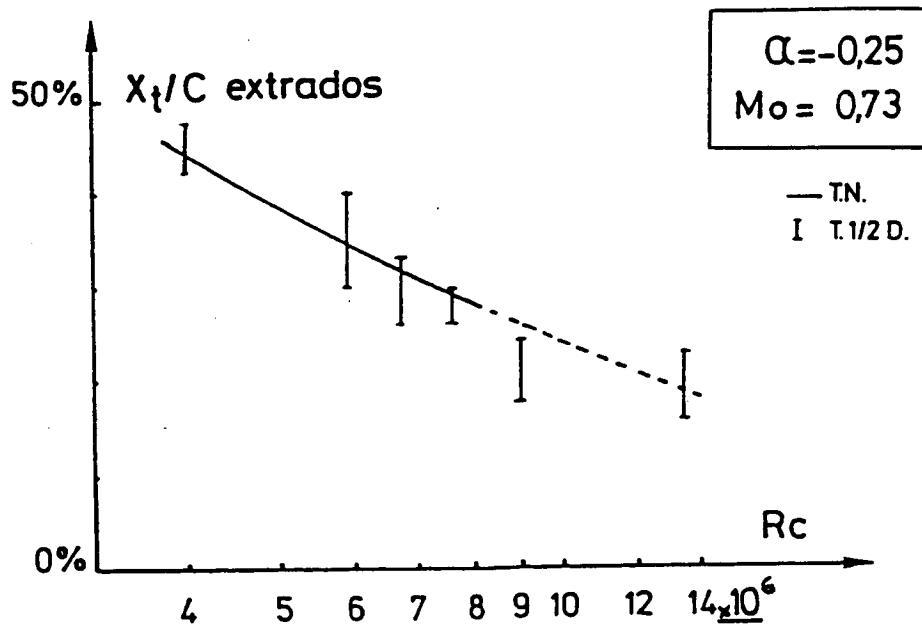
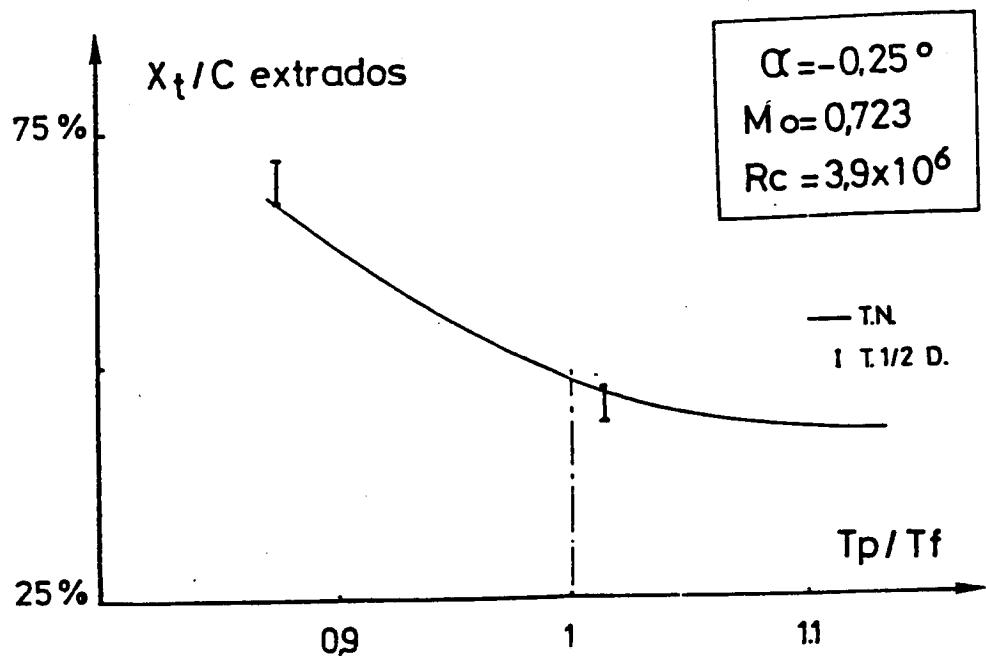
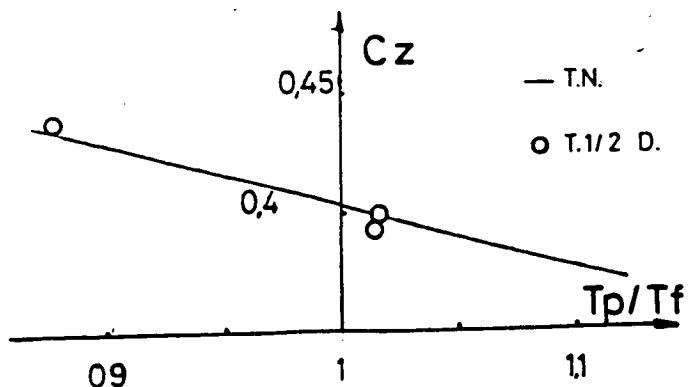
Page sans texte

**ESSAIS EN TRANSITION
DEMI-DECLENCHEE**

T. 1/2 D.



PLANCHES 16 à 47



COMPARAISON DE RESULTATS T.N. - T. 1/2 D.

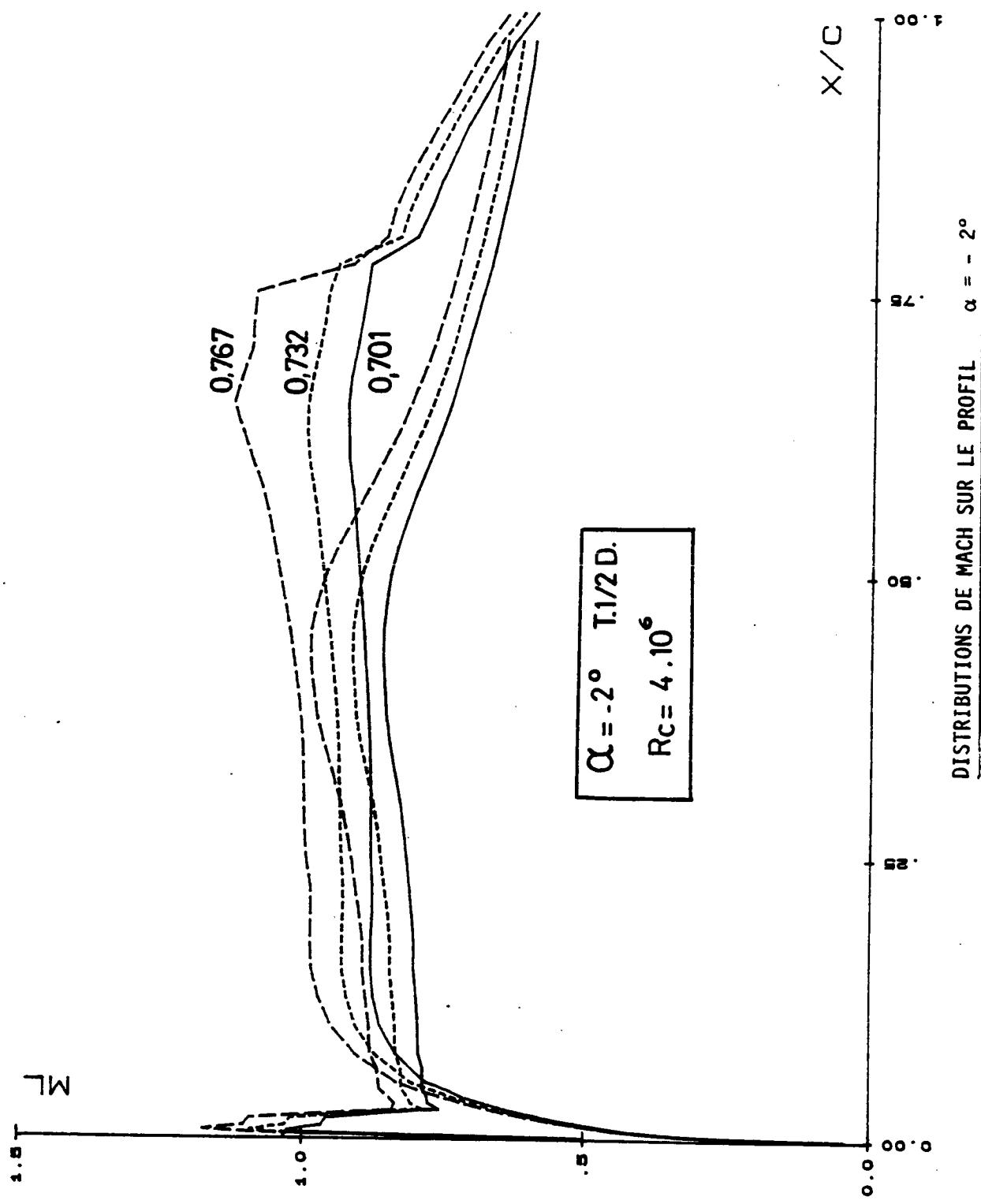
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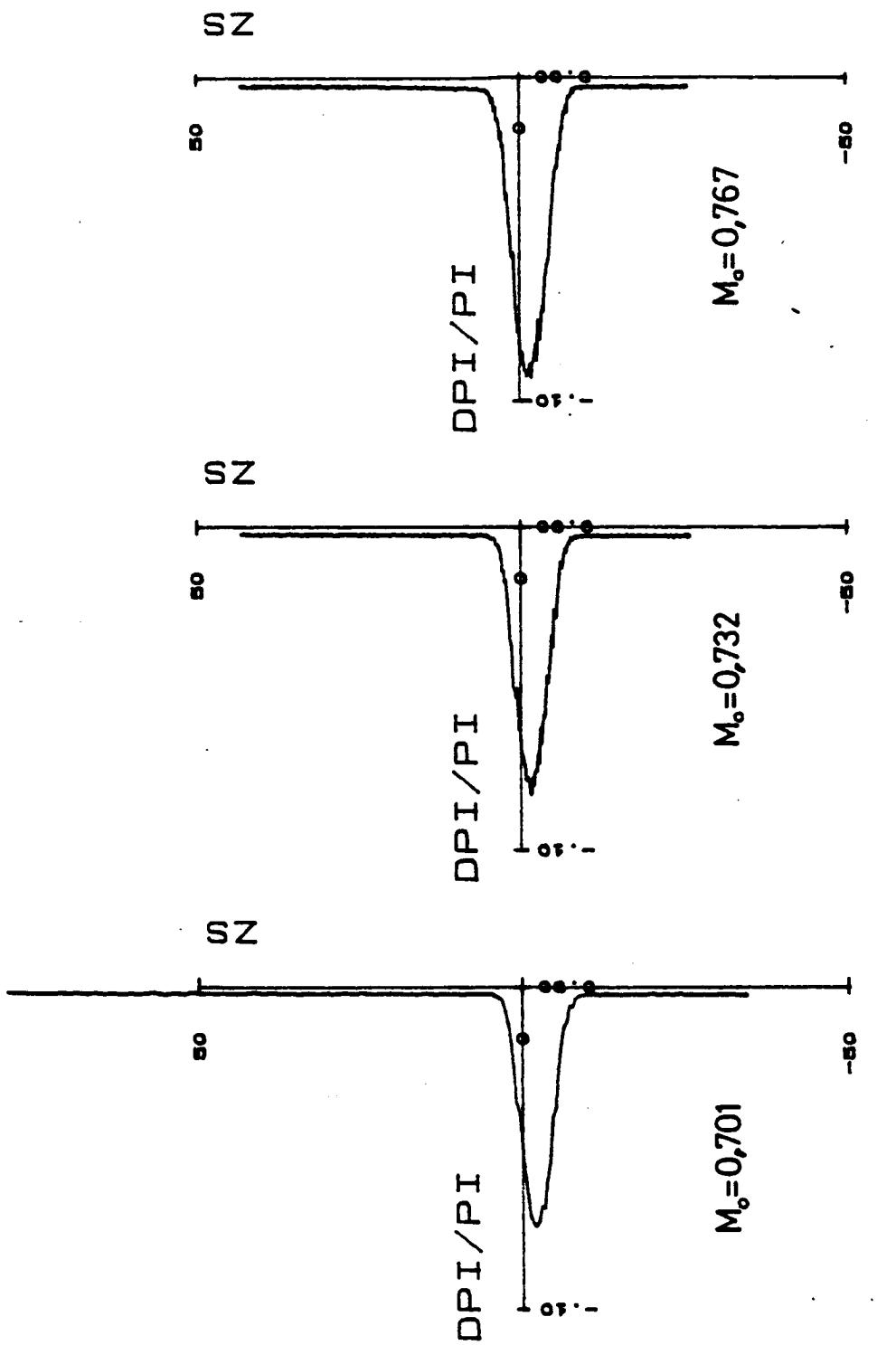
T. 1/2 D.

VARIATION DU NOMBRE DE MACH

$$R_C = 4 \times 10^6$$

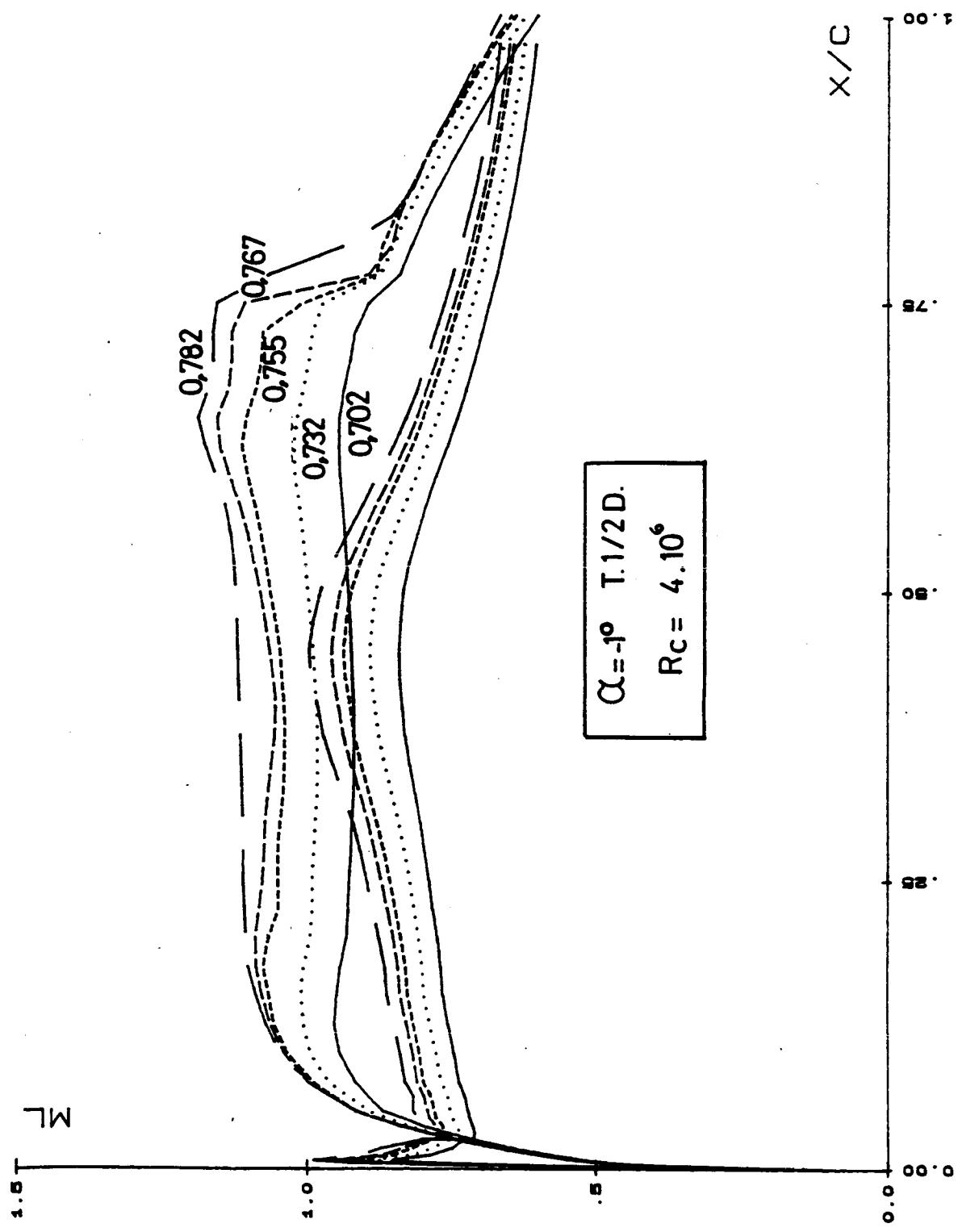
$\alpha = -2^\circ$	PL. 17 et 18
$\alpha = -1^\circ$	PL. 19 et 20
$\alpha = 0,5^\circ$	PL. 21 et 22
$\alpha = 0$	PL. 23 et 24
$\alpha = 1^\circ$	PL. 25 et 26
$\alpha = 2^\circ$	PL. 27 et 28





$\alpha = -2^\circ \quad T = 1/2 D \quad R_c = 4 \cdot 10^6$

SONDAGES DES SILLAGES $\alpha = -2^\circ$



PL. 20

NS

50

-50

DPI/PI

DPI/PI

DPI/PI

DPI/PI

M=0,782

M=0,767

M=0,755

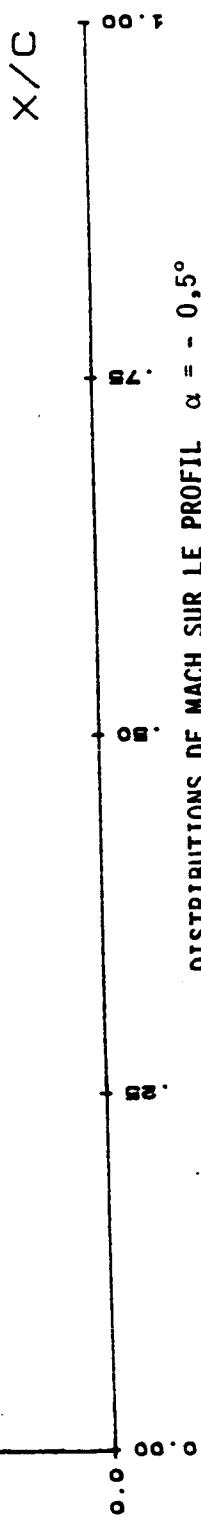
M=0,732

M=0,702

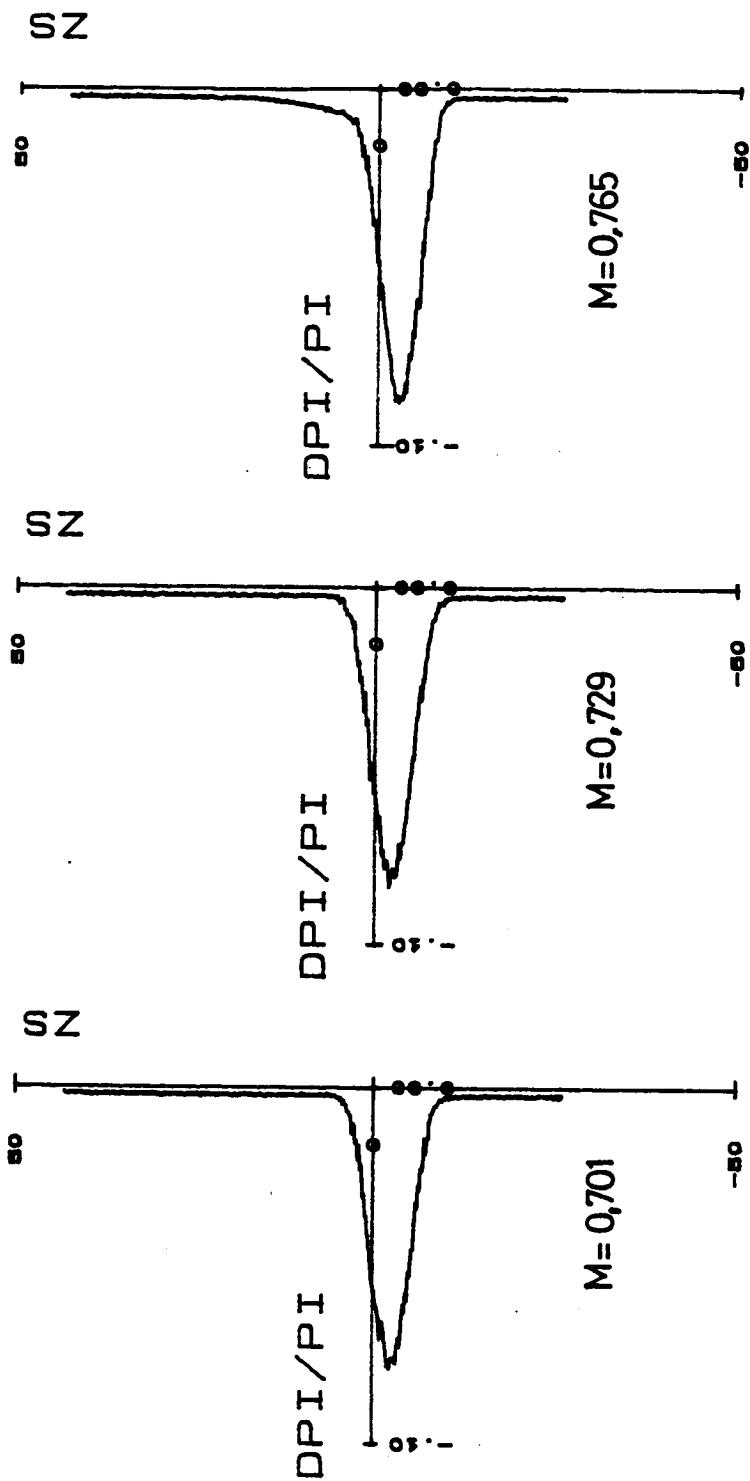
SONDAGES DES SILLAGES $\alpha = -1^\circ$

$\alpha = -1^\circ \quad R_c = 4 \cdot 10^6 \quad T = 1/2 D.$

DISTRIBUTIONS DE MACH SUR LE PROFIL $\alpha = -0.5^\circ$

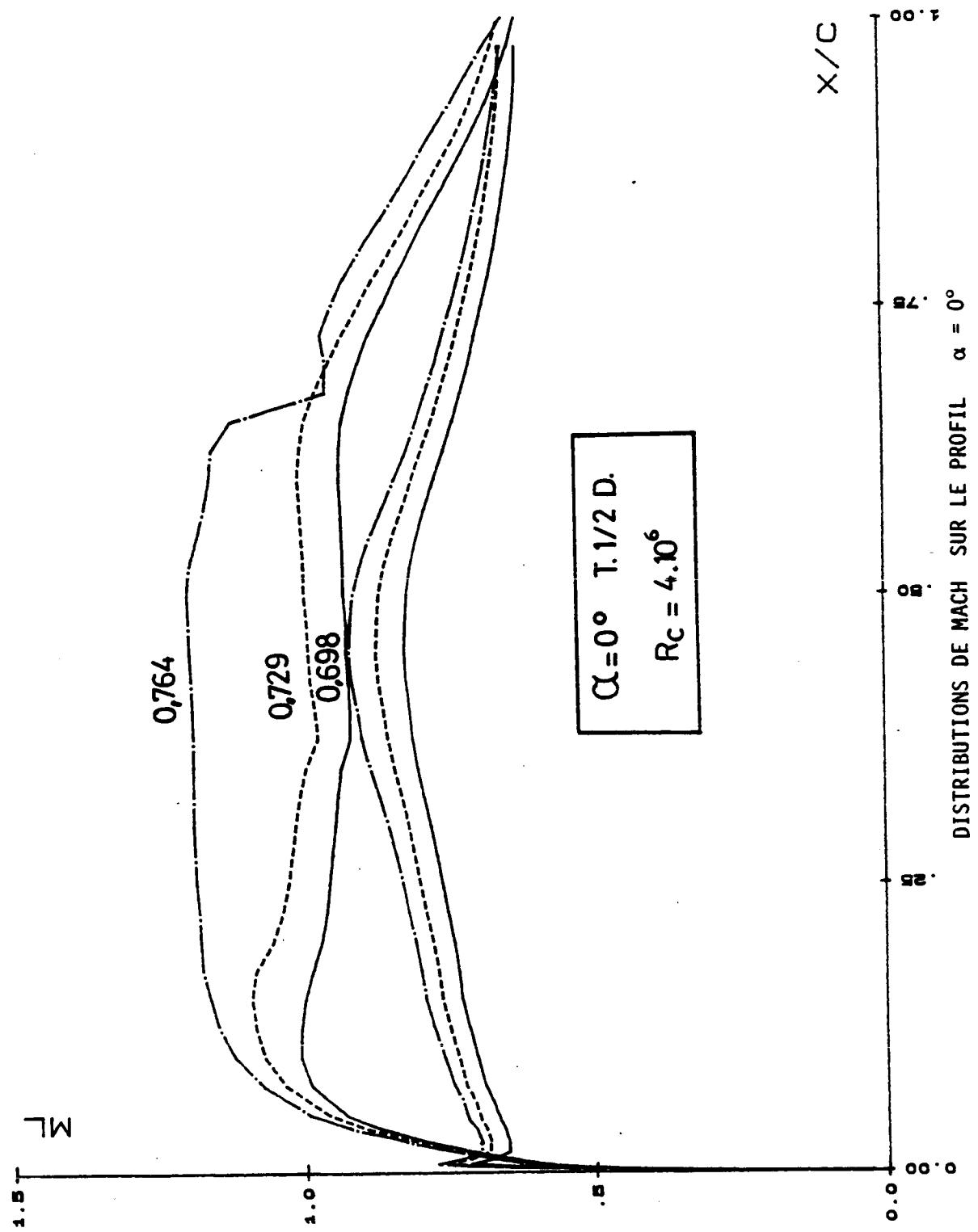


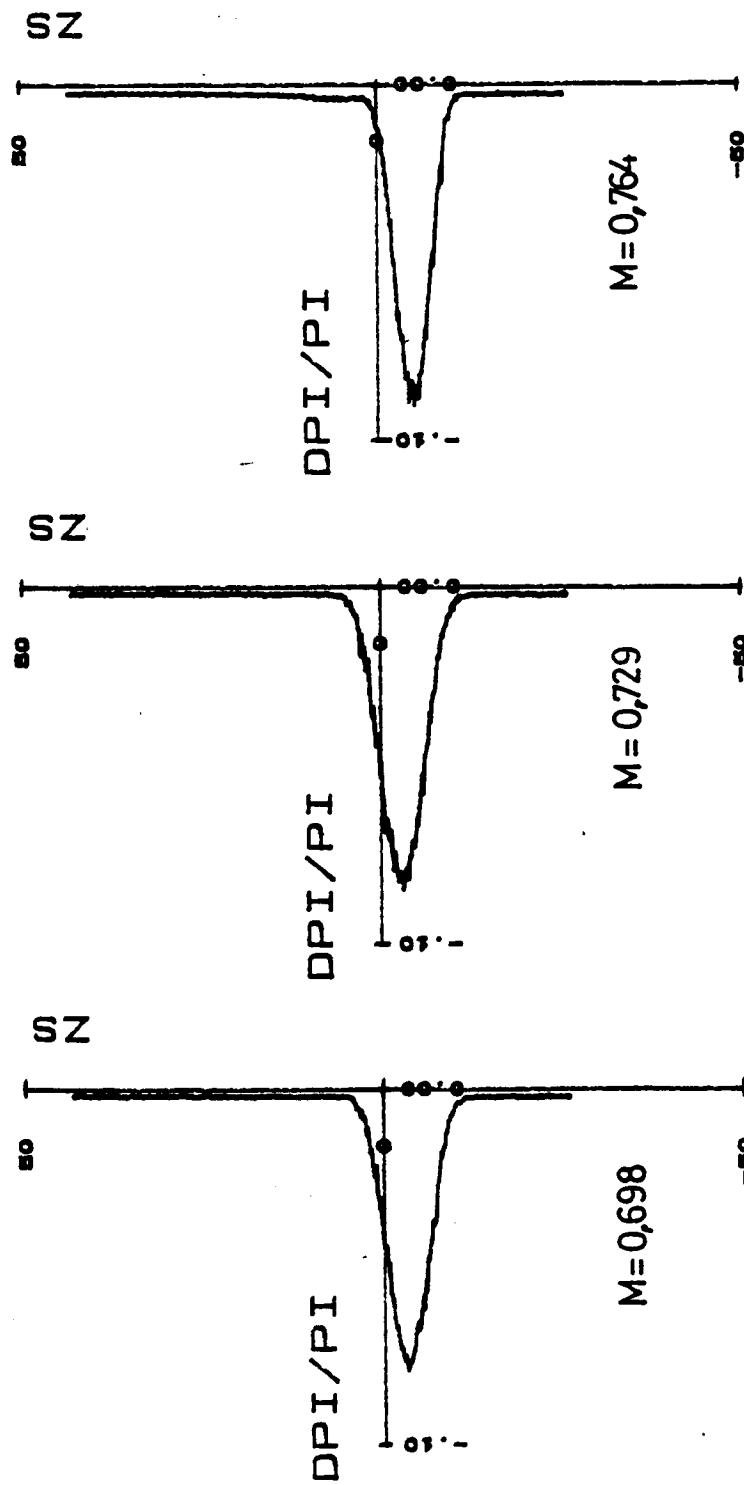
$\alpha = -0.5^\circ \quad T = 1/2 D$
 $R_C = 4 \cdot 10^6$



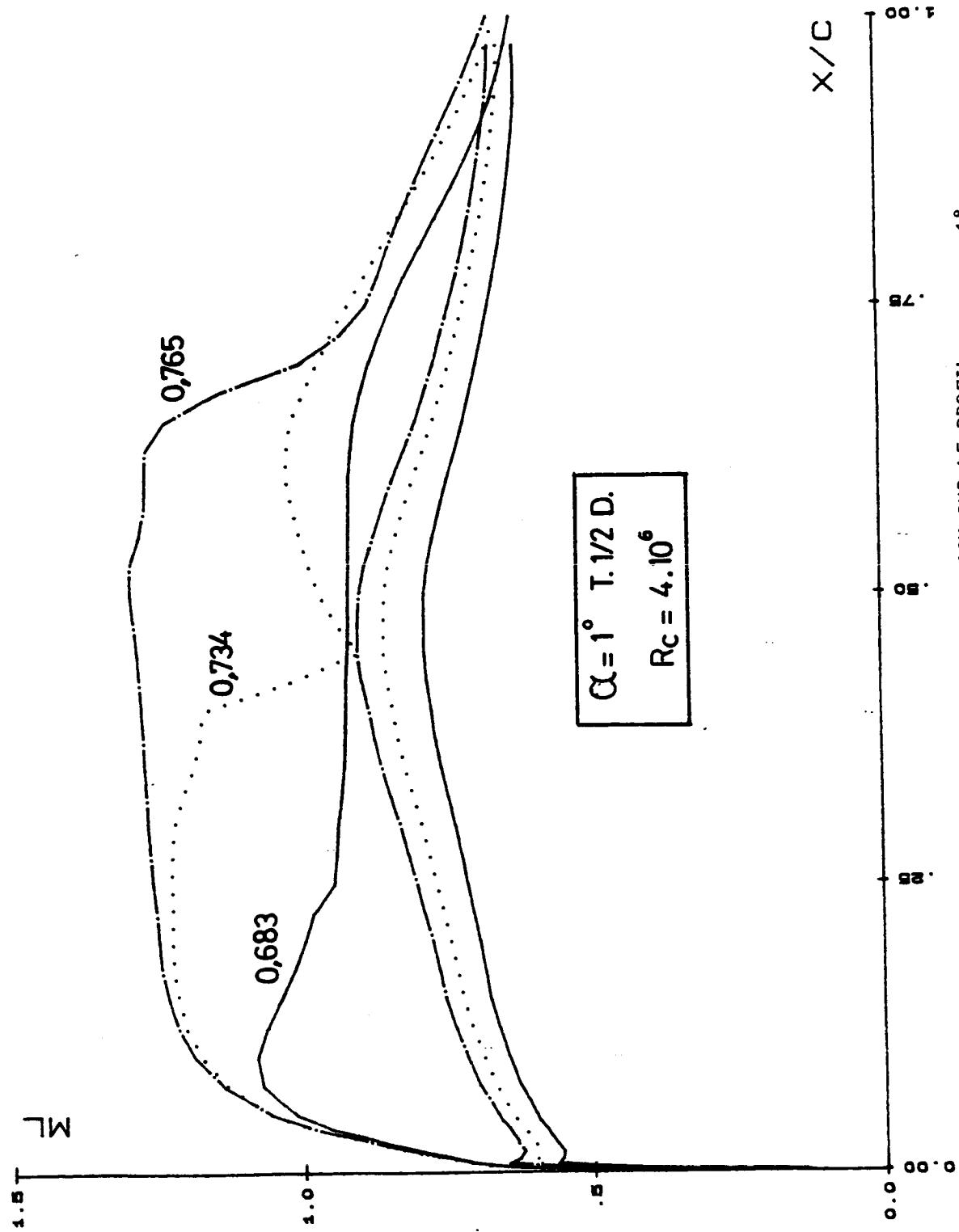
$$\alpha = -0.5^\circ \quad R_c = 4 \cdot 10^6 \quad T = 1/2 D.$$

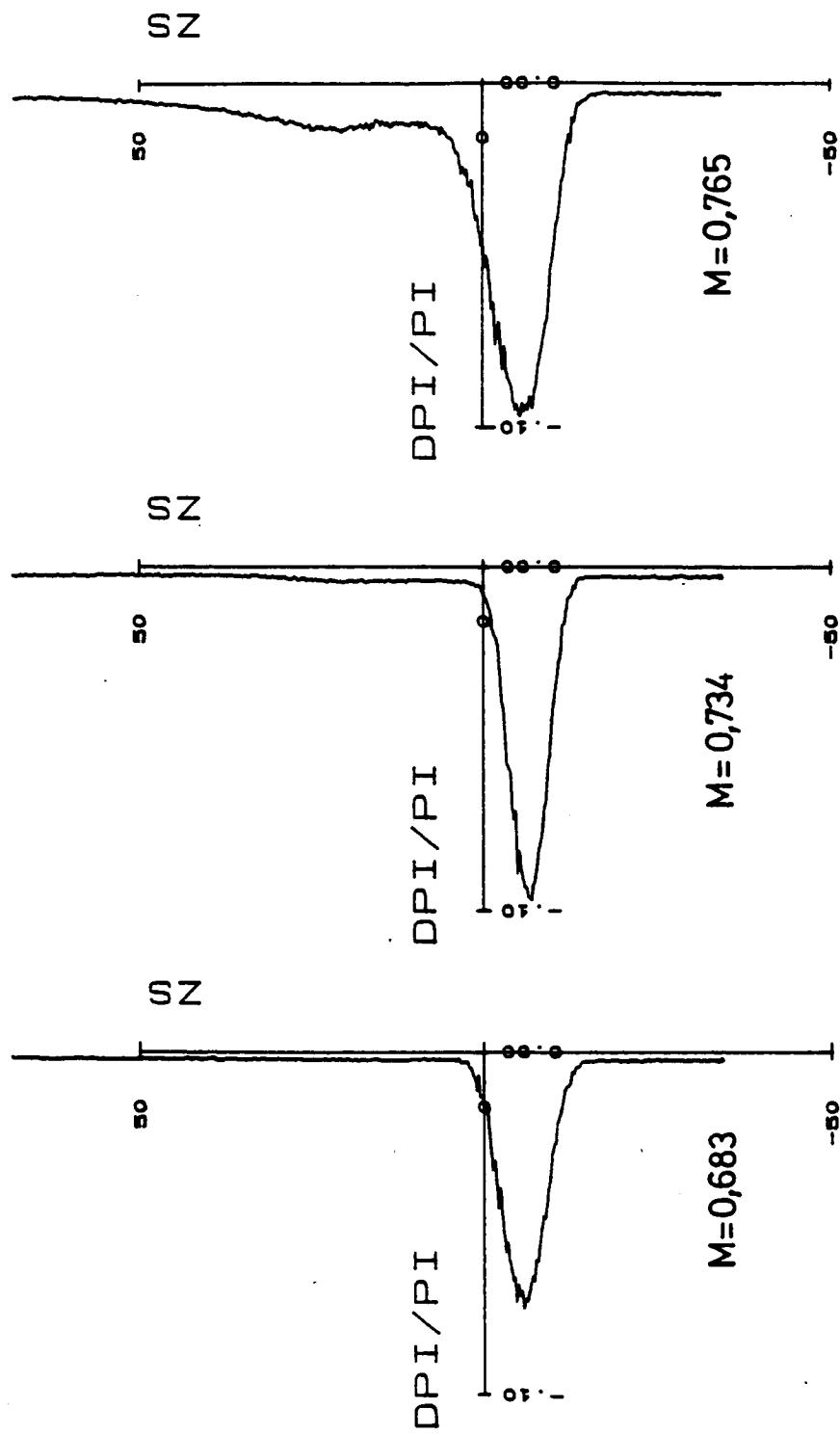
SONDAGES DES SILLAGES $\alpha = -0.5^\circ$





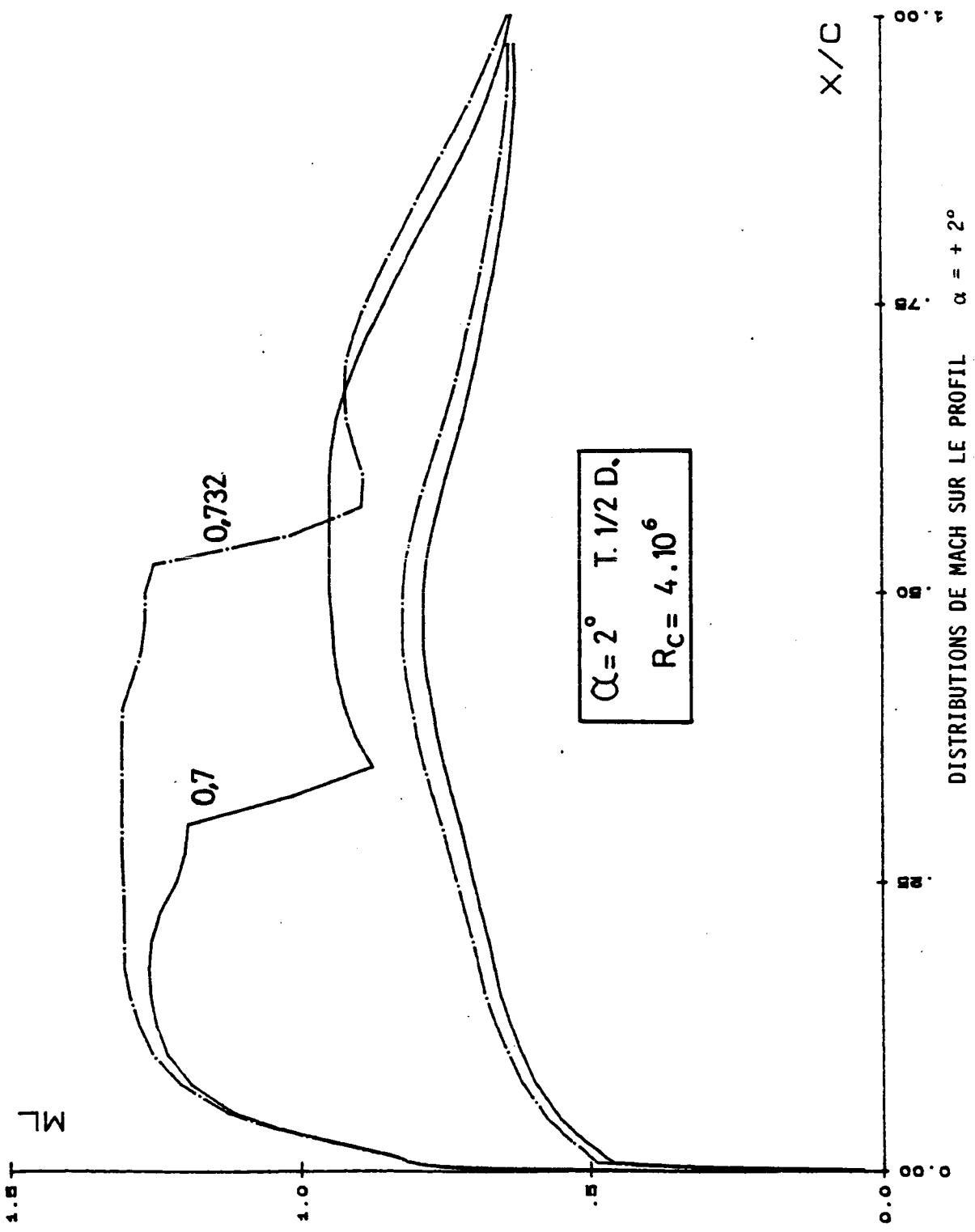
$\alpha = 0^\circ \quad R_c = 4 \cdot 10^6 \quad T = 1/2 D.$
SONDAGES DES SILLAGES $\alpha = 0^\circ$

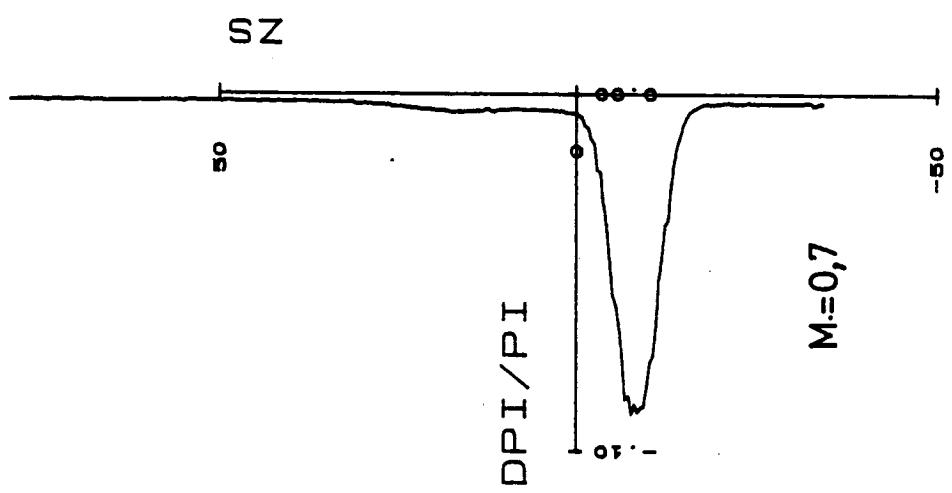
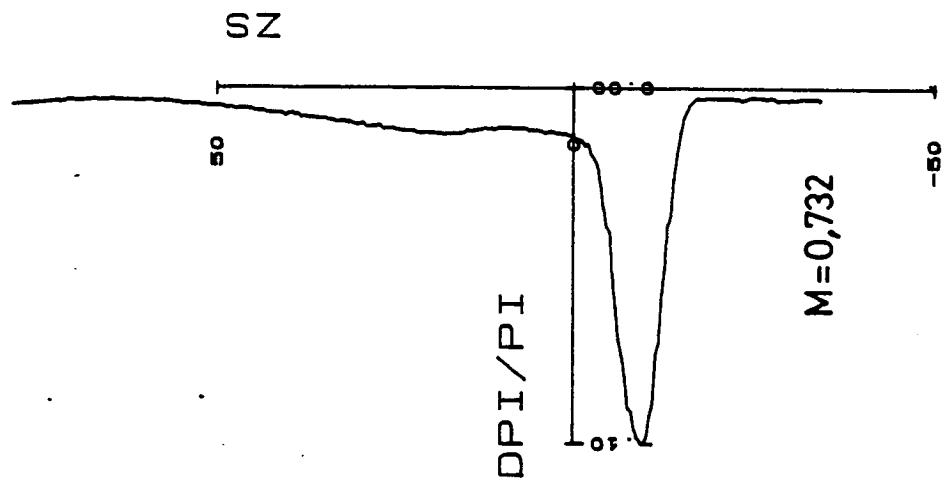




$$\alpha = 1^\circ \quad R_c = 4.10^6 \quad T. 1/2 D.$$

SONDAGES DES SILLAGES $\alpha = 1^\circ$





$\alpha = 2^\circ$ $R_c = 4 \cdot 10^6$ $T \cdot 1/2 D.$

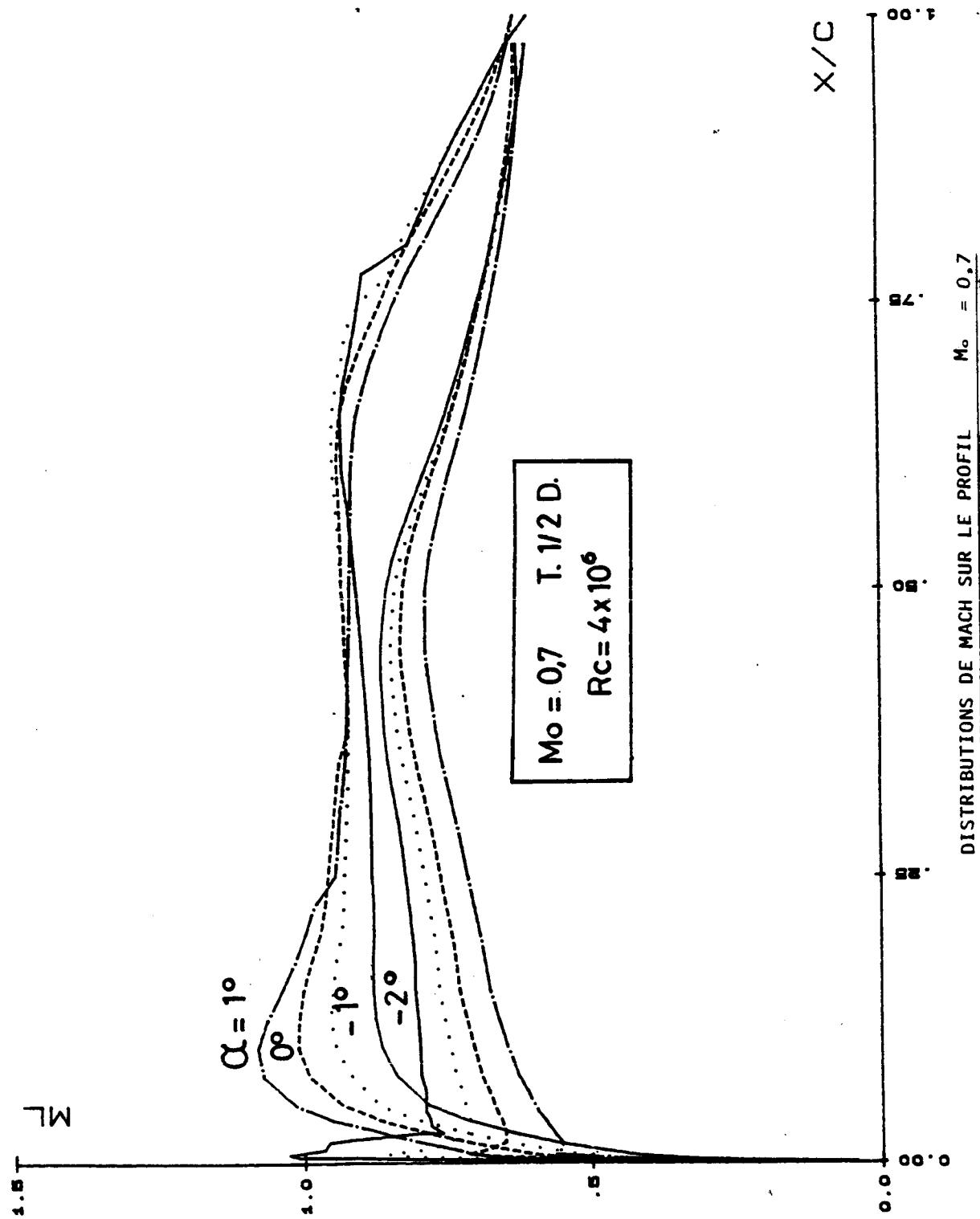
SONDAGES DES SILLAGES $\alpha = + 2^\circ$

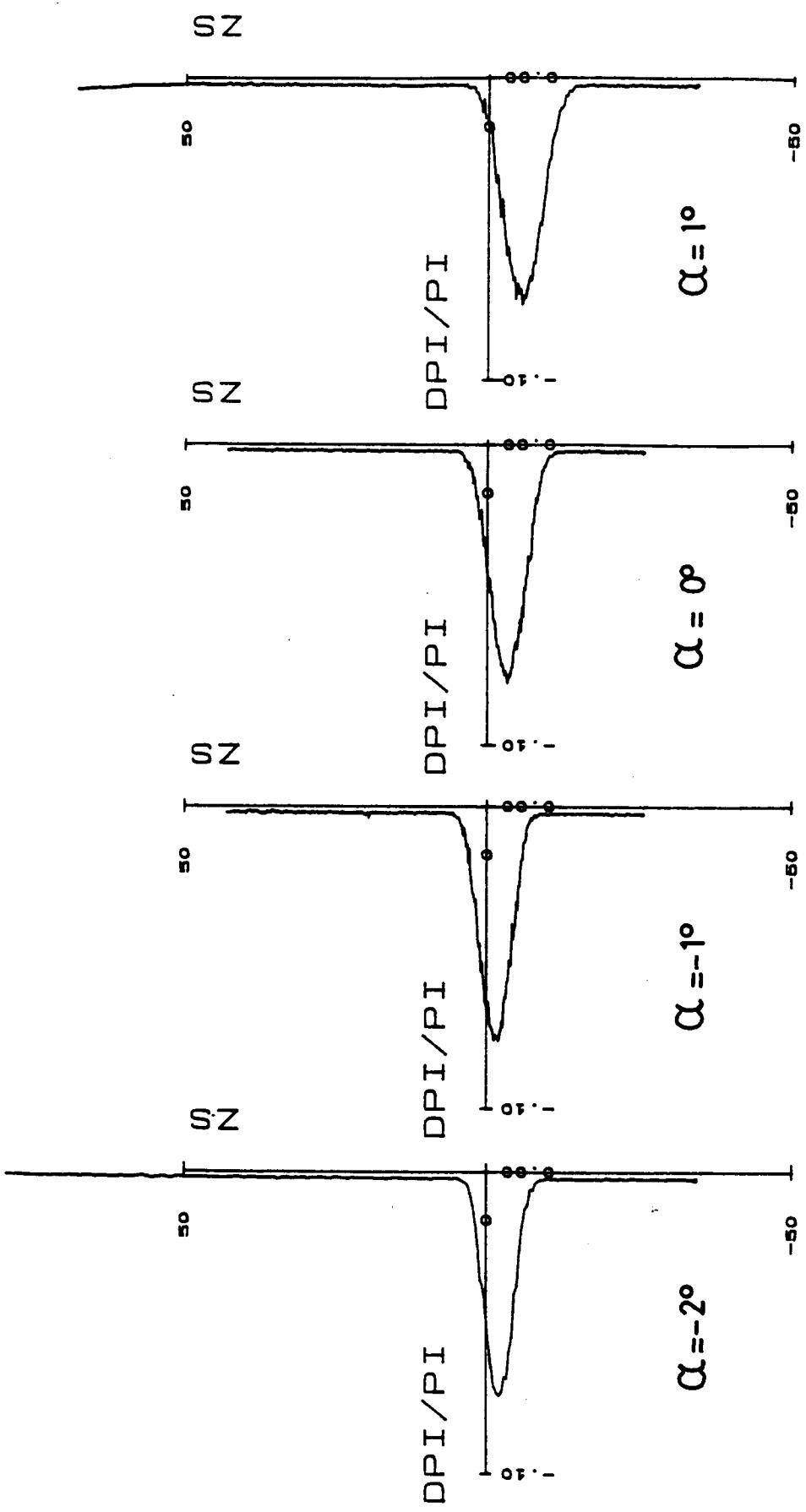
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T. 1/2 D.

VARIATION D'INCIDENCE

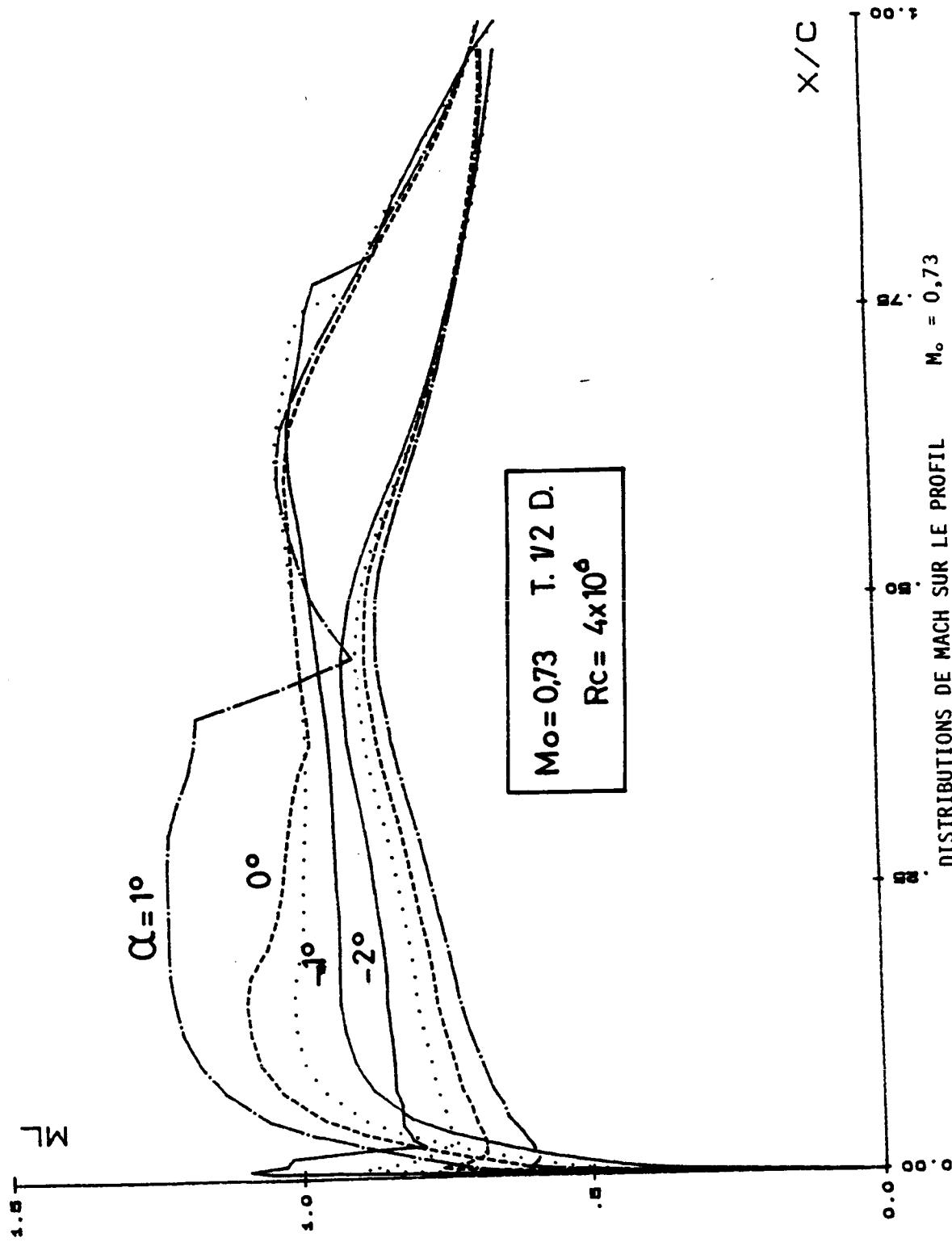
$M_o = 0,7$	PL. 29 et 30
$M_o = 0,73$	PL. 31 et 32
$M_o = 0,766$	PL. 33 et 34
$M_o = 0,784$	PL. 35 et 36

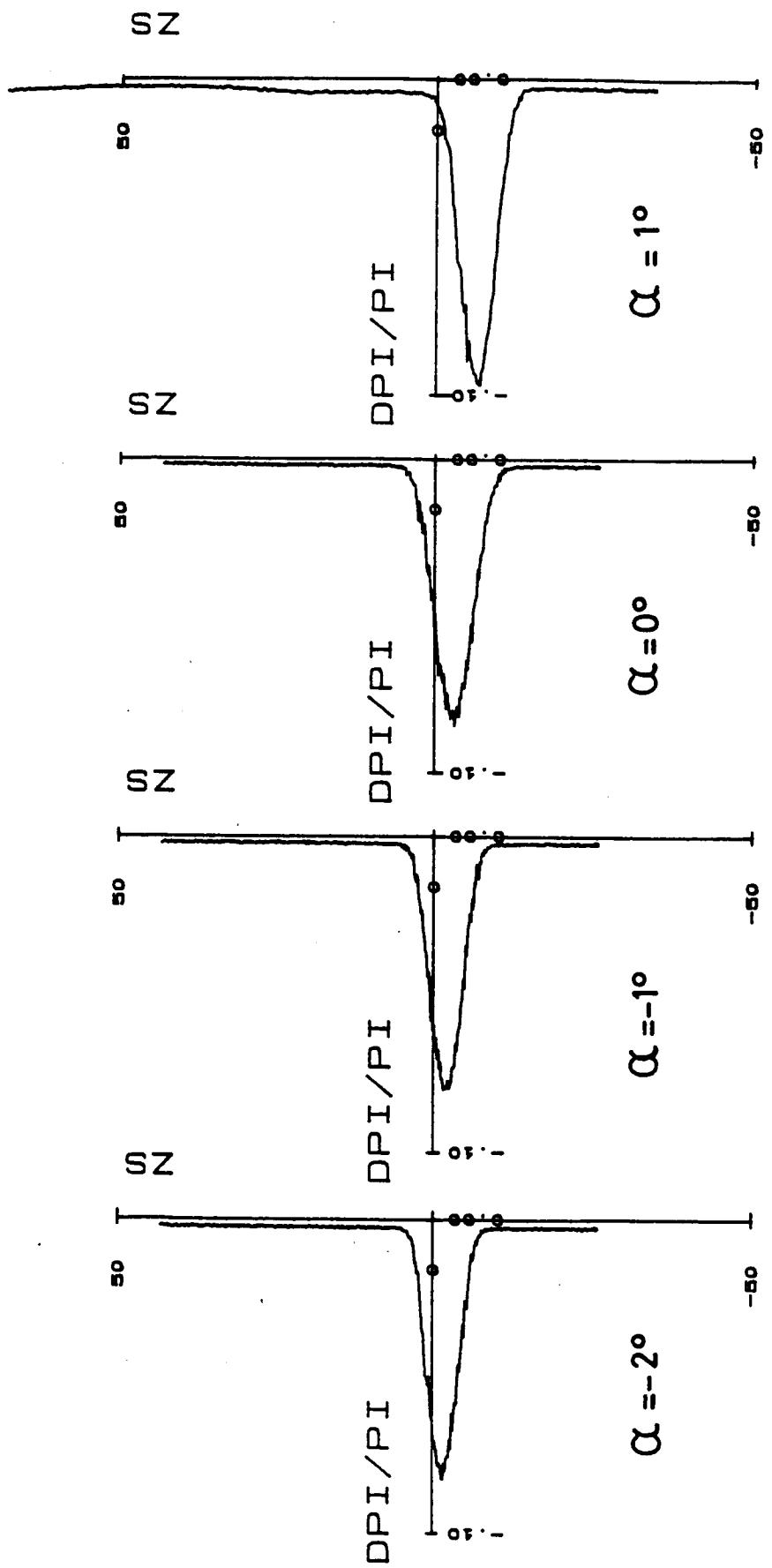




M_o = 0,7 R_c = 4 x 10⁶ T. 1/2 D.

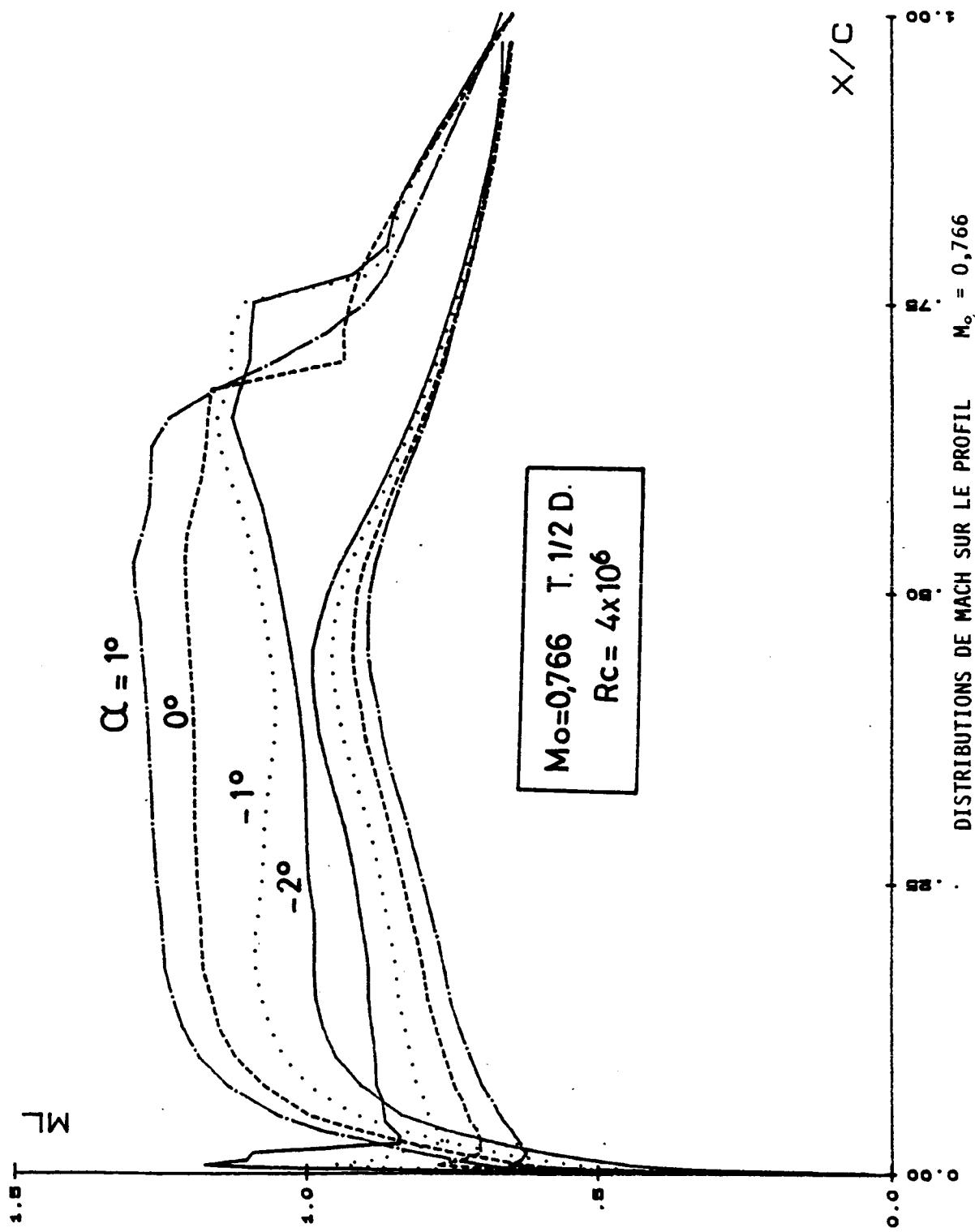
SONDAGES DES SILLAGES M_o = 0,7

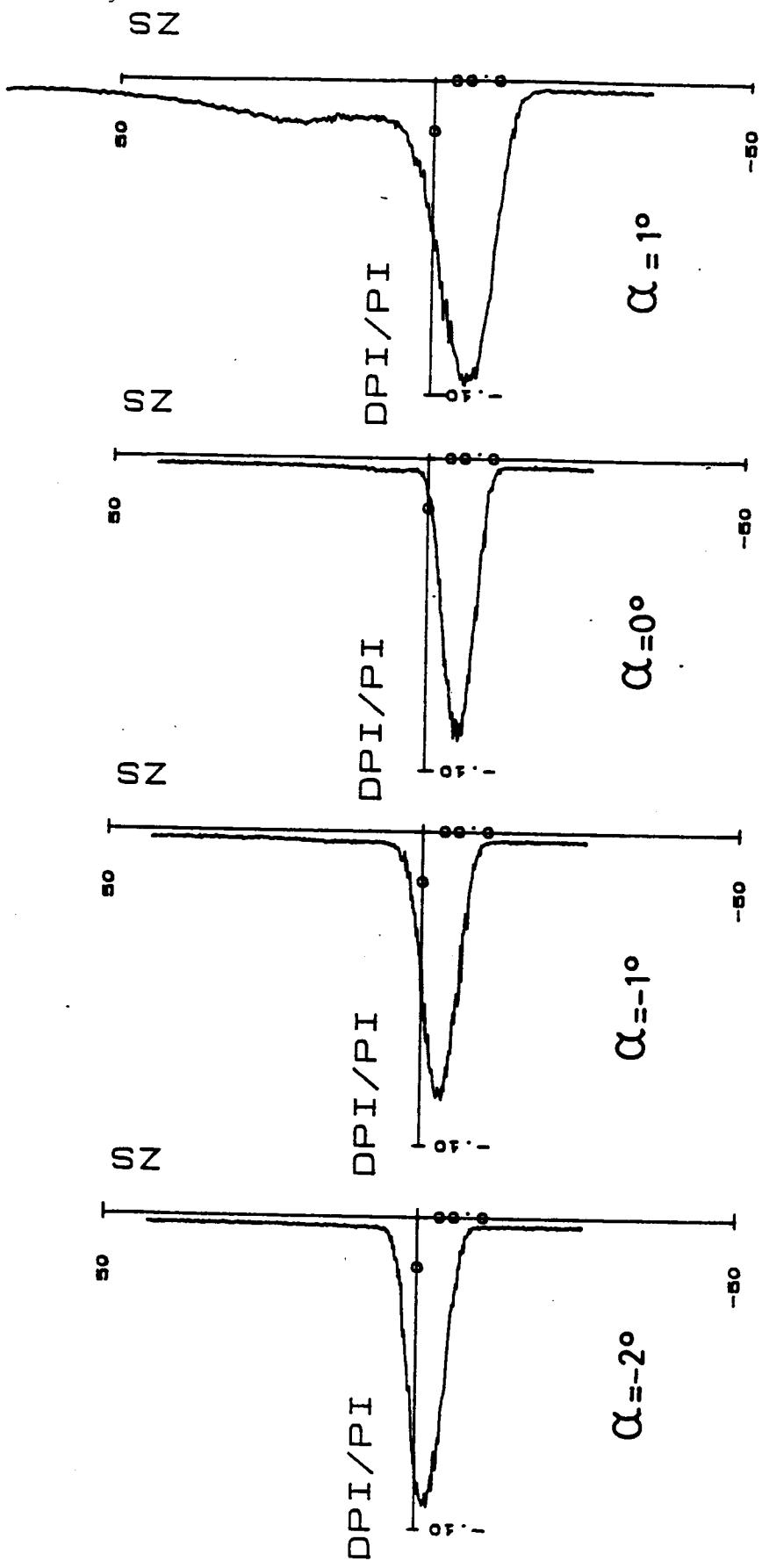




$M_o = 0.73$ $R_c = 4 \times 10^6$ $T. 1/2 D.$

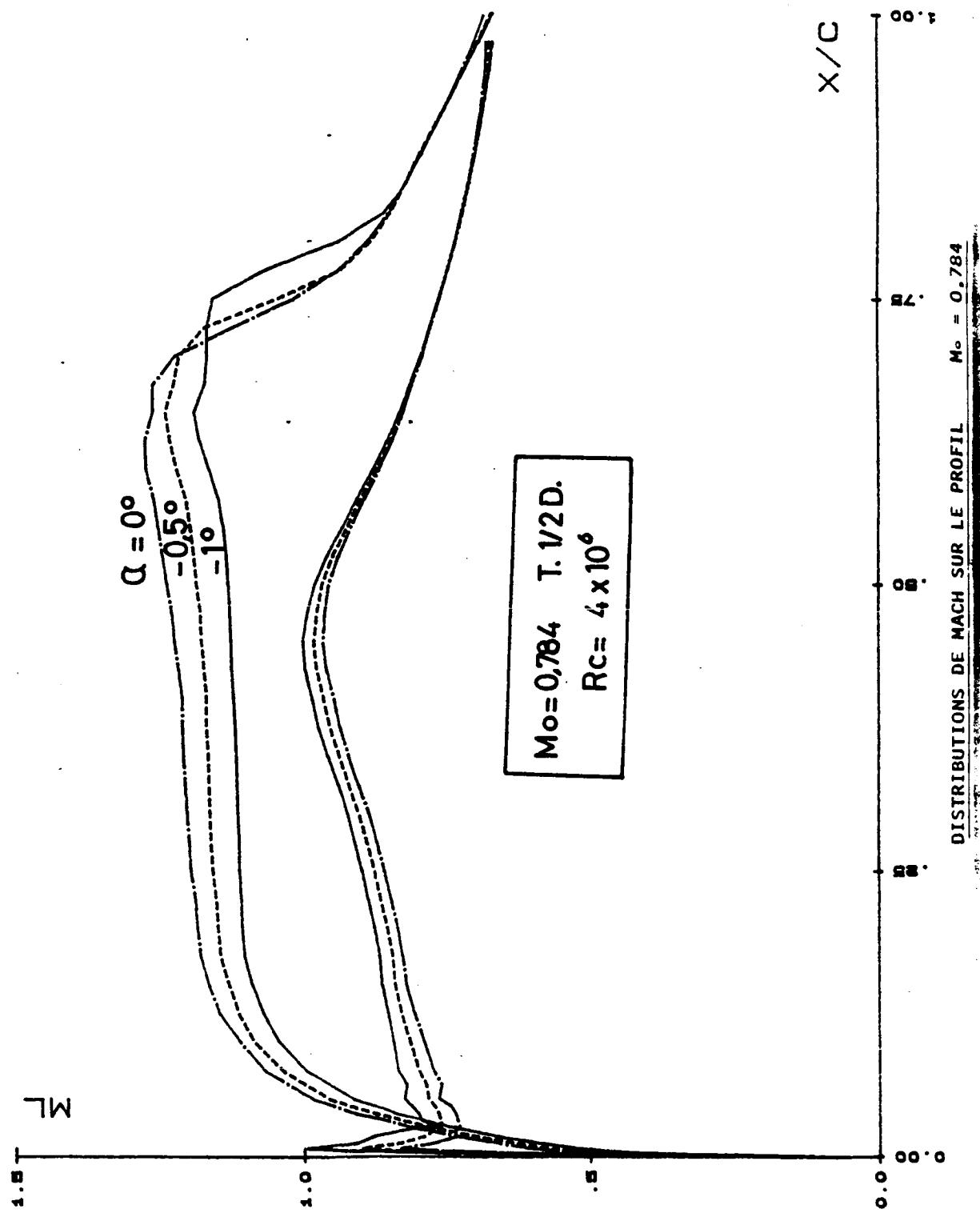
SONDAGES DES SILLAGES $M_o = 0.73$



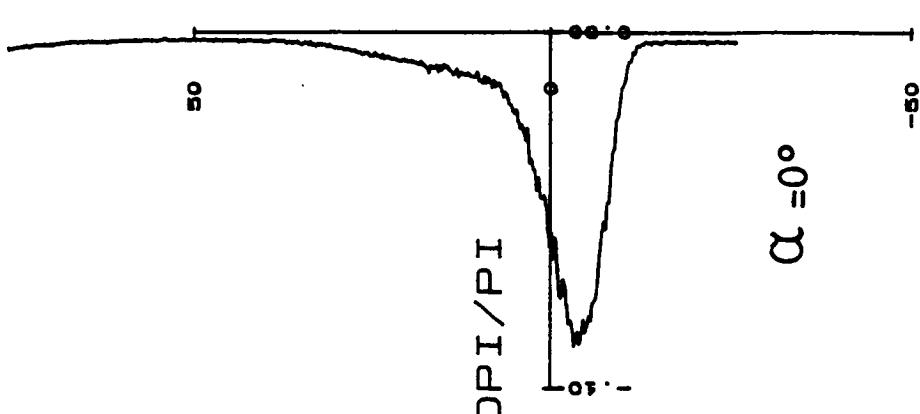


Mo=0,766 $Rc=4 \times 10^6$ T. 1/2. D.

SONDAGES DES SILLAGES $M_o = 0,766$

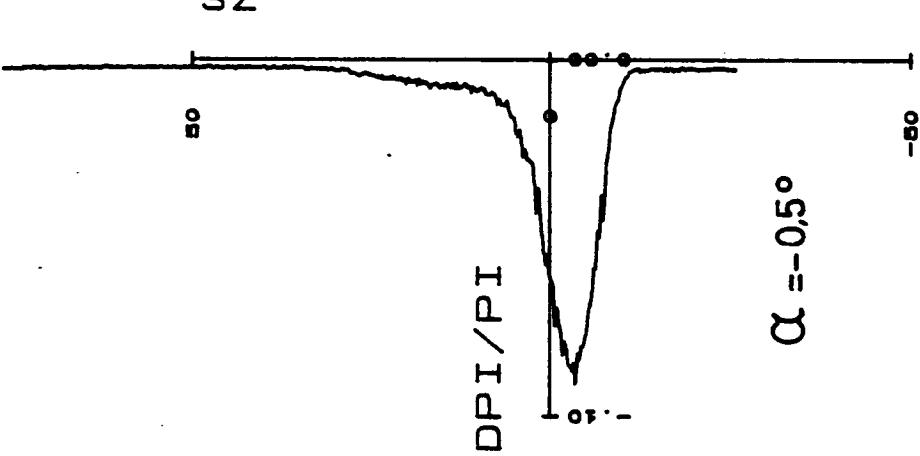


S Z



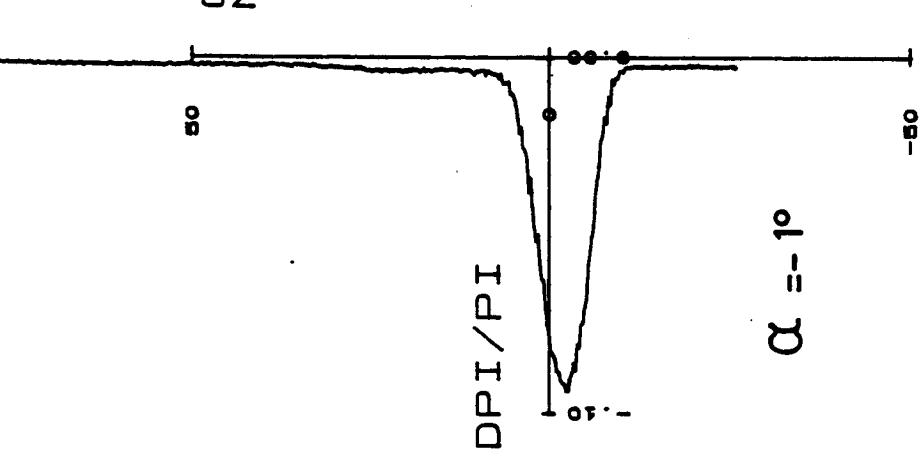
$$\alpha = 0^\circ$$

S Z



$$\alpha = -0.5^\circ$$

S Z



$$\alpha = -1^\circ$$

$M_o = 0,784 \quad R_c = 4 \times 10^6 \quad T. 1/2 D.$

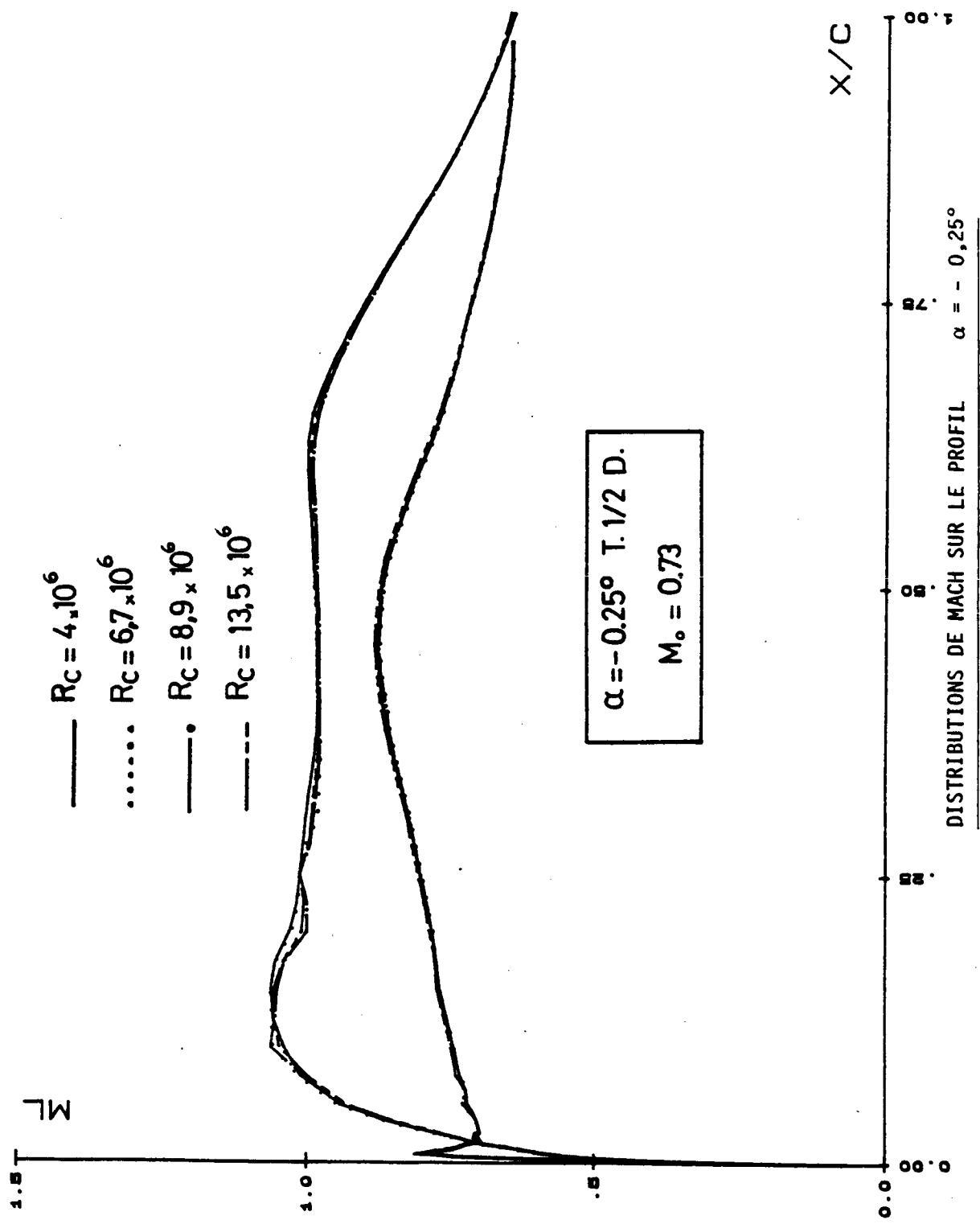
SONDAGES DES SILLAGES $M_o = 0,784$

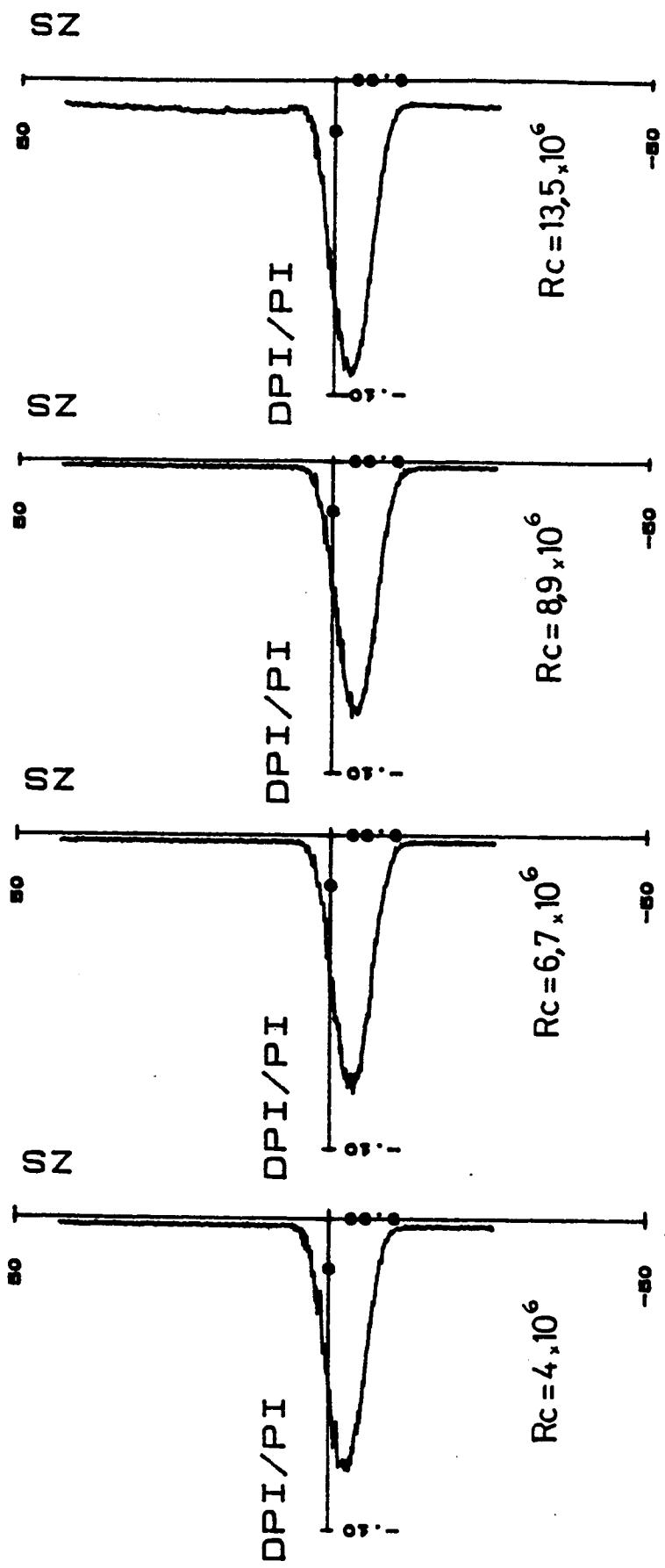
T. 1/2 D.

VARIATION DU NOMBRE DE REYNOLDS

$M_\infty = 0,73$ et $\alpha = -0,25^\circ$ PL. 37 et 38

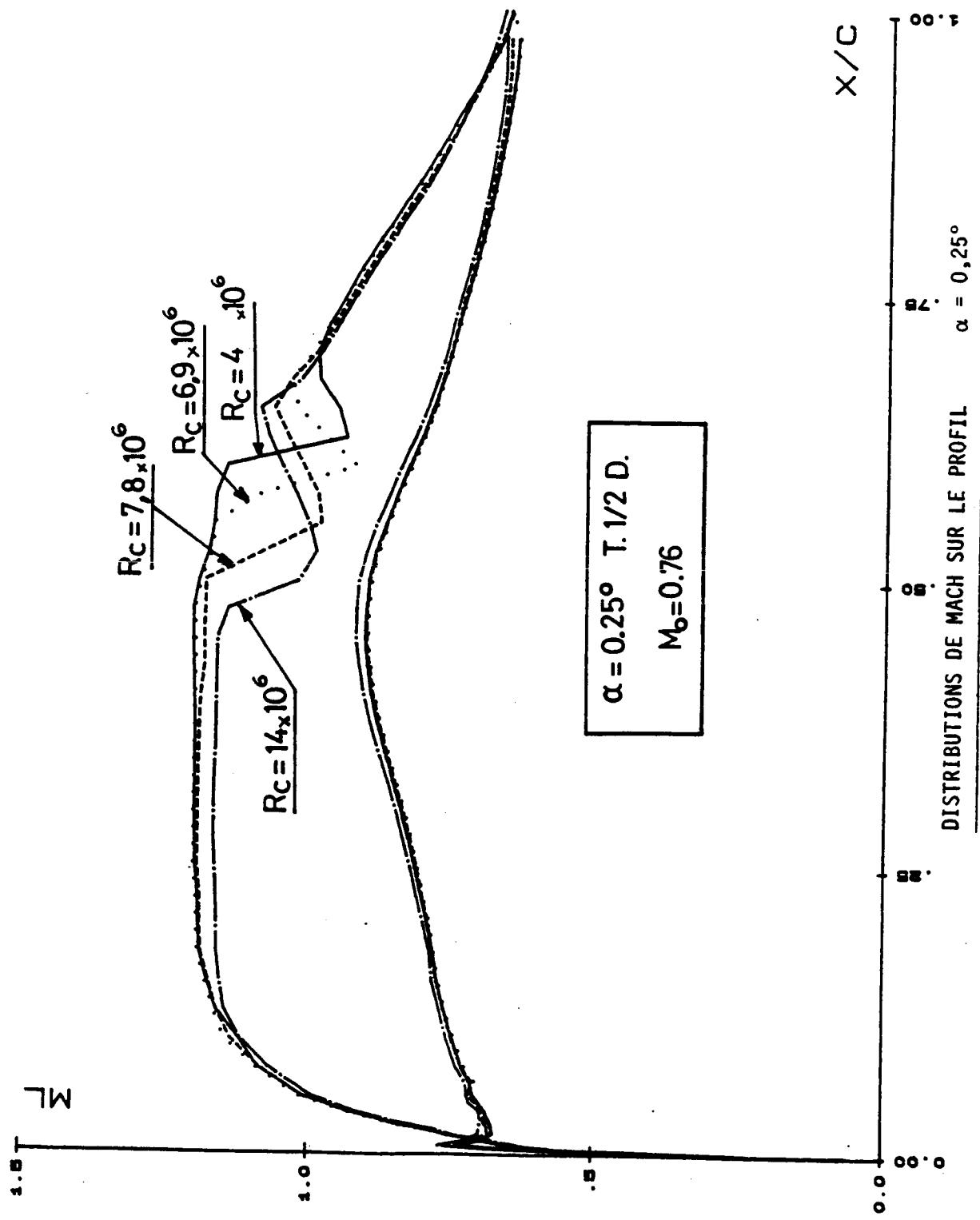
$M_\infty = 0,76$ et $\alpha = +0,25^\circ$ PL. 39 et 40



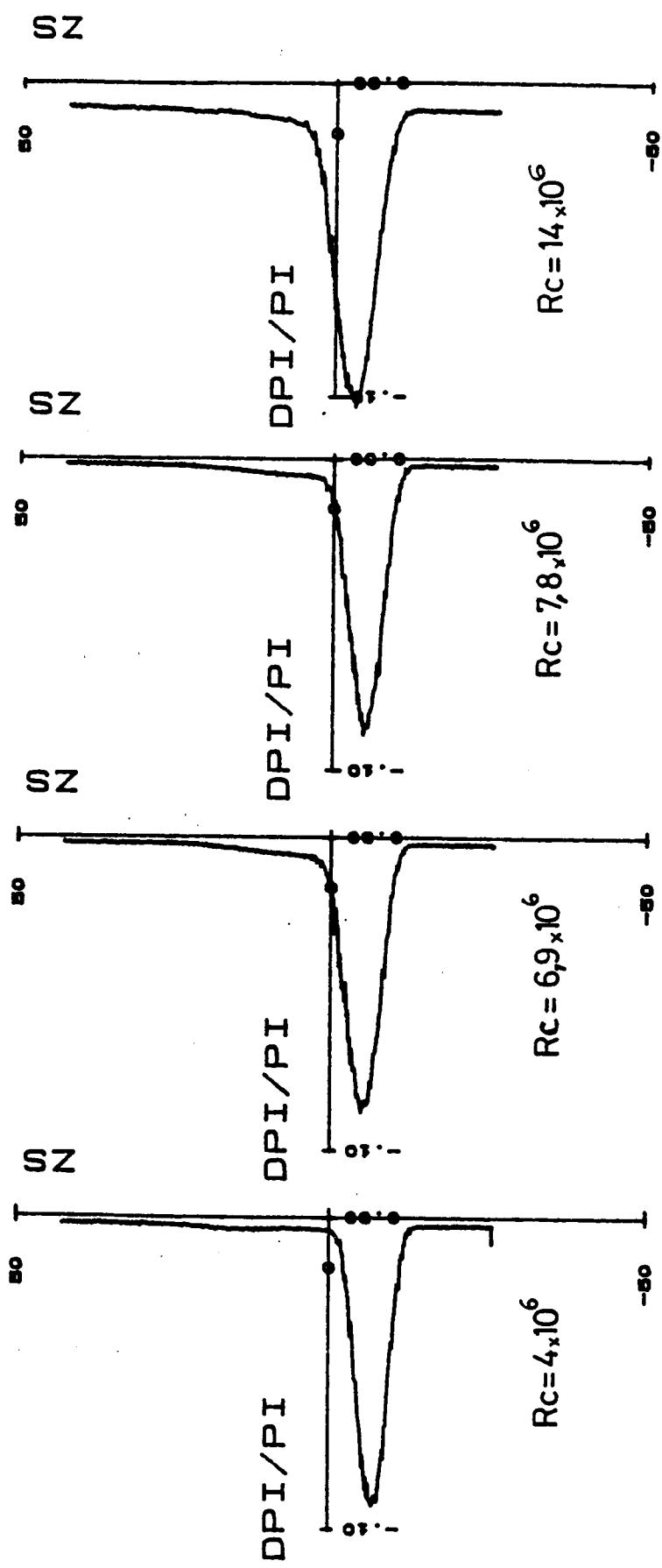


$\alpha = -0,25^\circ$ $M_o = 0,73$ T. 1/2 D.

SONDAGES DES SILLAGES $M_o = 0,73$



PL. 40



$$\alpha = 0.25^\circ \quad M=0.76 \quad T. 1/2 D.$$

SONDAGES DES SILLAGES $M = 0.76$

T. 1/2 D.

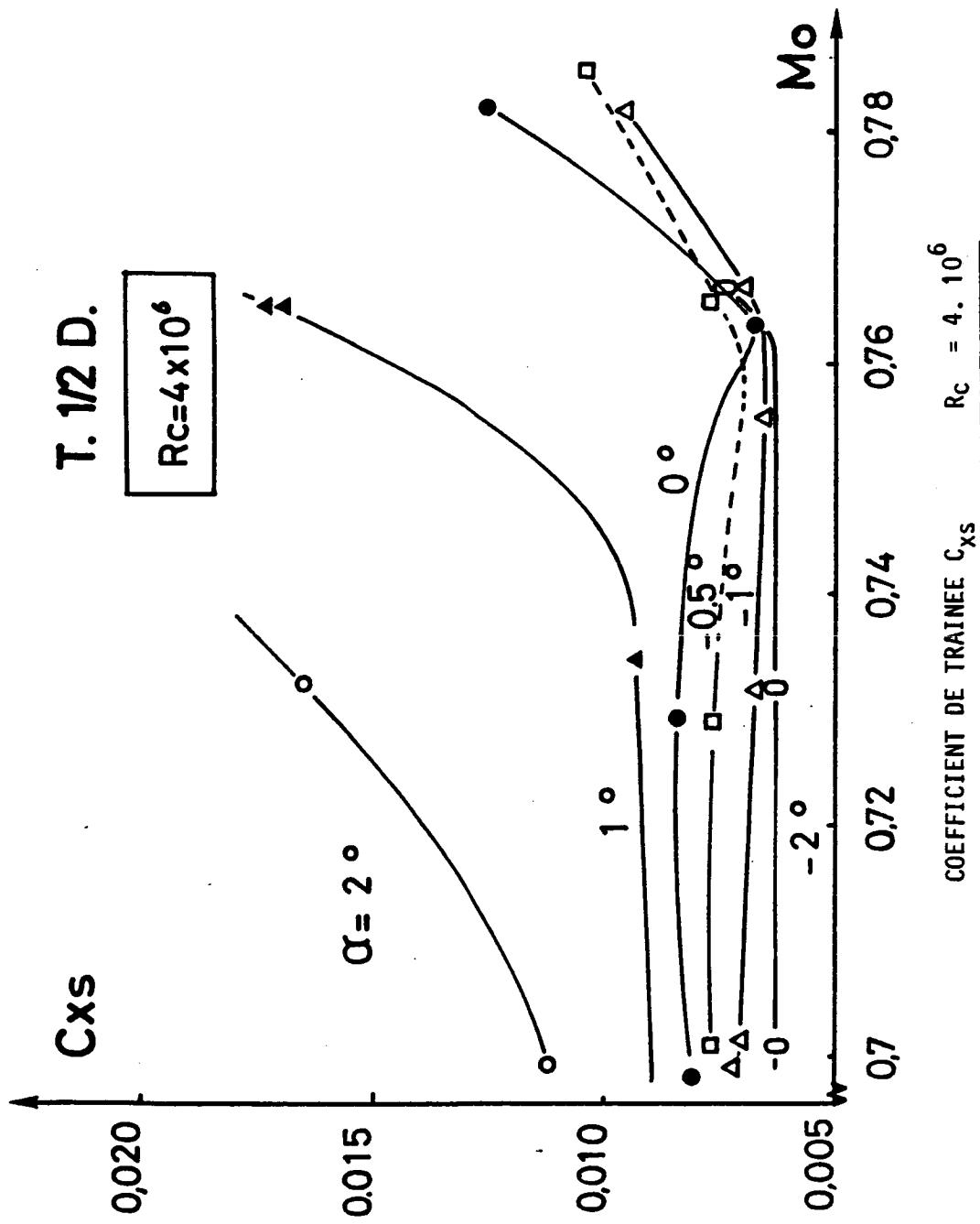
COEFFICIENTS AERODYNAMIQUES EN FONCTION DU NOMBRE DE MACH

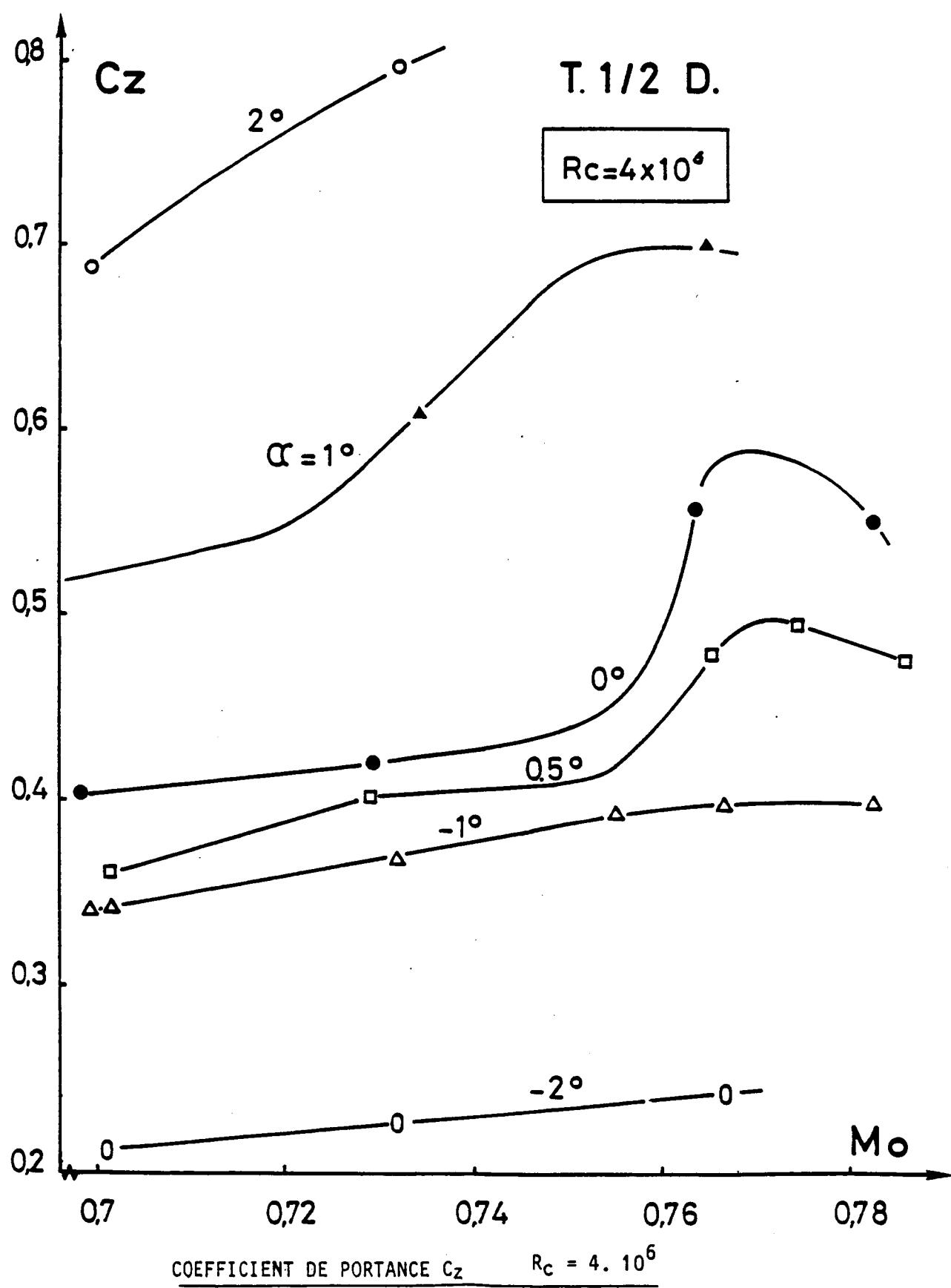
$$R_C = 4 \cdot 10^6$$

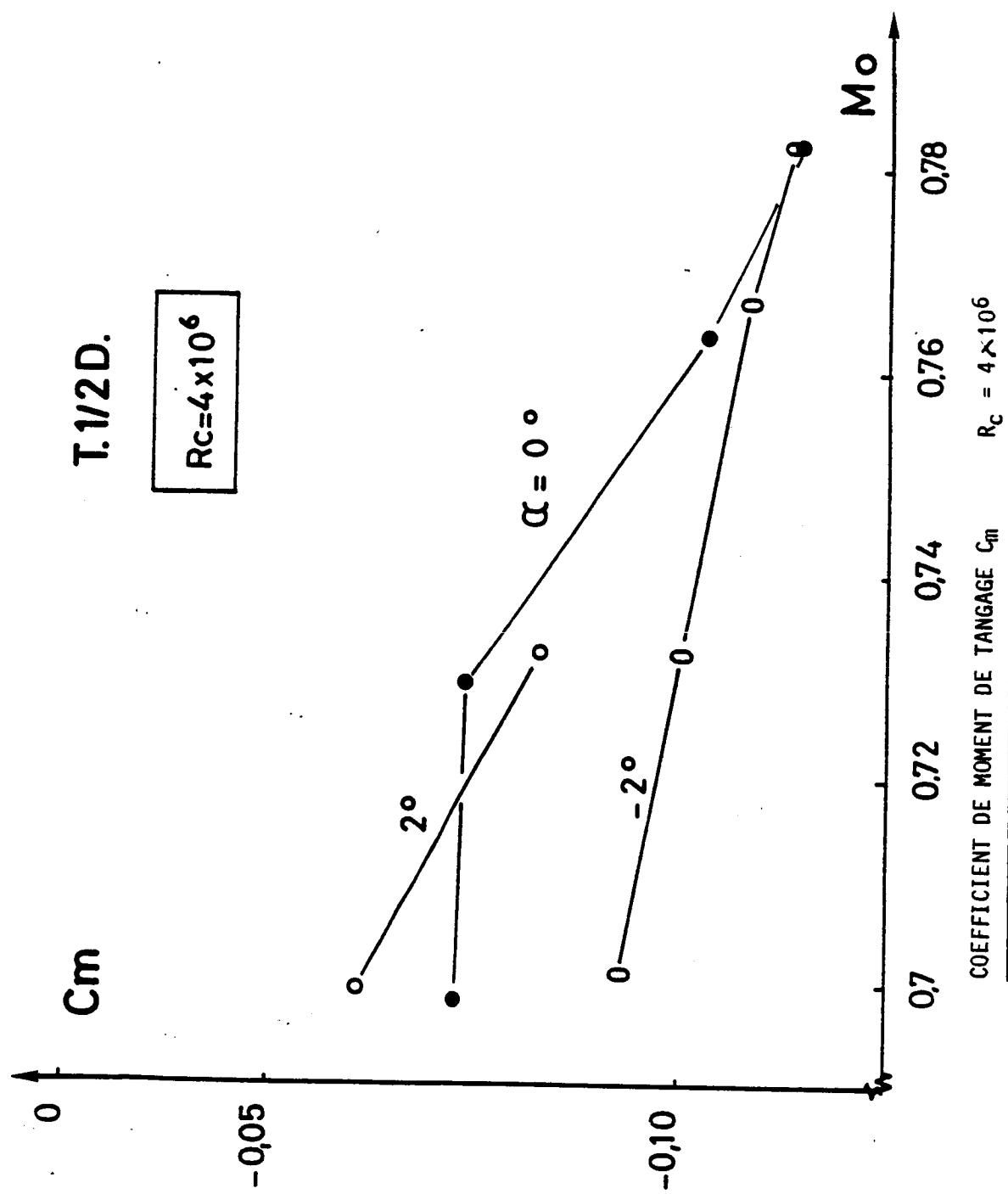
C_{xs} (M_0) PL. 41

C_z (M_0) PL. 42

C_m (M_δ) PL. 43





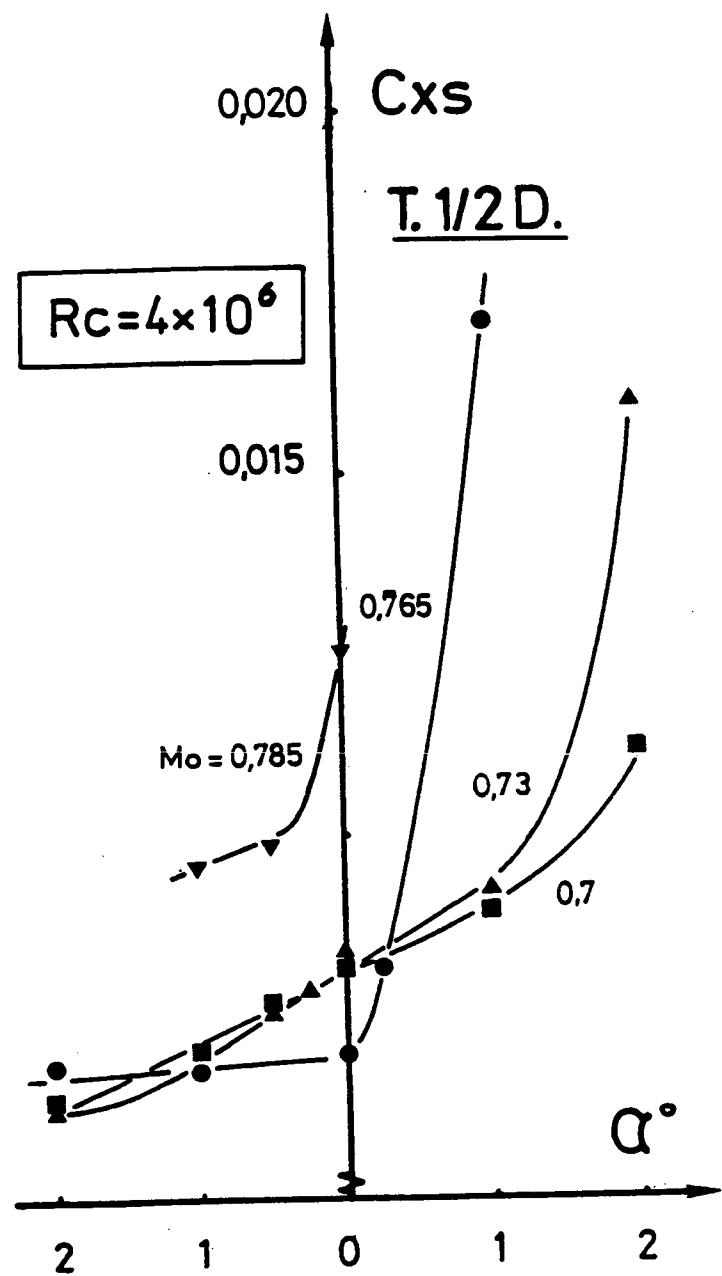


T. 1/2 D.

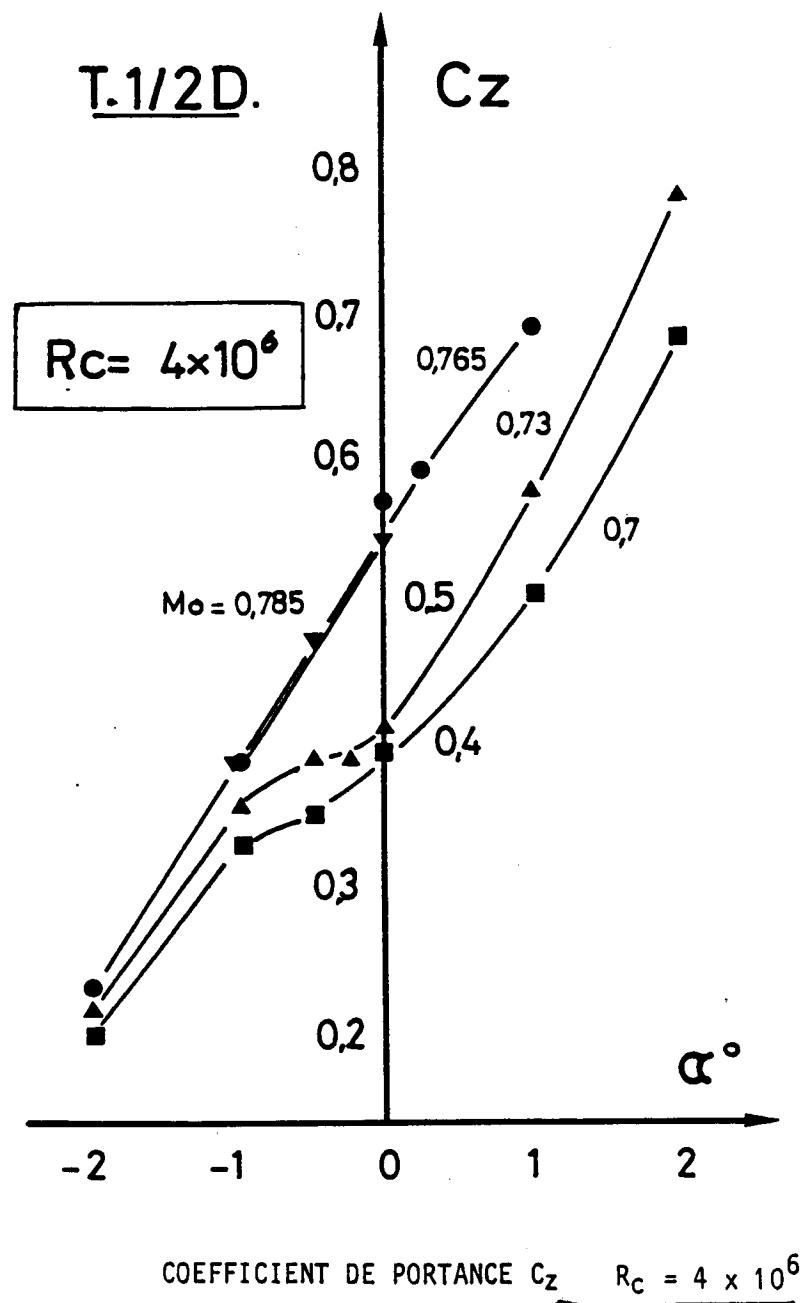
COEFFICIENTS AERODYNAMIQUE EN FONCTION DE L'INCIDENCE

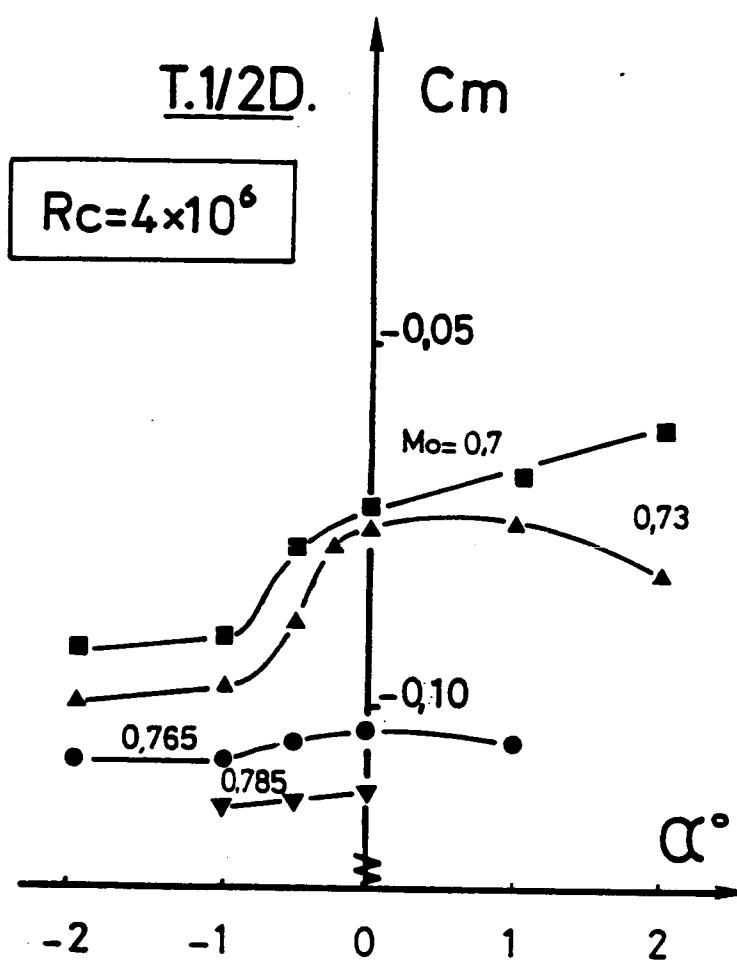
$$R_C = 4 \cdot 10^6$$

C_{xs}	(α)	PL. 44
C_z	(α)	PL. 45
C_m	(α)	PL. 46
Polaire C_z	(C_x)	PL. 47

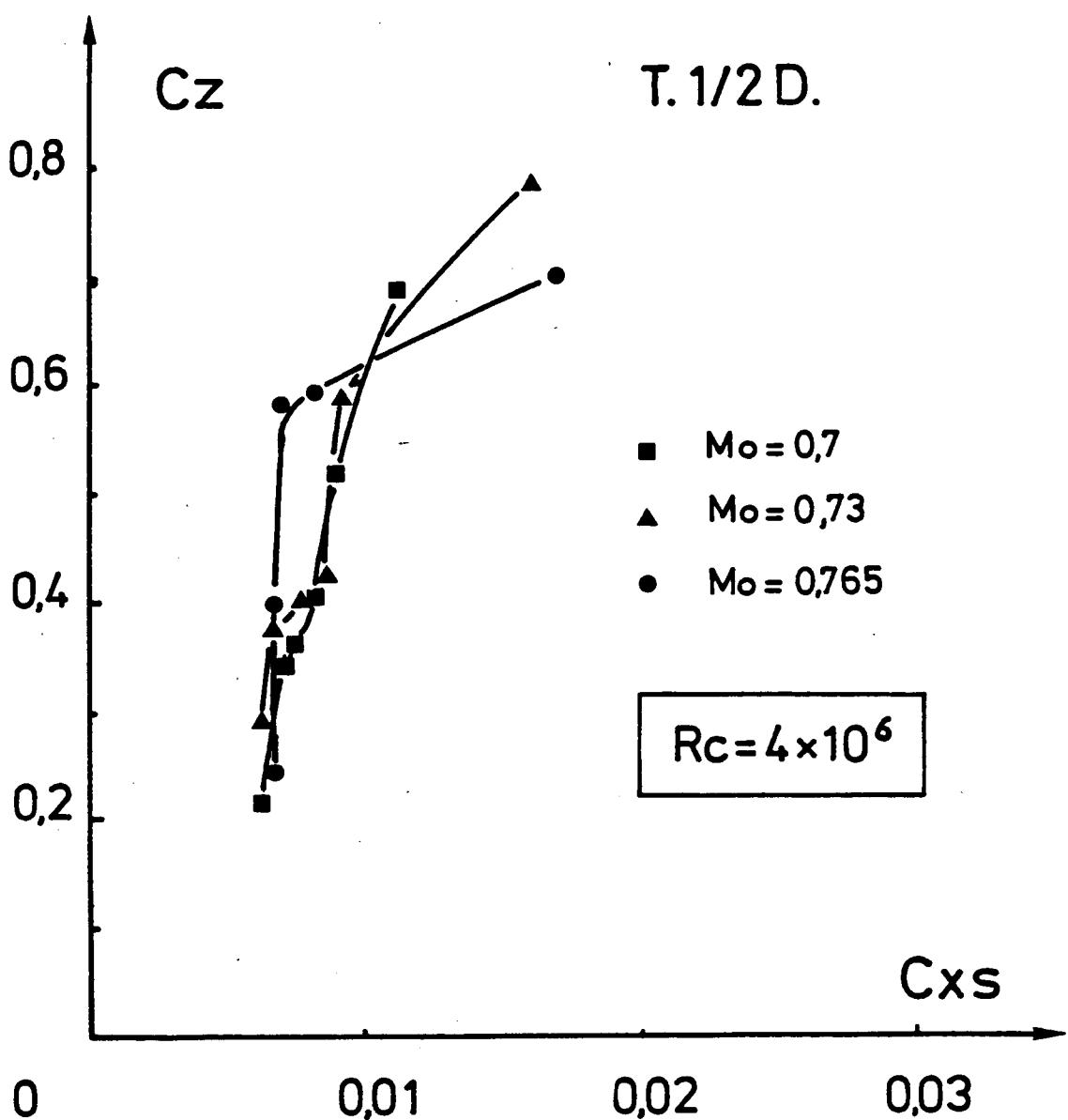


COEFFICIENT DE TRAINEE C_{xs} $R_c = 4 \times 10^6$





COEFFICIENT DE MOMENT DE TANGAGE C_m $R_c = 4 \times 10^6$

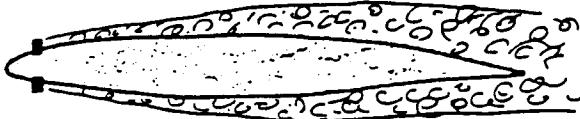


POLAIRE C_z (C_x) $R_c = 4 \times 10^6$

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ESSAIS EN TRANSITION DECLENCHEE

T.D.



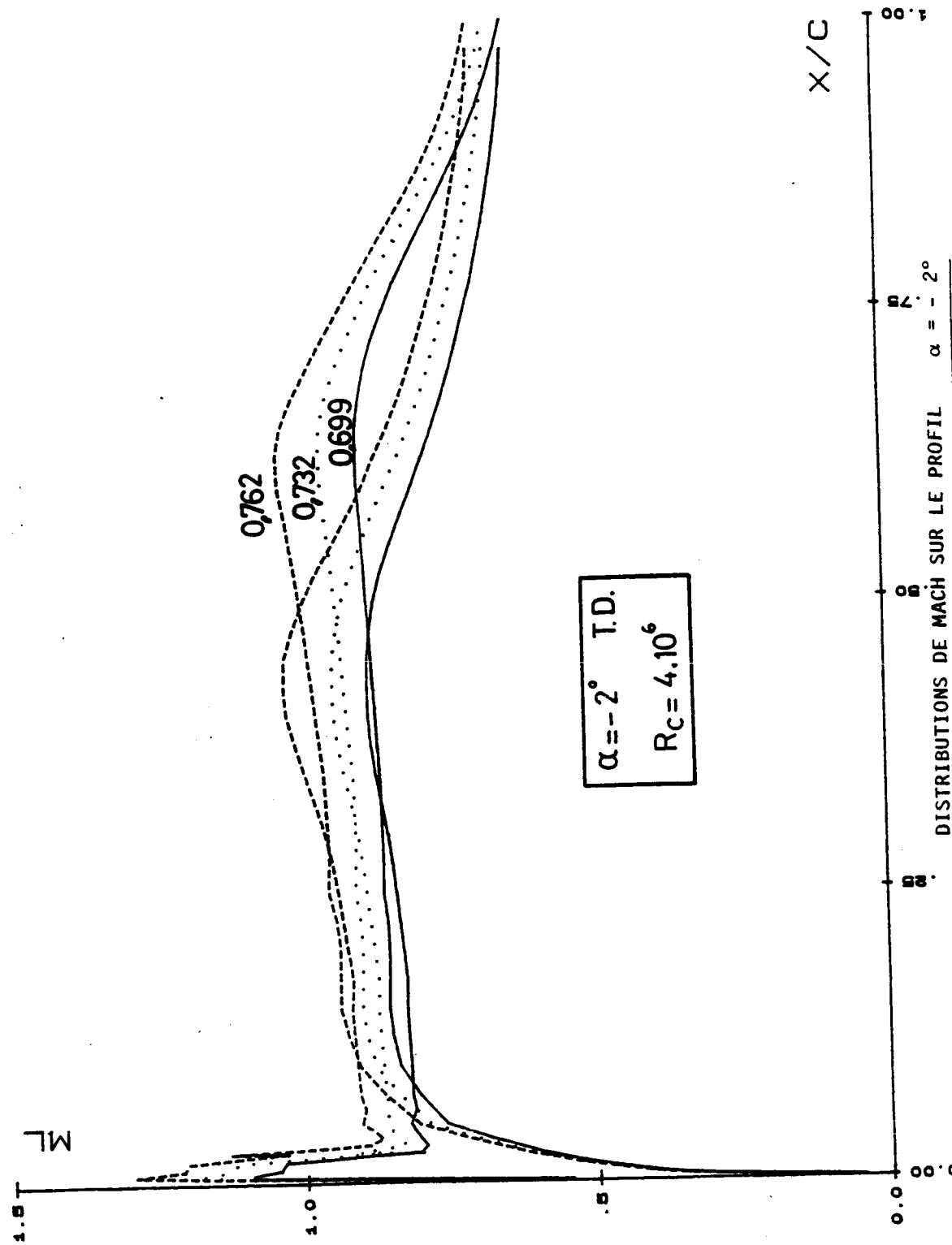
PLANCHES 48 à 92

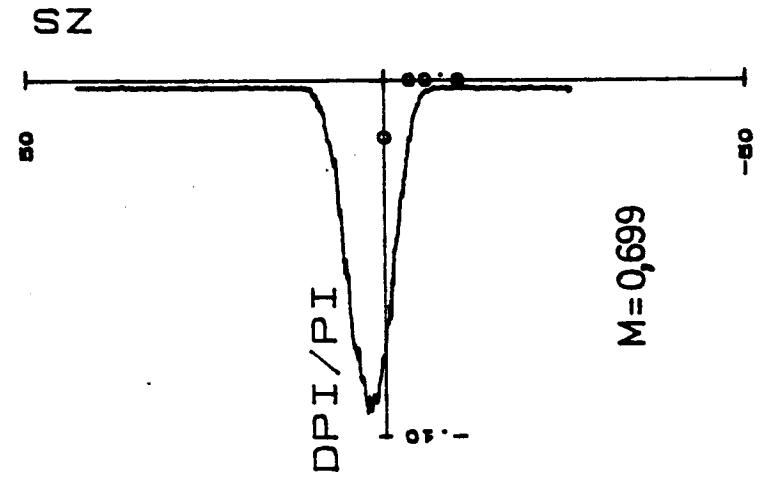
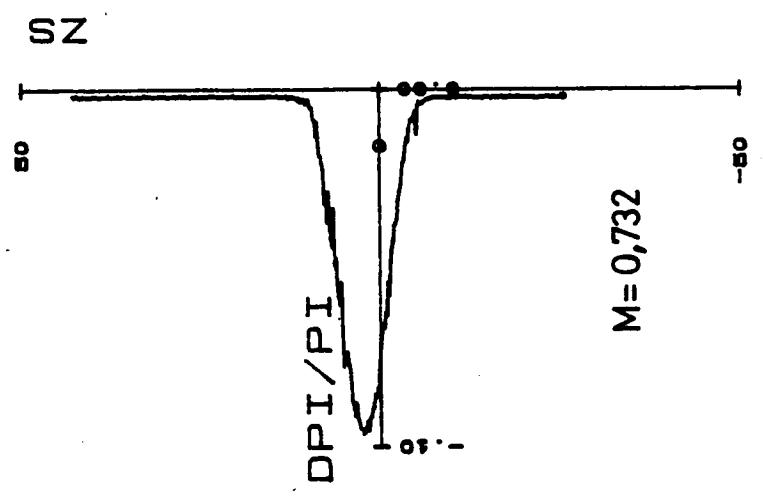
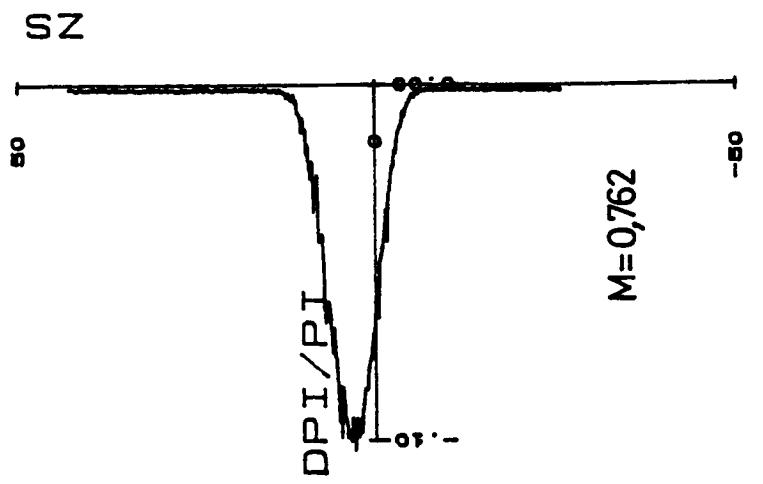
T.D.

VARIATION DU NOMBRE DE MACH

$$R_C = 4 \cdot 10^6$$

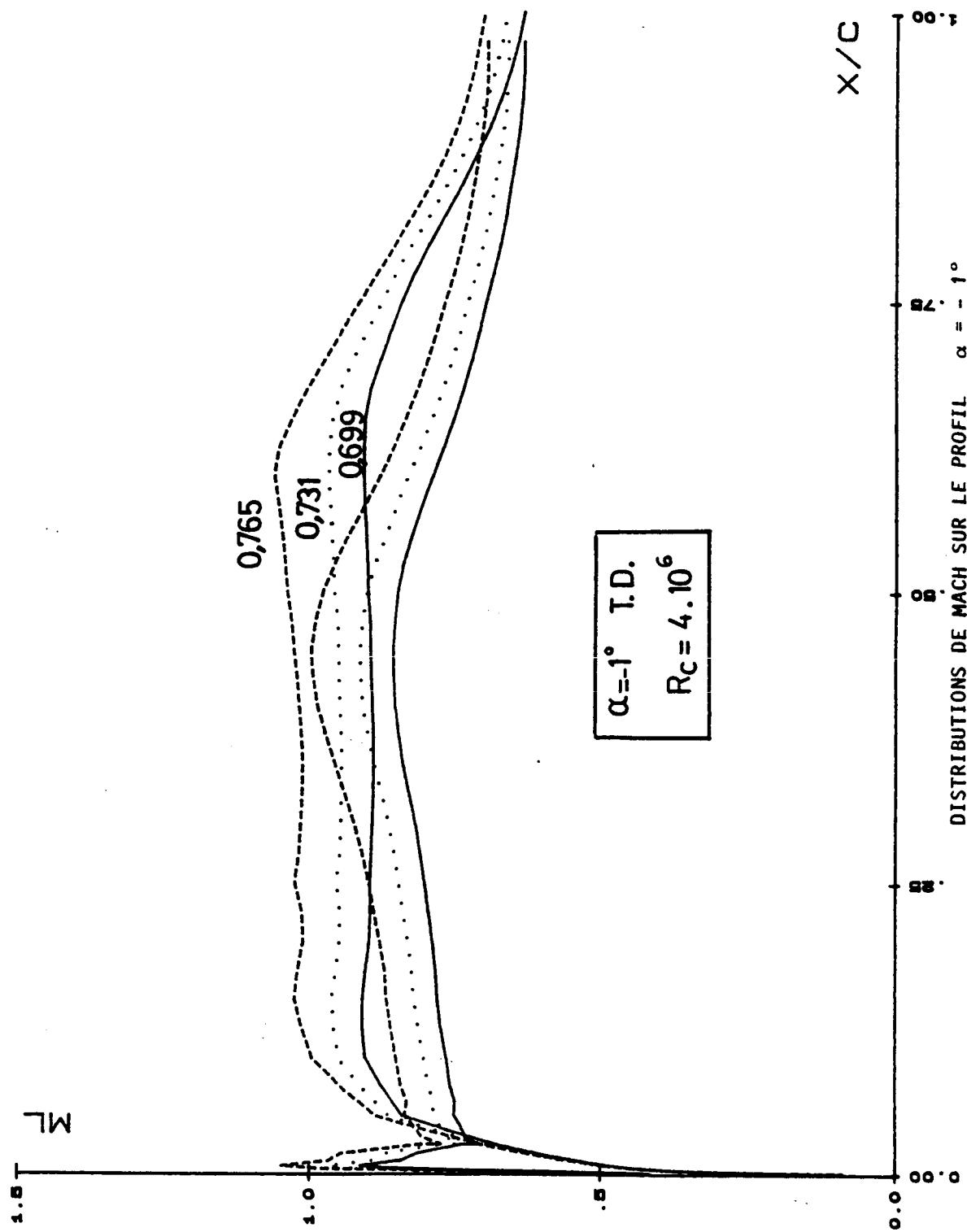
$\alpha = - 2^\circ$	PL. 48 et 49
$\alpha = - 1^\circ$	PL. 50 et 51
$\alpha = 0^\circ$	PL. 52 et 53
$\alpha = + 0,25^\circ$	PL. 54 et 55
$\alpha = + 1^\circ$	PL. 56 et 57
$\alpha = + 2^\circ$	PL. 58 et 59
$\alpha = + 3^\circ$	PL. 60 et 61
$\alpha = + 4^\circ$	PL. 62 et 63

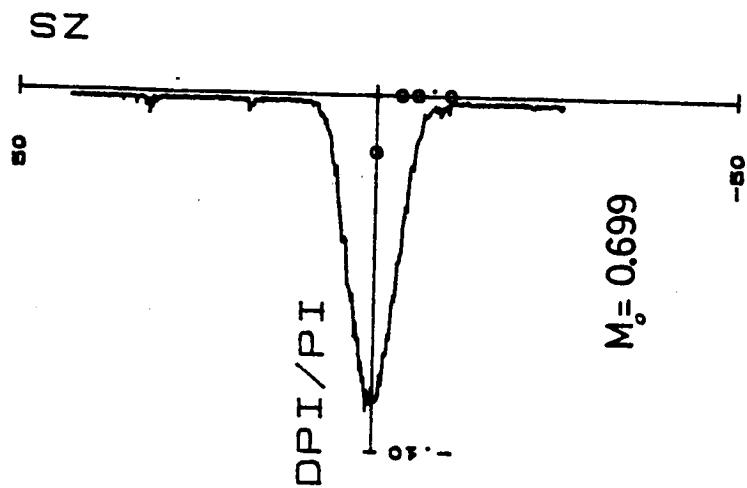
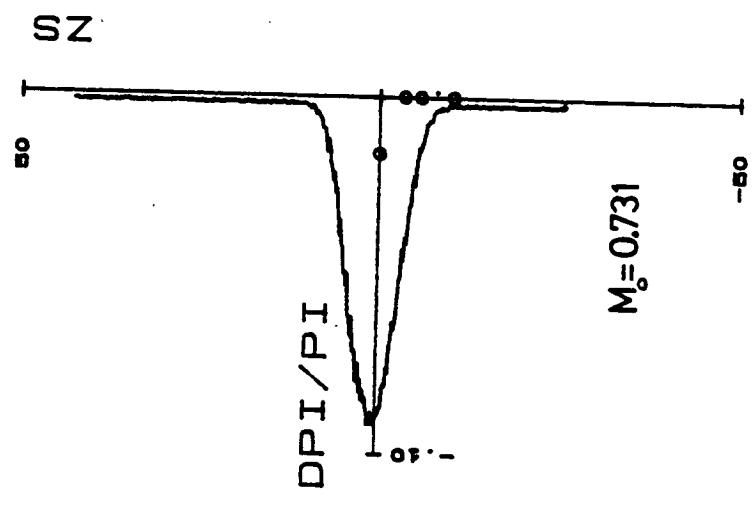
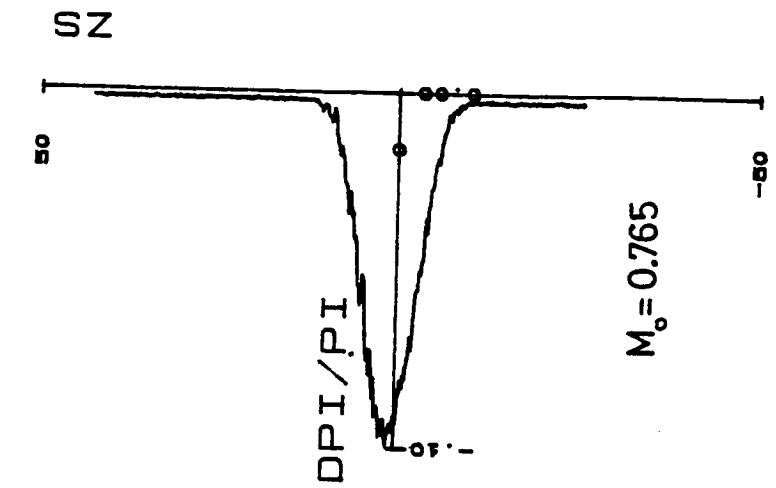




$\alpha = -2^\circ \quad R_c = 4 \cdot 10^6 \quad T.D.$

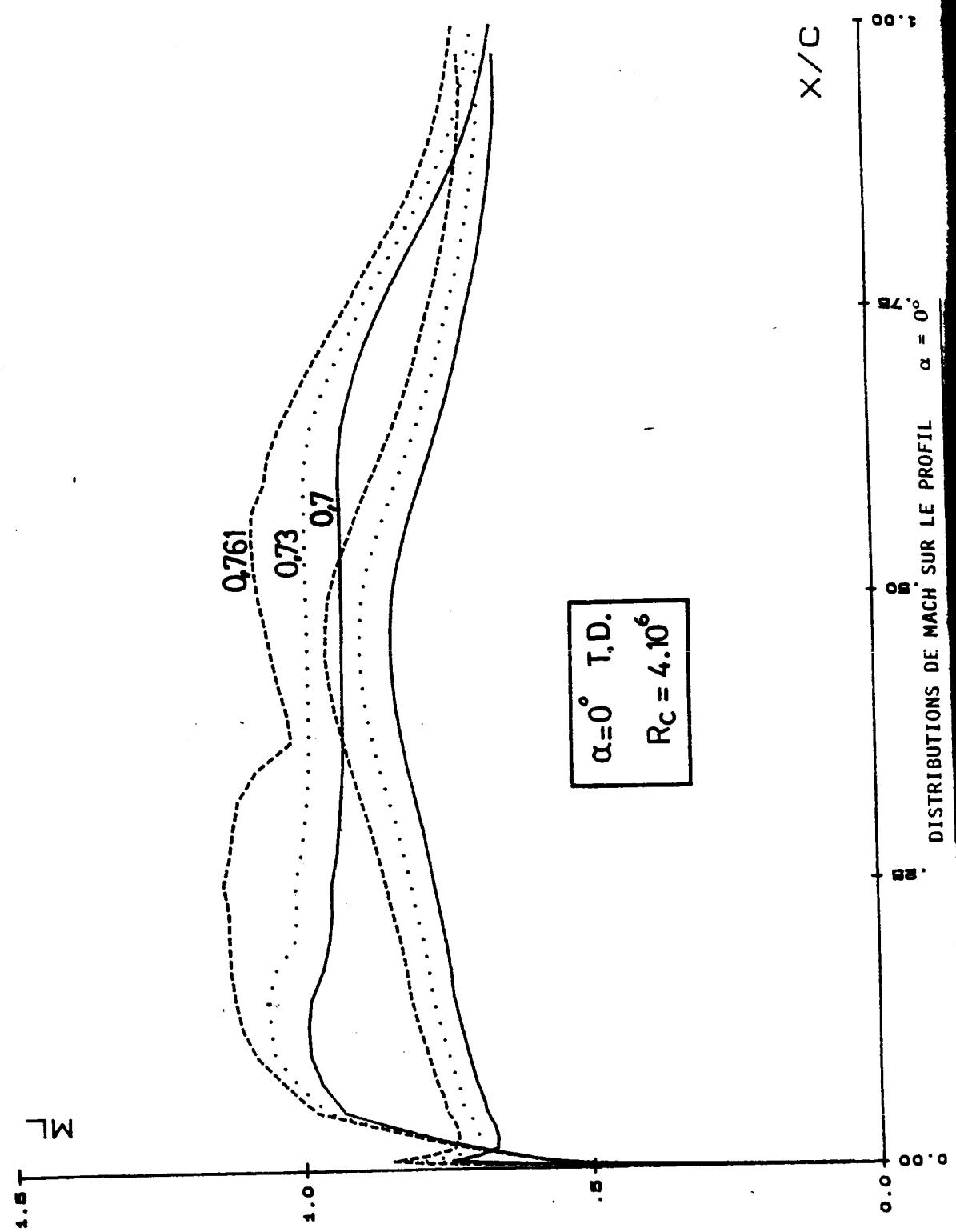
SONDAGES DES SILLAGES $\alpha = -2^\circ$

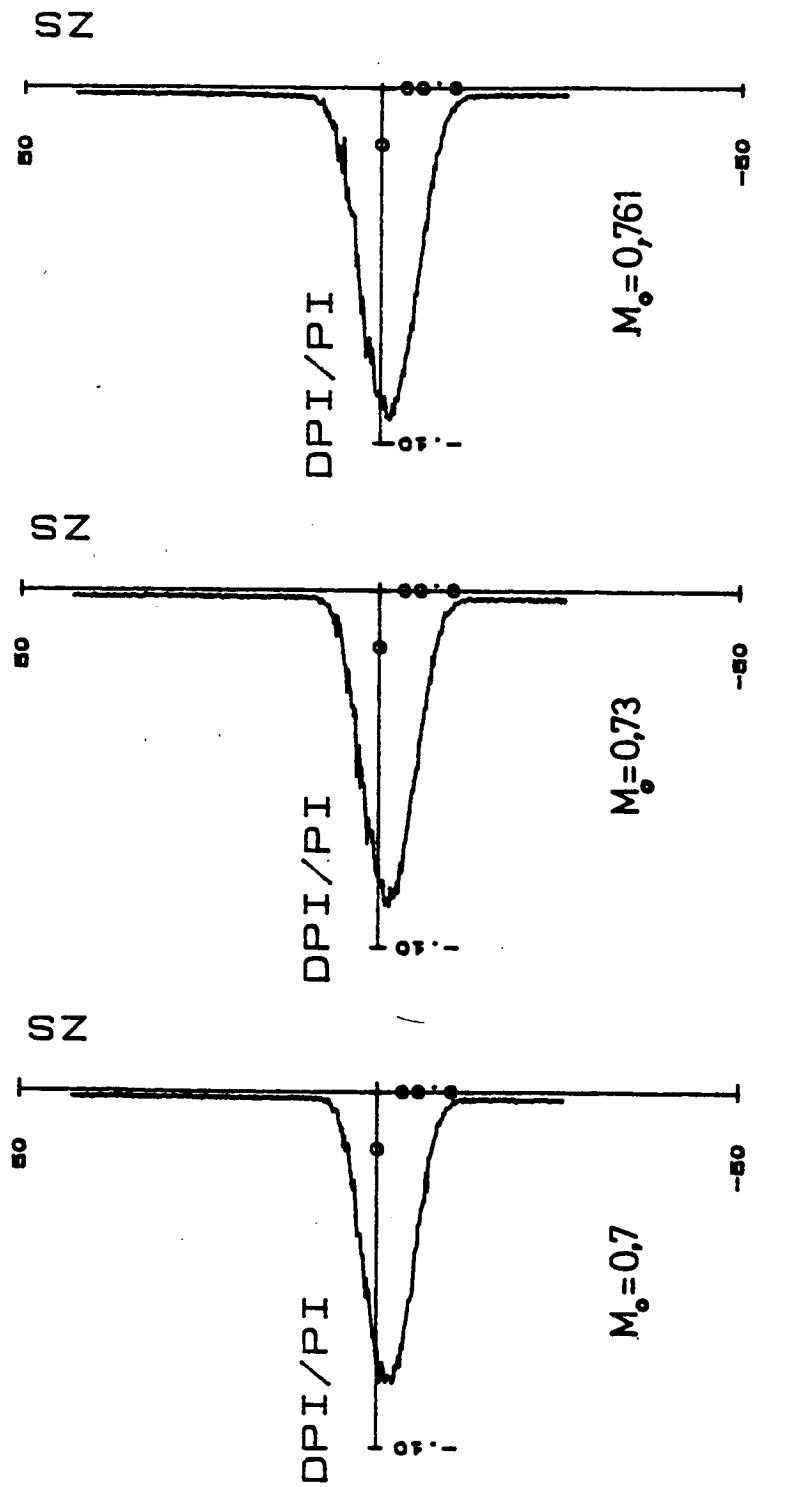




$\alpha = -1^\circ \quad R_c = 4 \cdot 10^6 \quad T.D.$

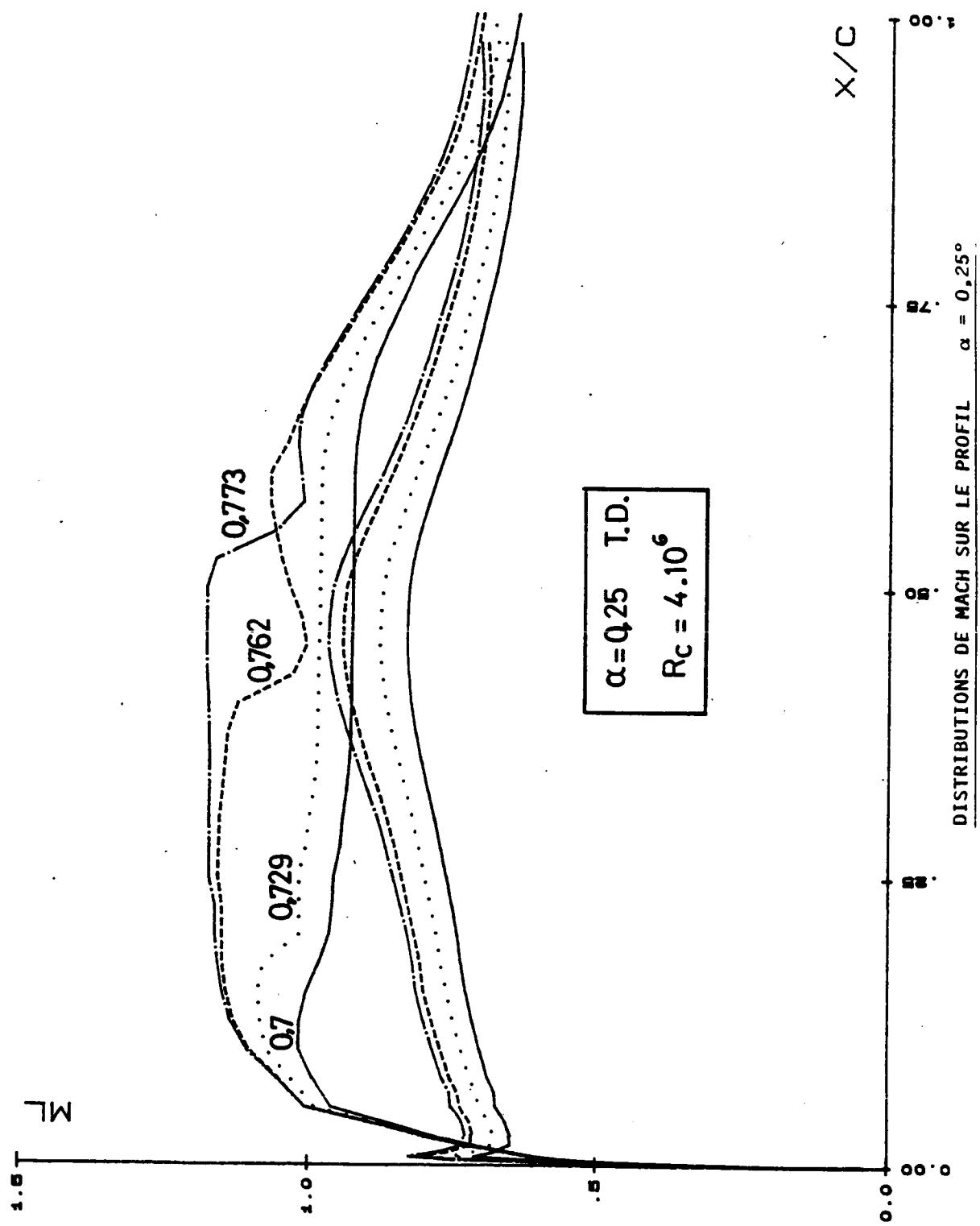
SONDAGES DES SILLAGES $\alpha = -1^\circ$

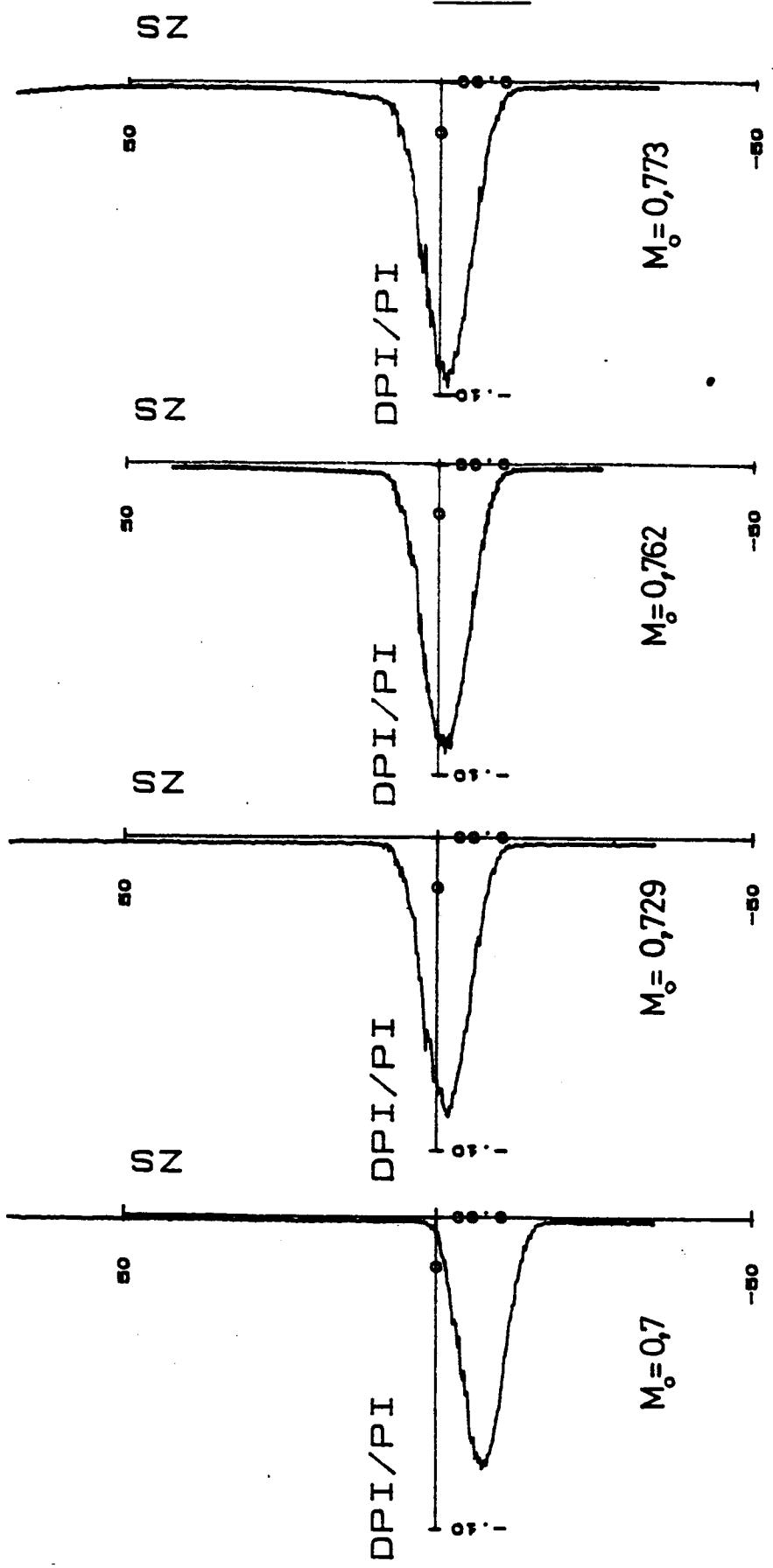




$\alpha = 0^\circ \quad R_c = 4.10^6 \quad T.D.$

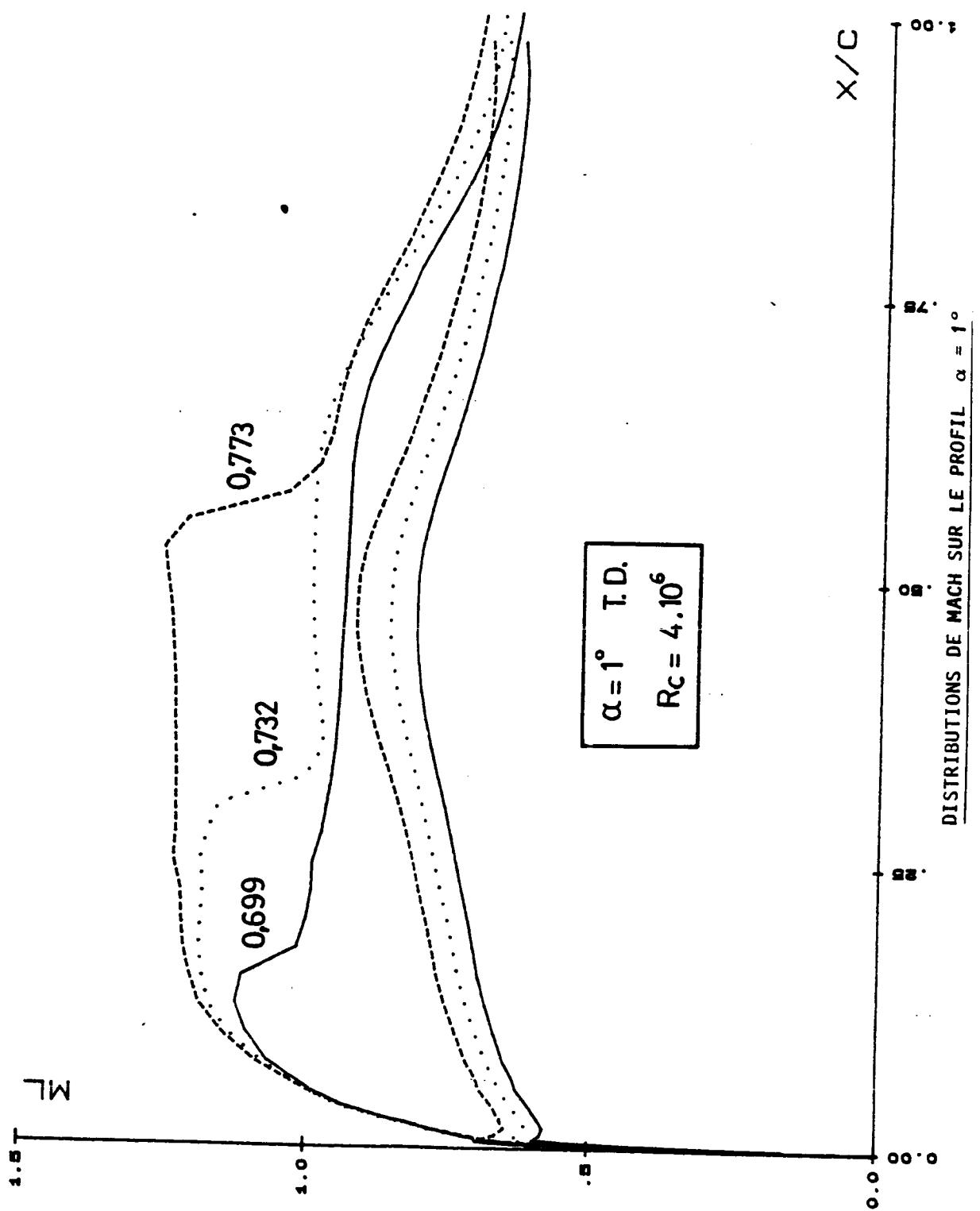
SONDAGES DES SILLAGES $\alpha = 0^\circ$

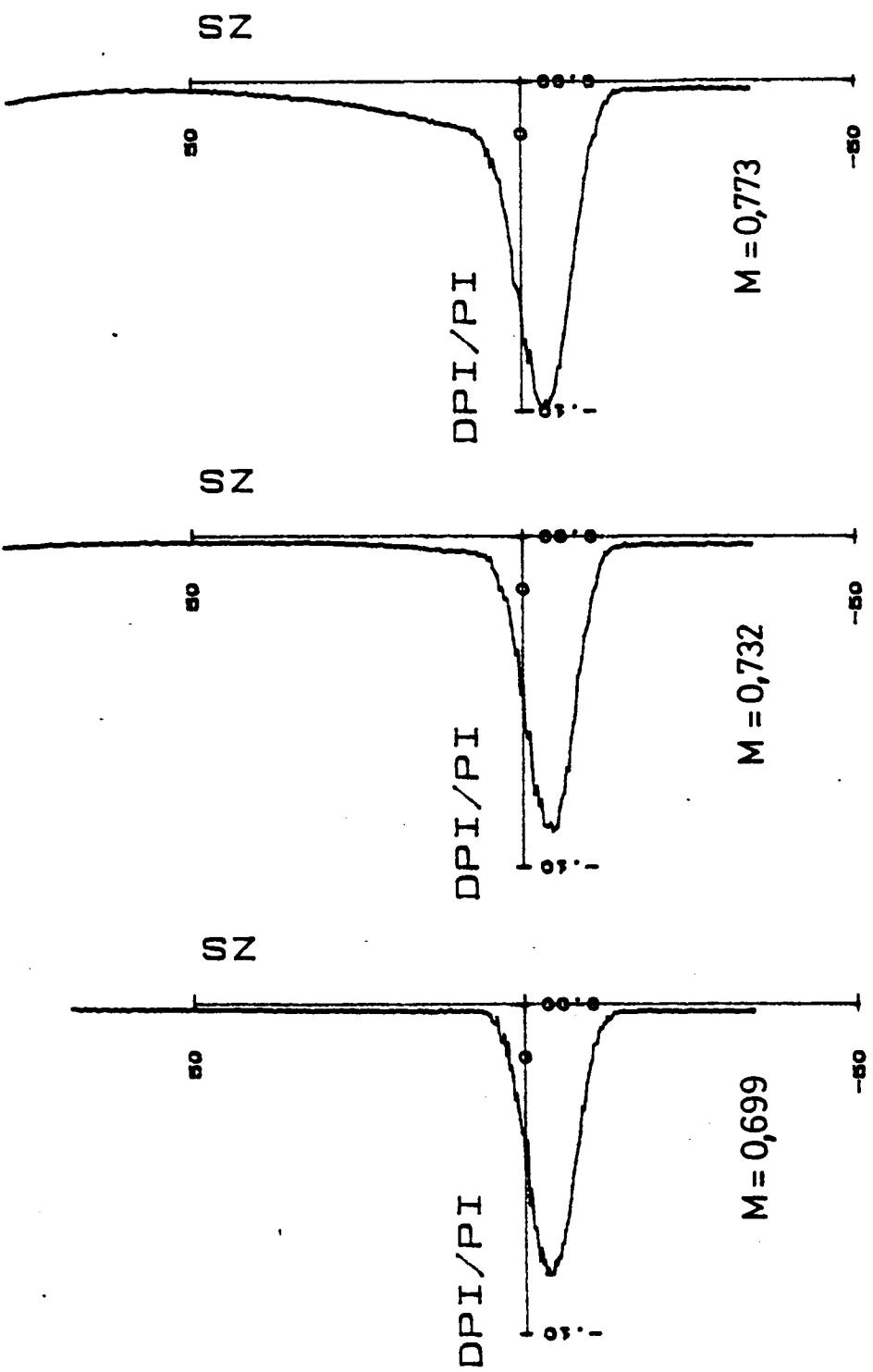




$$\alpha = 0,25^\circ \quad R_c = 4 \cdot 10^6 \quad T.D.$$

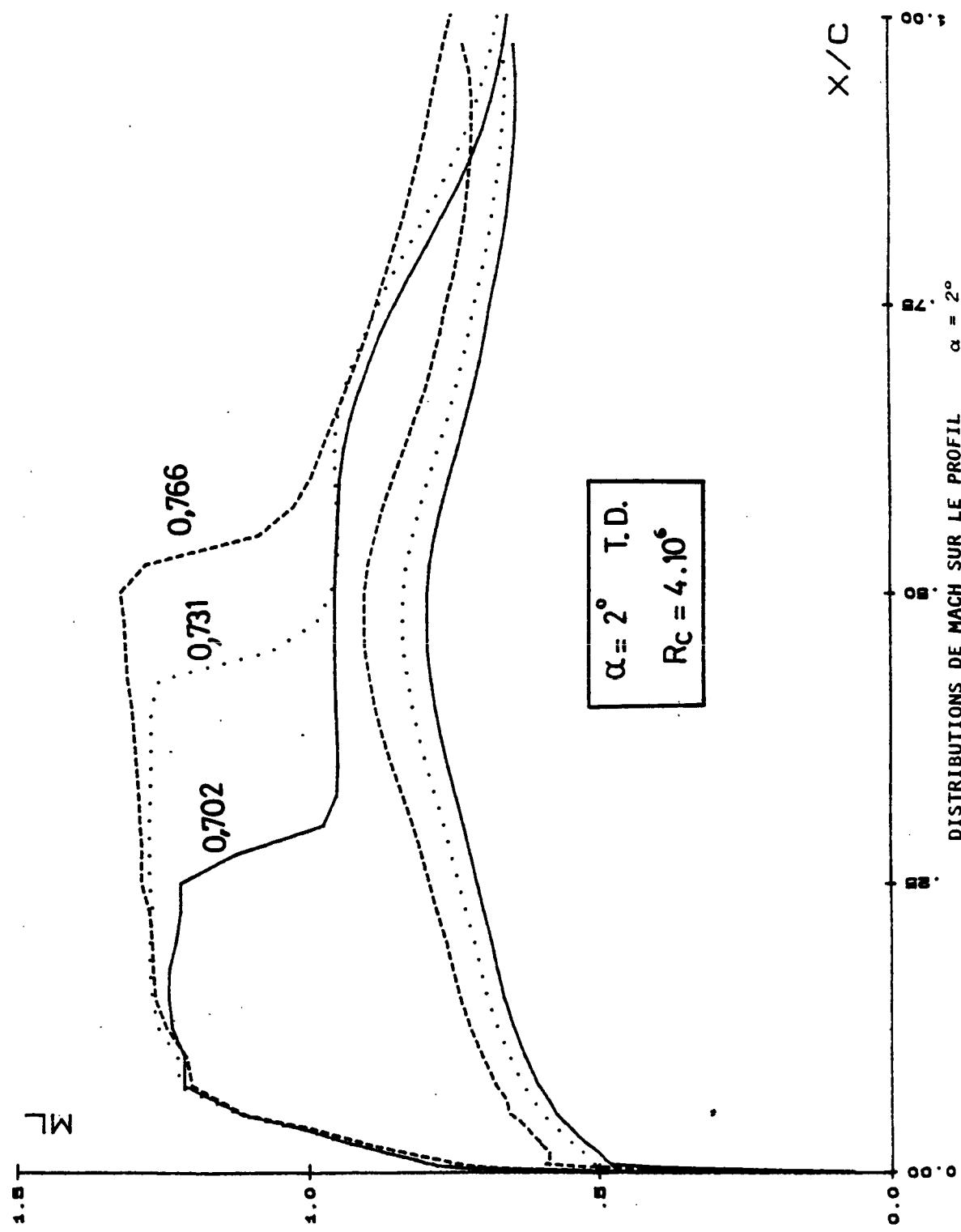
SONDAGES DES SILLAGES $\alpha = 0,25^\circ$

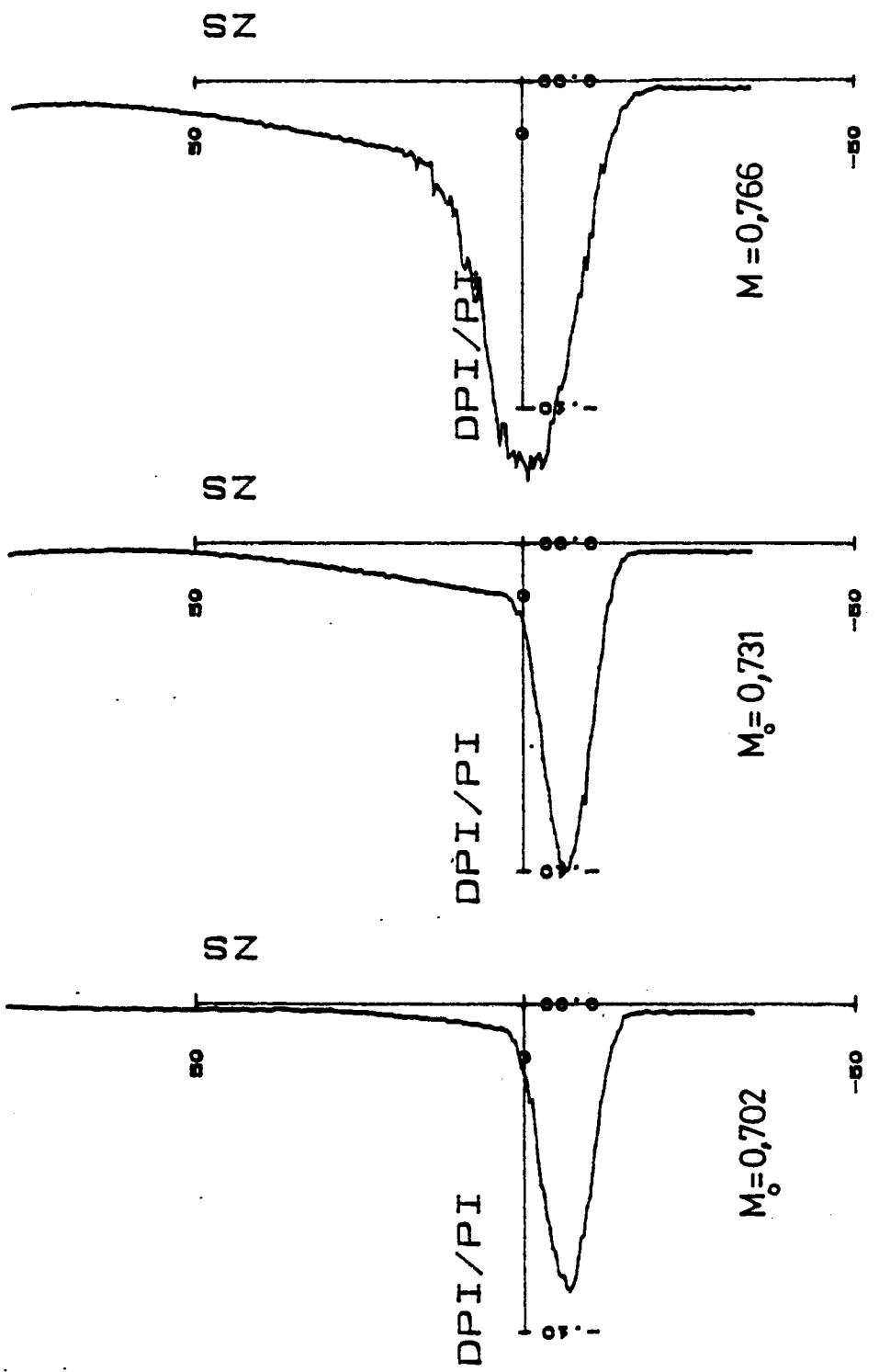




$\alpha = 1^\circ \quad R_c = 4 \cdot 10^6 \quad T.D.$

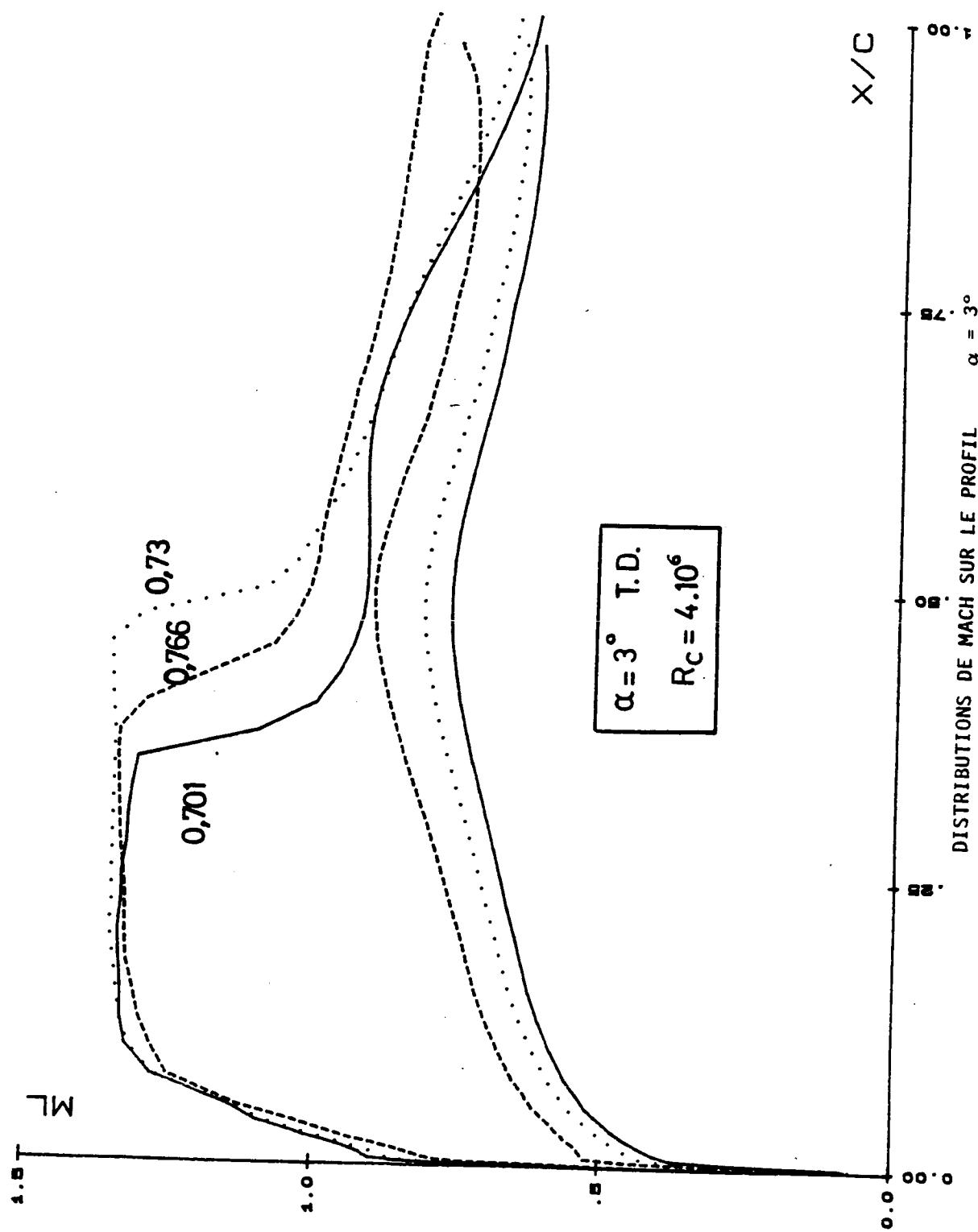
SONDAGES DES SILLAGES $\alpha = 1^\circ$

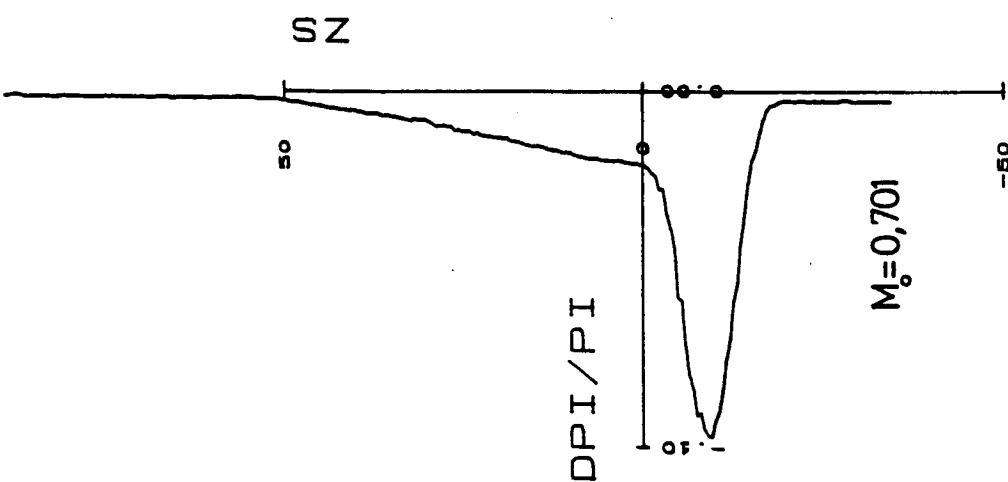
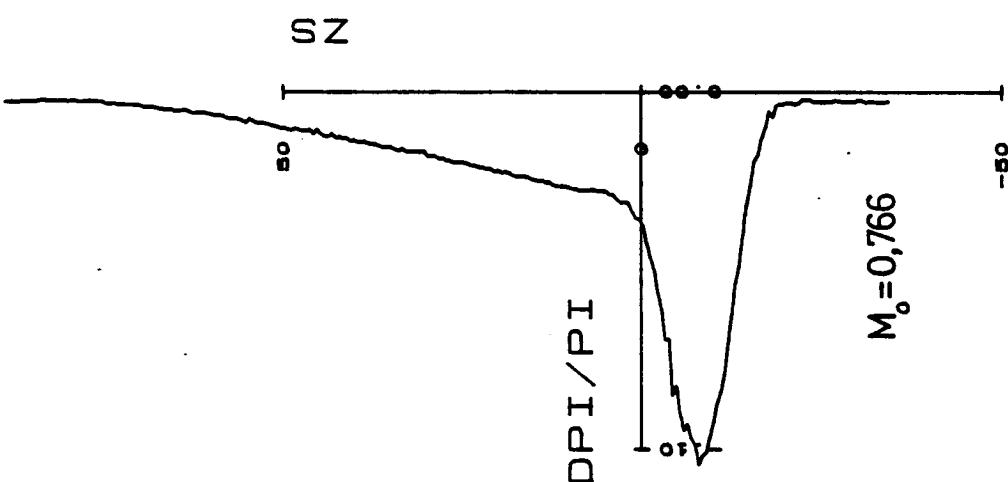
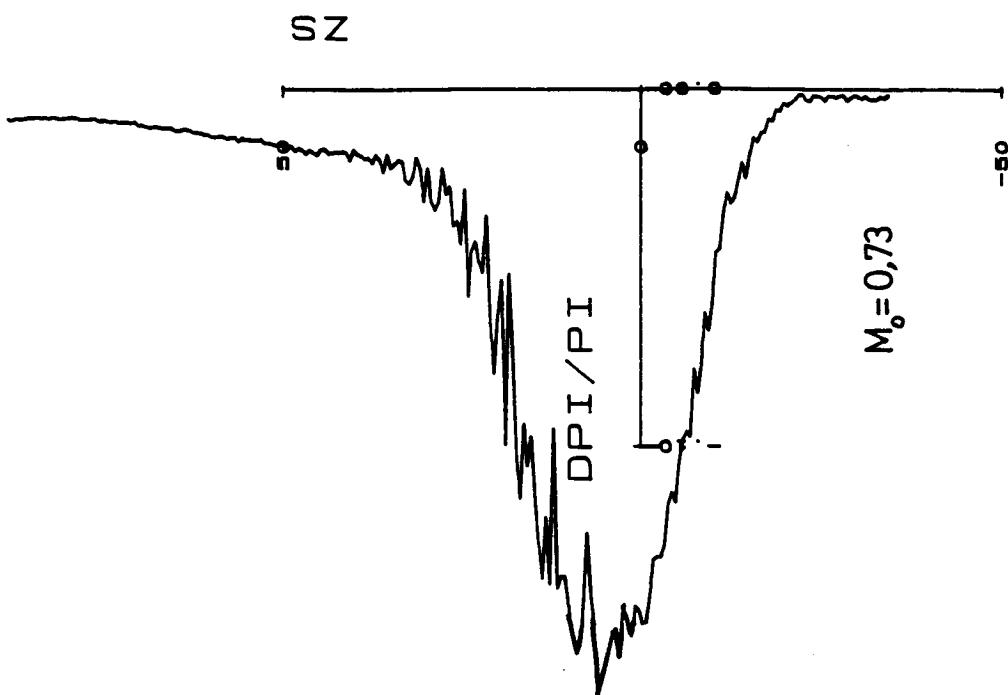




$\alpha = 2^\circ \quad R_c = 4 \cdot 10^6 \quad T.D.$

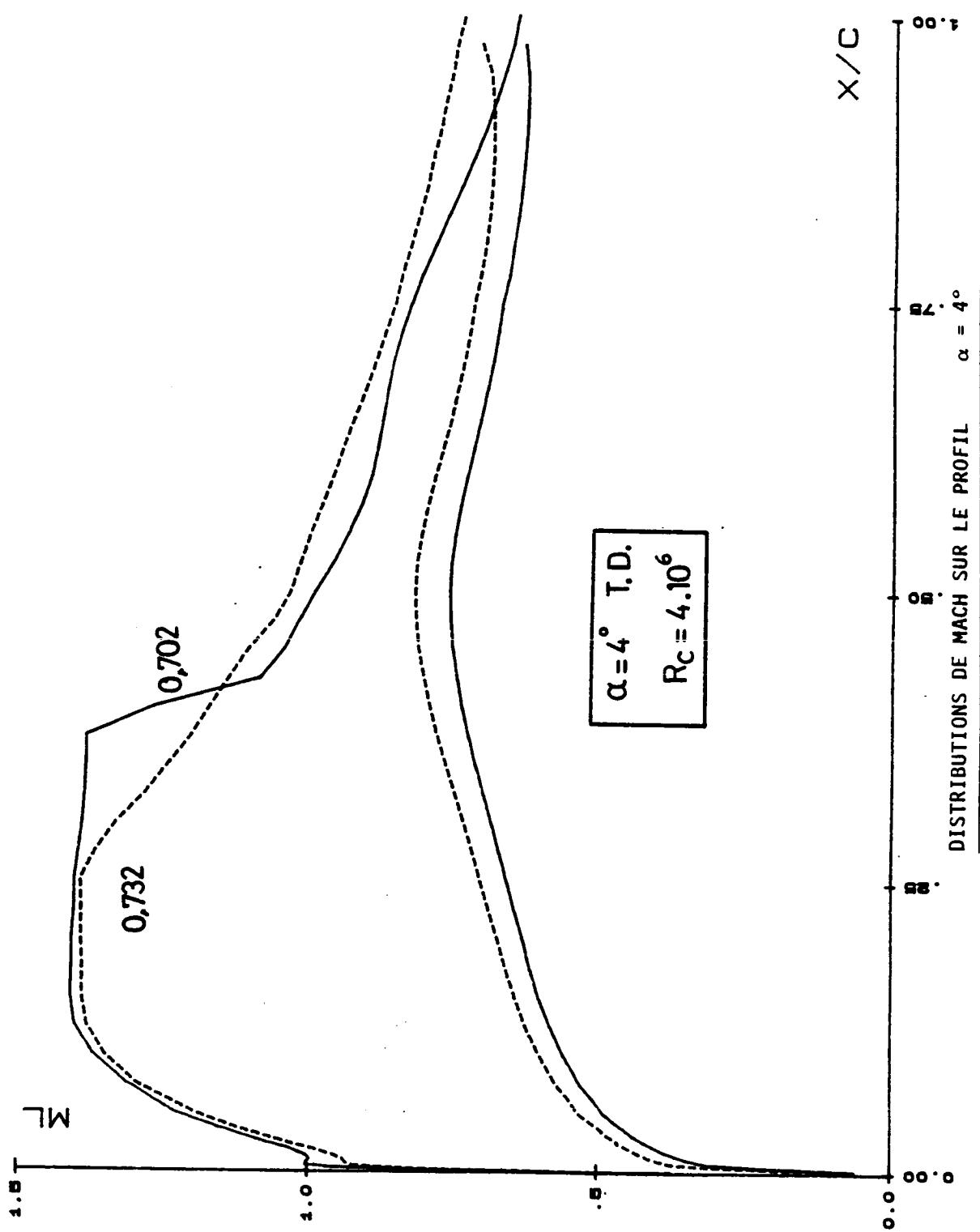
SONDAGES DES SILLAGES $\alpha = 2^\circ$

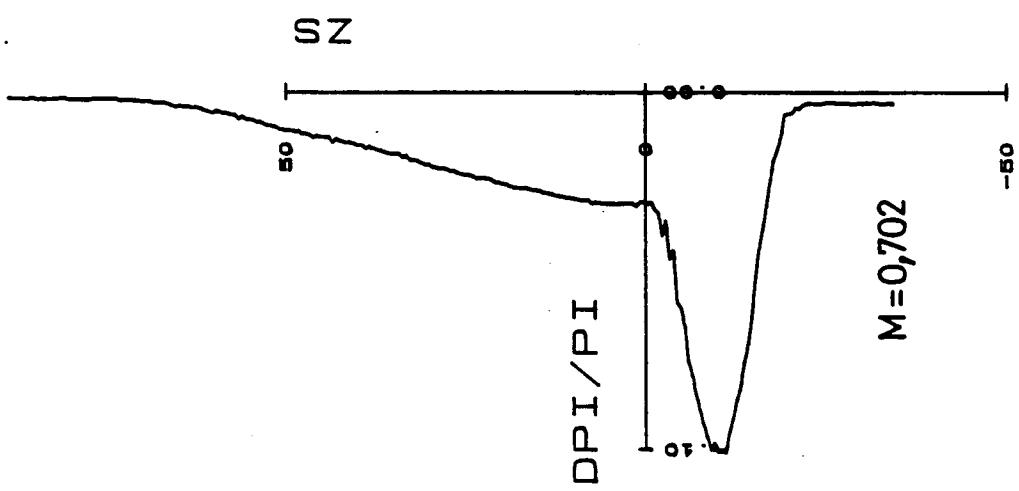
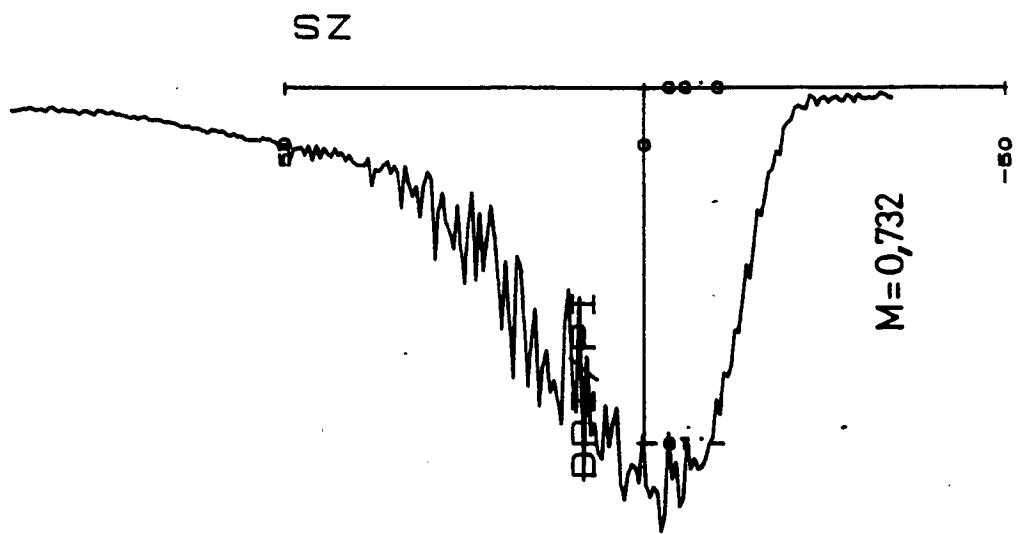




$\alpha = 3^\circ \quad R_C = 4 \cdot 10^6 \quad T.D.$

SONDAGES DES SILLAGES $\alpha = 3^\circ$





$\alpha = 4^\circ$ $Rc = 4 \cdot 10^6$ T. D.

SONDAGES DES SILLAGES $\alpha = 4^\circ$

T.D.

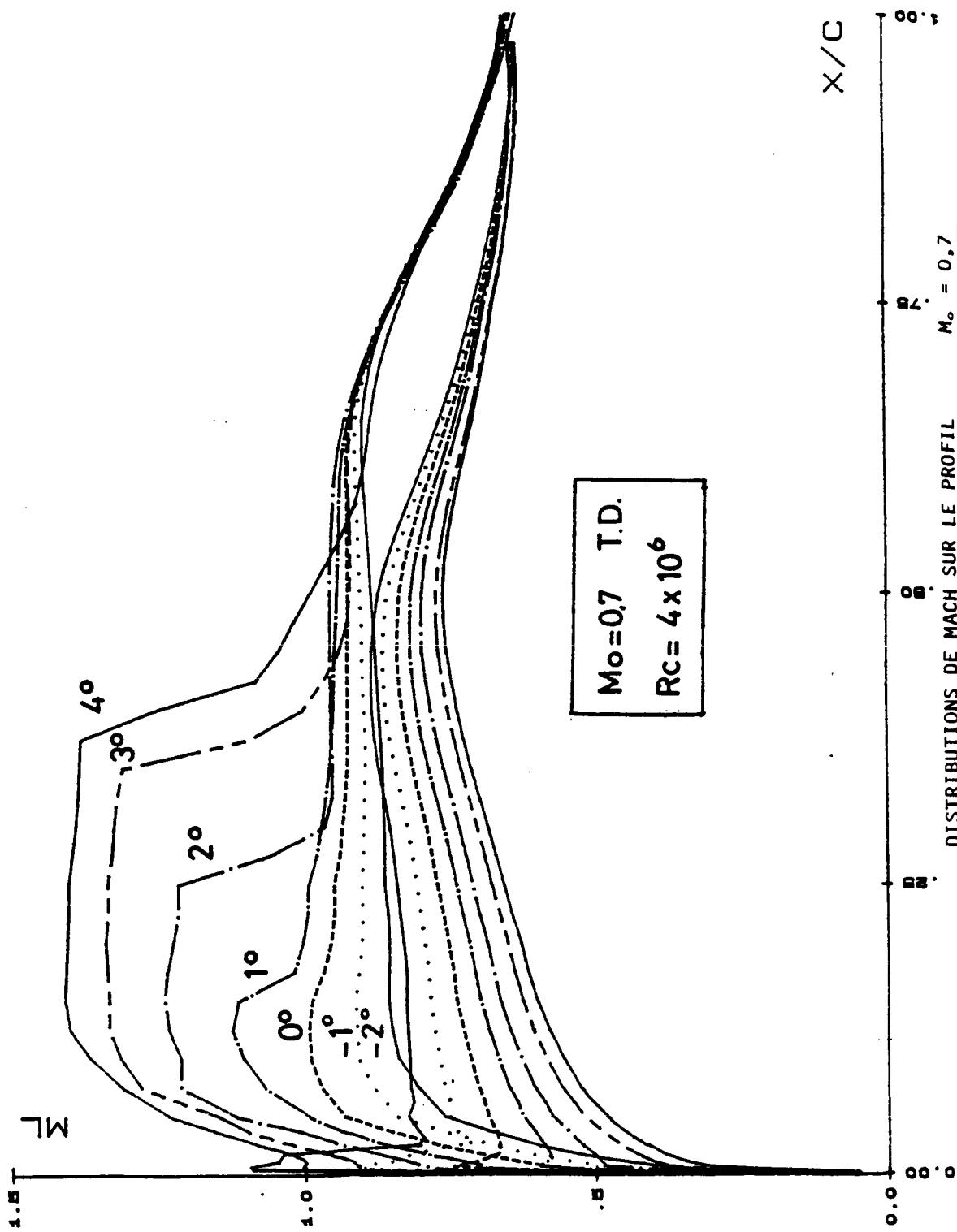
VARIATION D'INCIDENCE

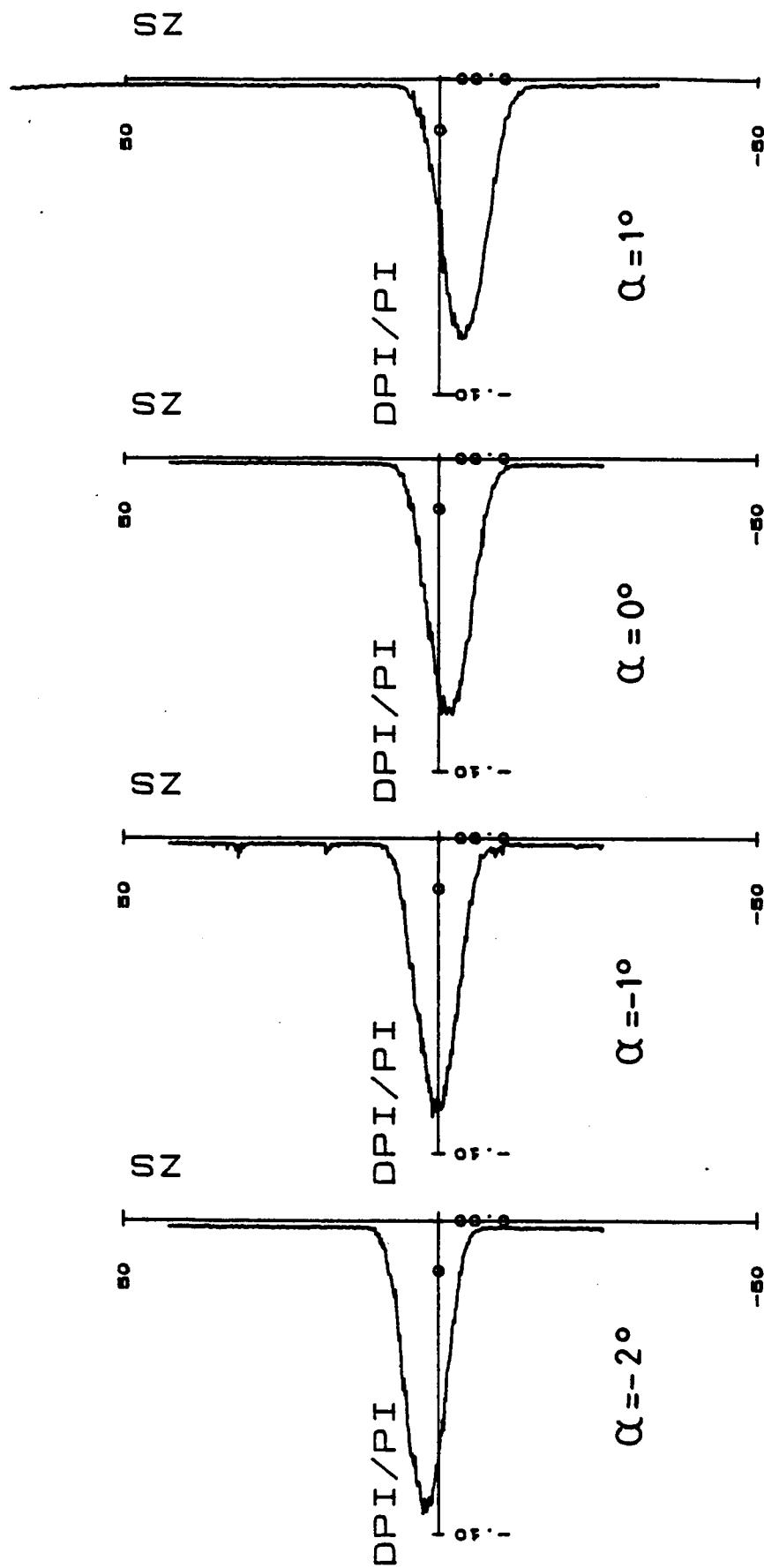
$$R_C = 4 \cdot 10^6$$

$M_o = 0,7$ PL. 64 à 66

$M_o = 0,73$ PL. 67 à 69

$M_o = 0,765$ PL. 70 et 71





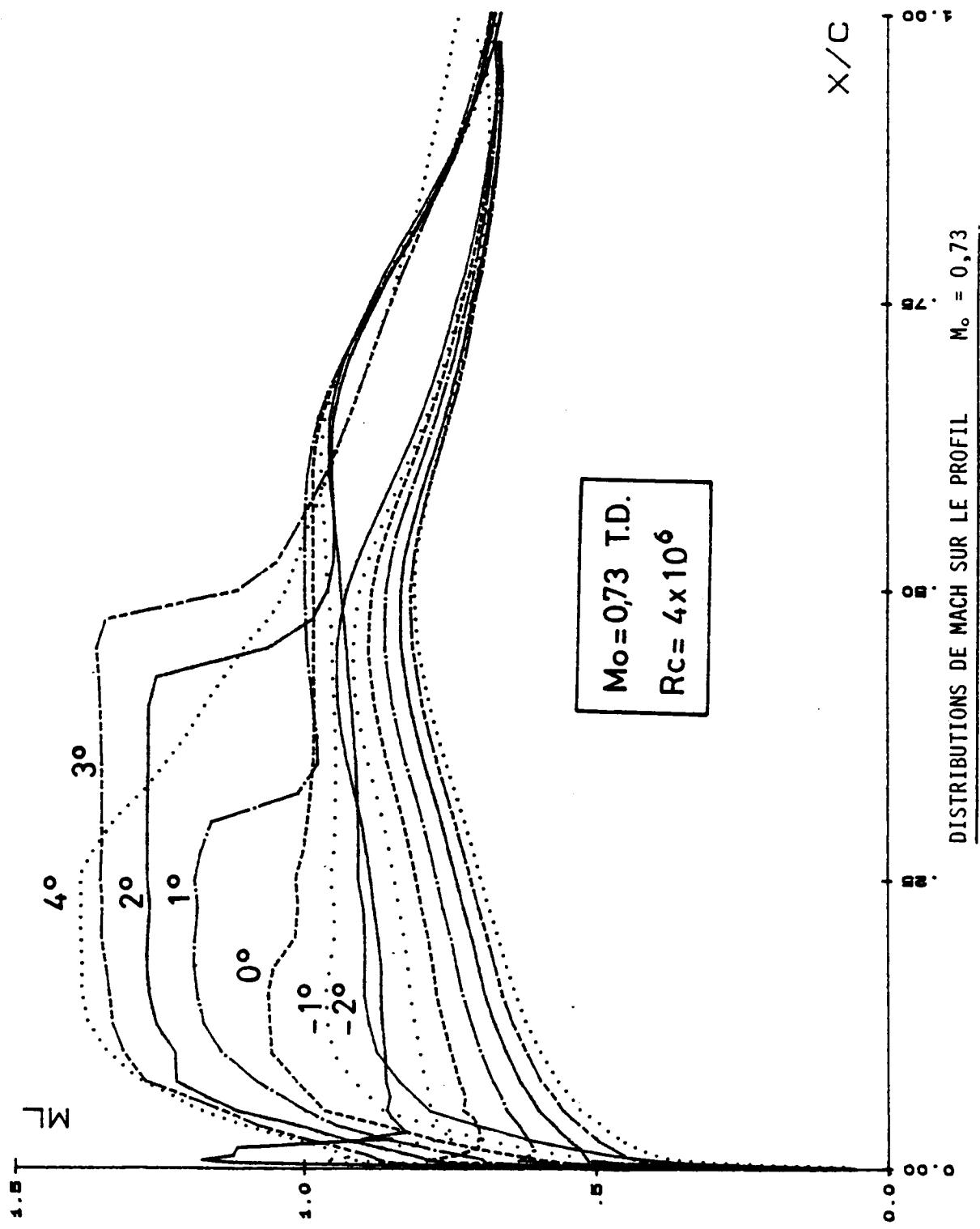
$M_o = 0,7 \quad R_c = 4 \times 10^6 \quad T.D.$

SONDAGES DES SILLAGES $M_o = 0,7$

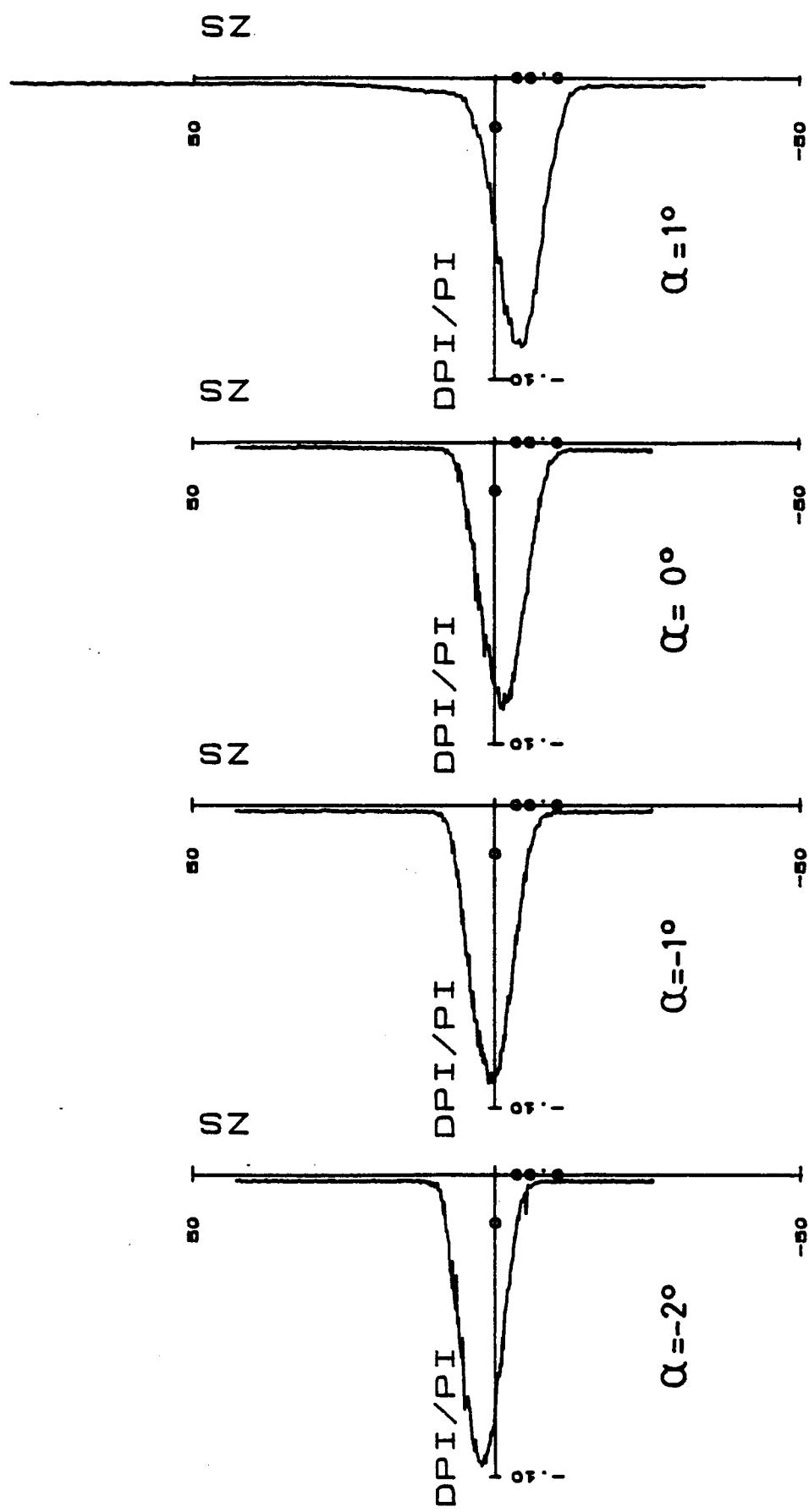


$M_o = 0,7 \quad R_c = 4 \times 10^6 \quad T.D.$

SONDAGES DES SILLAGES (suite) $M_o = 0,7$

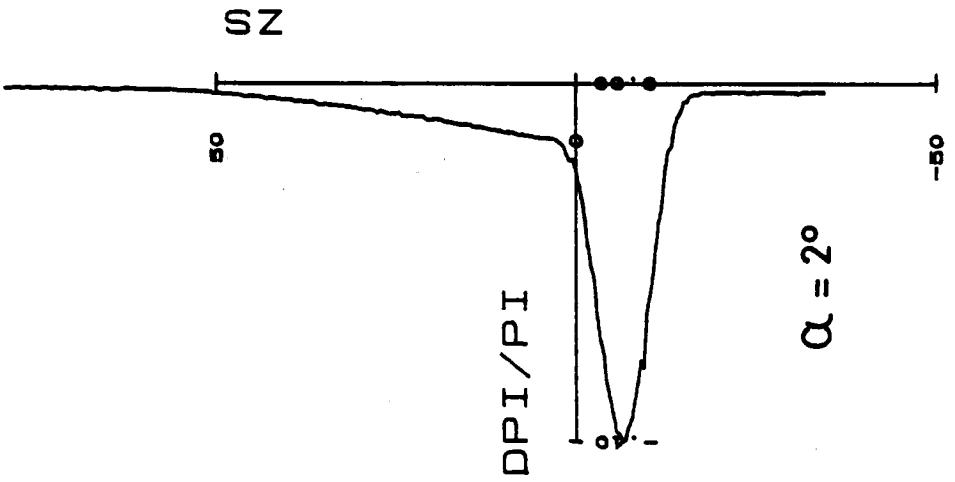
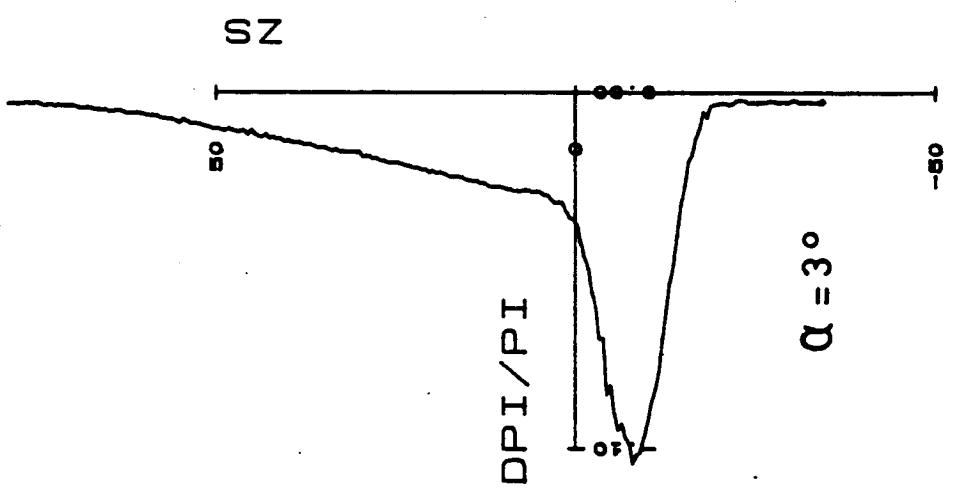
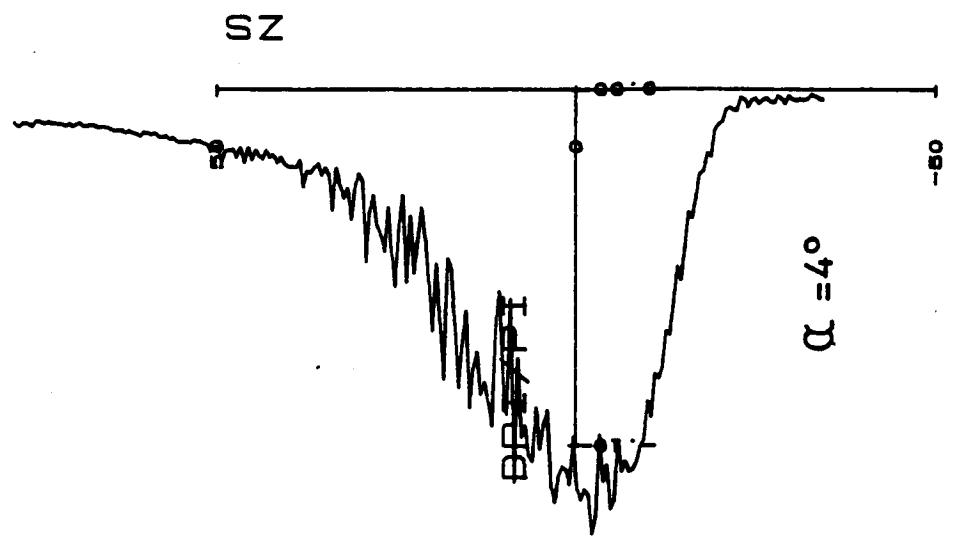


PL. 68



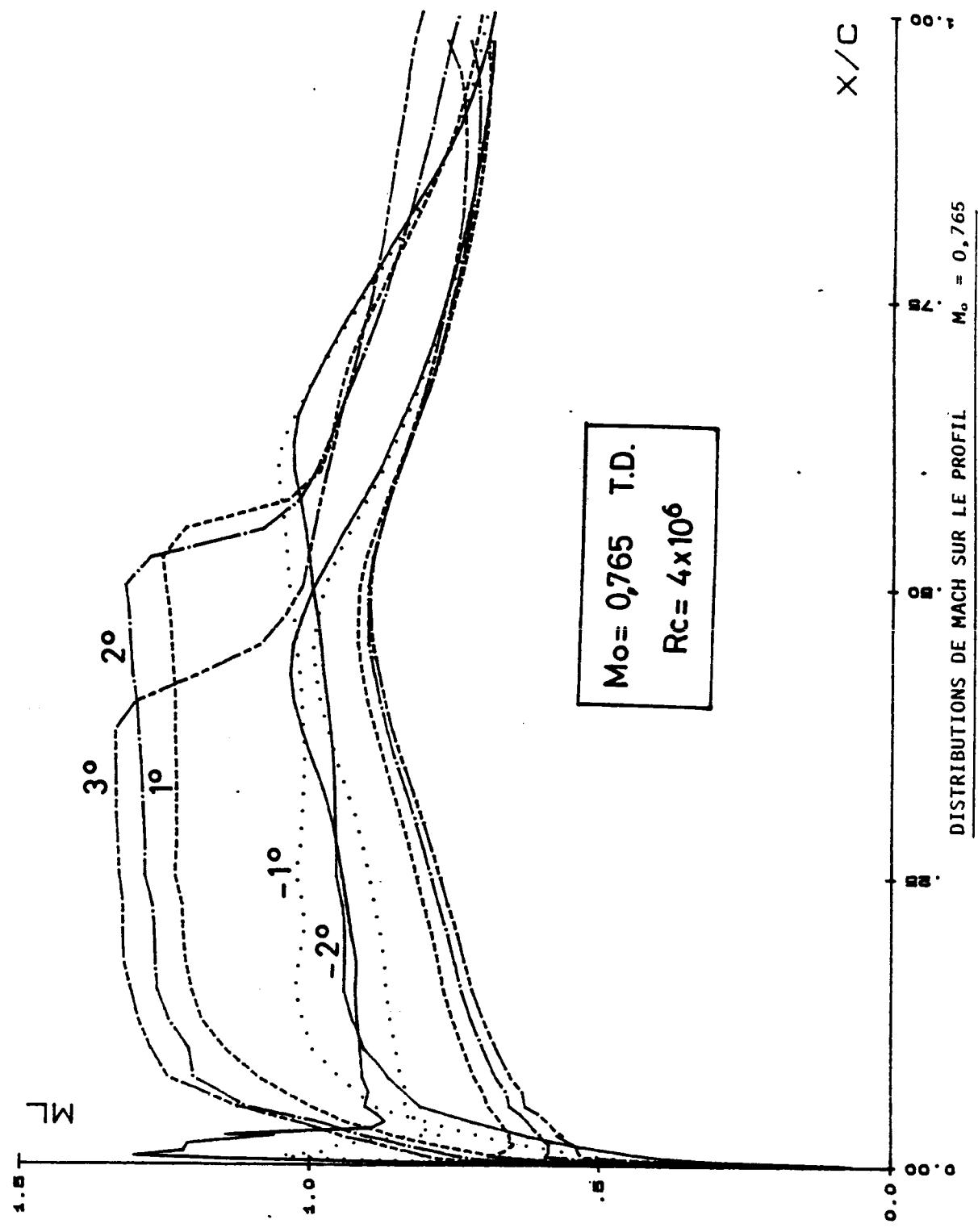
$M_o = 0,73 \quad R_c = 4 \times 10^6 \quad T.D.$

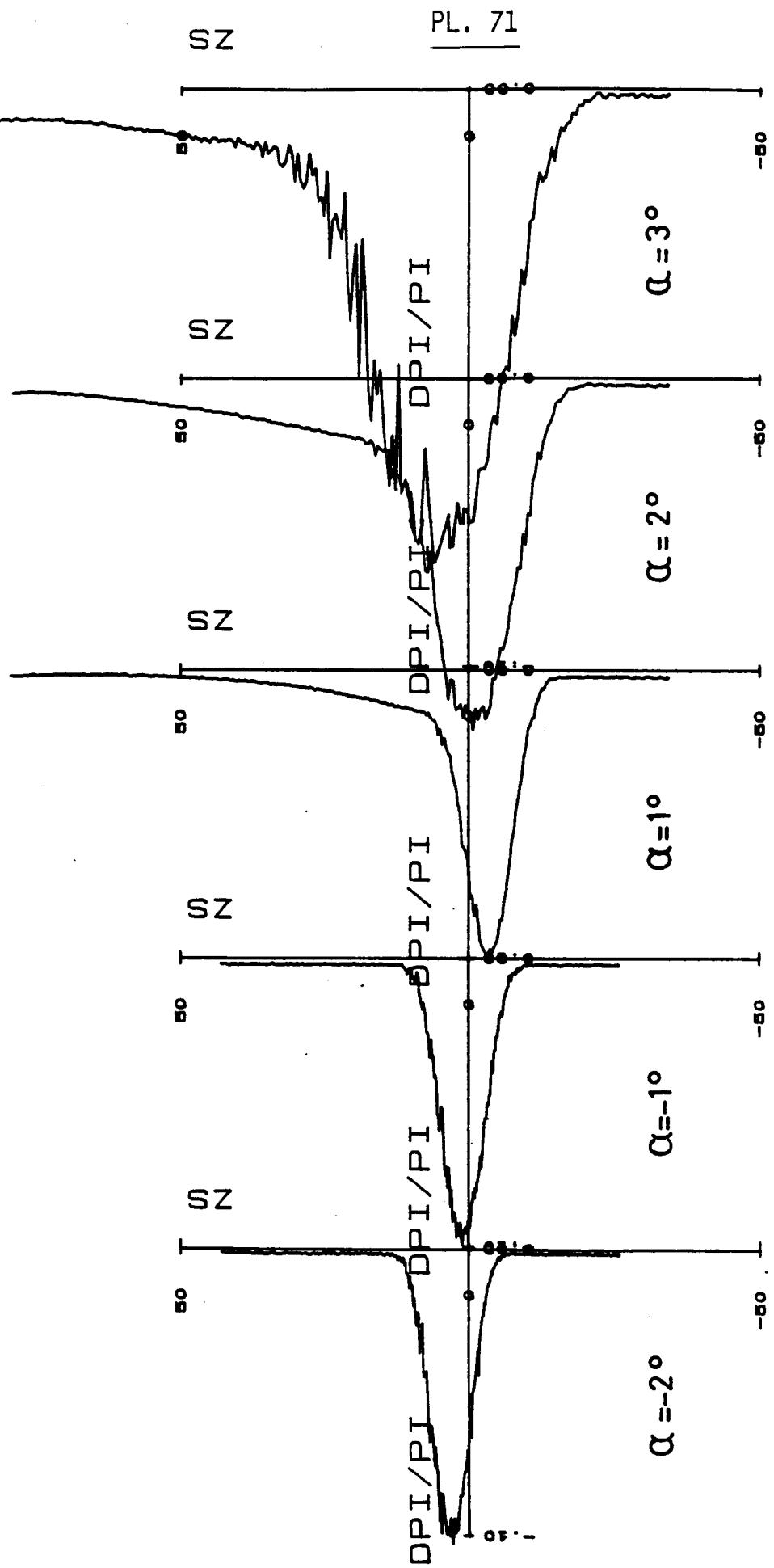
SONDAGES DES SILLAGES $M_o = 0,73$



$M_o = 0,73 \quad R_c = 4 \times 10^6 \quad T.D.$

SONDAGES DES SILLAGES (suite) $M_o = 0,73$





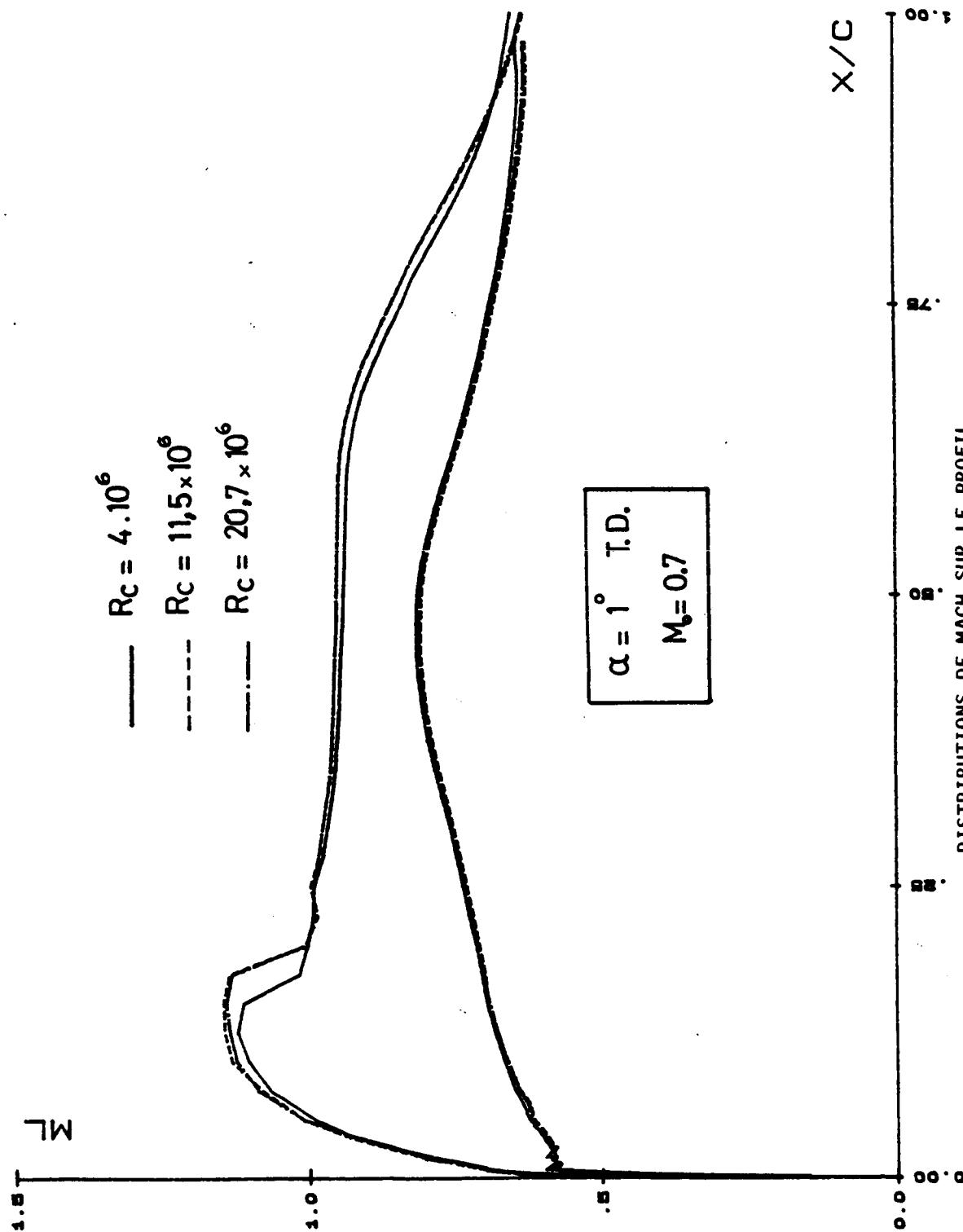
$M_o = 0,765 \quad R_c = 4 \times 10^6 \quad T.D.$

SONDAGES DES SILLAGES $M_o = 0,765$

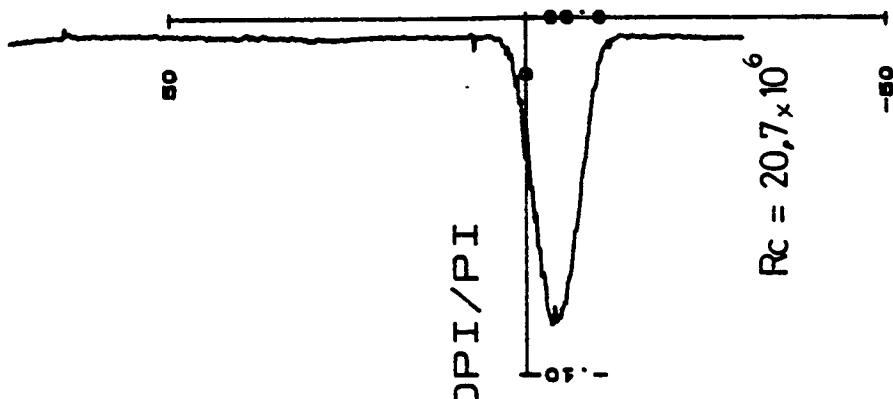
T.D.

VARIATION DU NOMBRE DE REYNOLDS

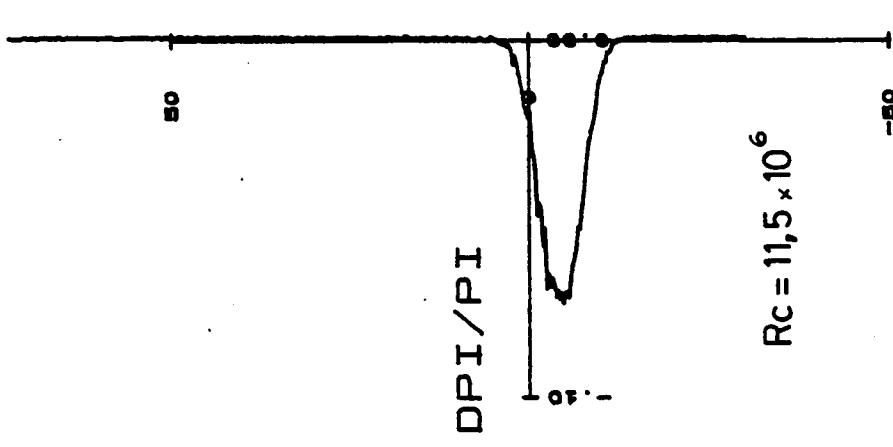
$M_o = 0,7$	et $\alpha = + 1^\circ$	PL. 72 et 73
$M_o = 0,73$	et $\alpha = - 0,25^\circ$	PL. 74 et 75
$M_o = 0,76$	et $\alpha = + 0,25^\circ$	PL. 76 et 77
$M_o = 0,76$	et $\alpha = + 1^\circ$	PL. 78 et 79
$M_o = 0,765$	et $\alpha = - 2^\circ$	PL. 80 et 81
$M_o = 0,765$	et $\alpha = + 2^\circ$	PL. 82 et 83



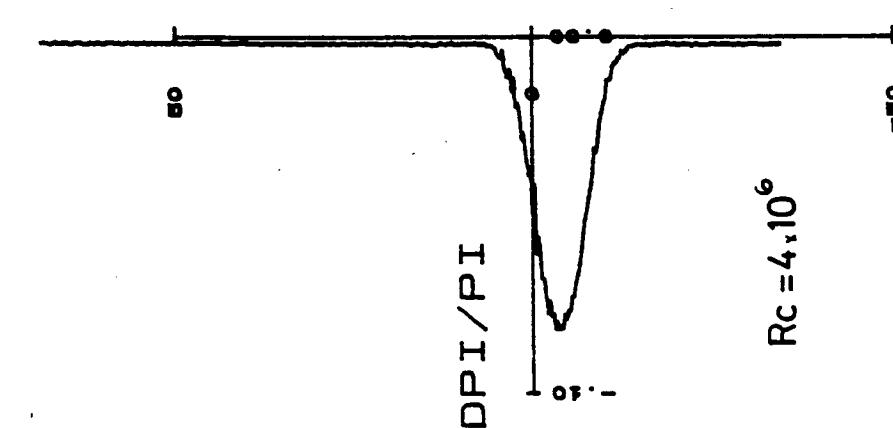
SN



SN

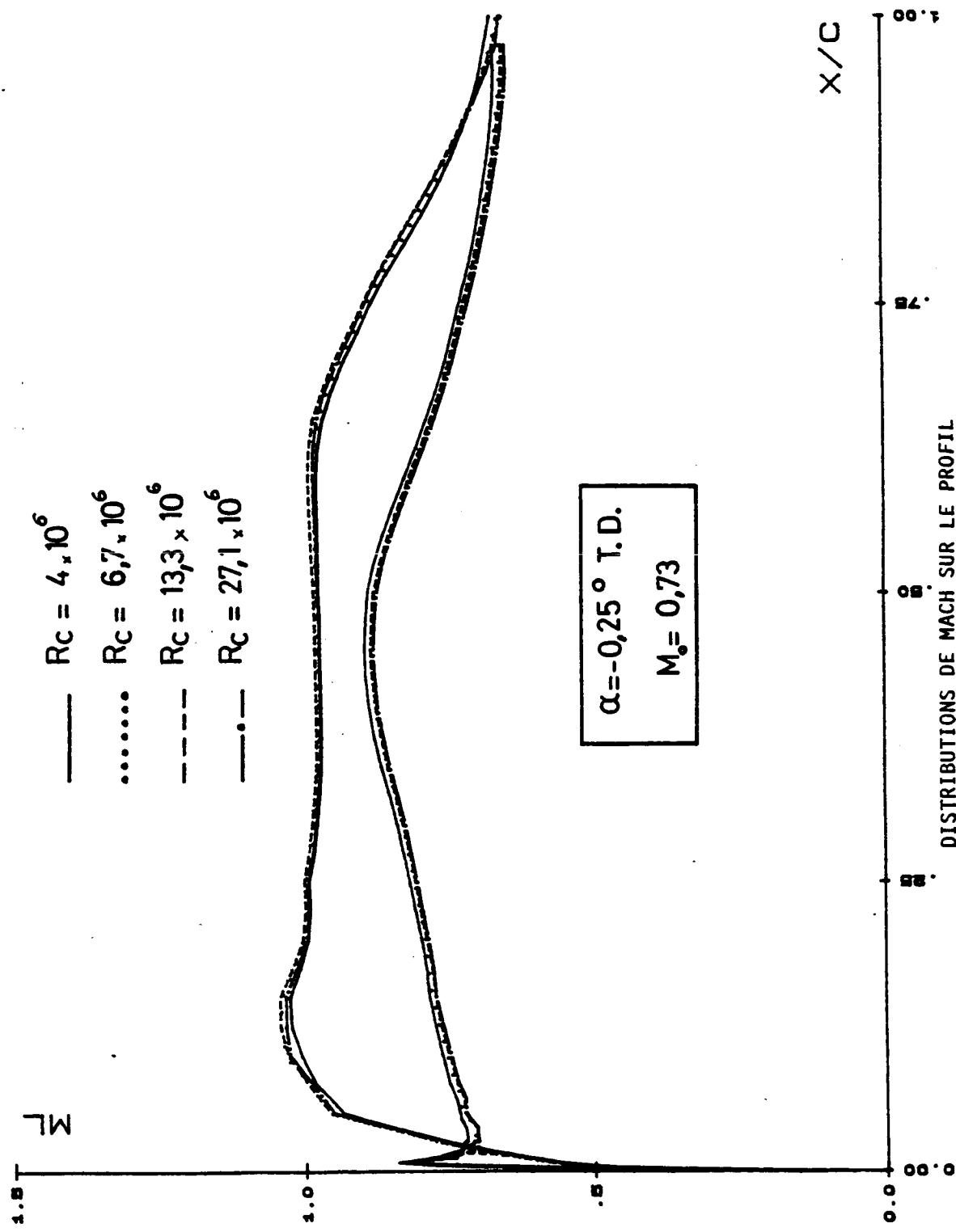


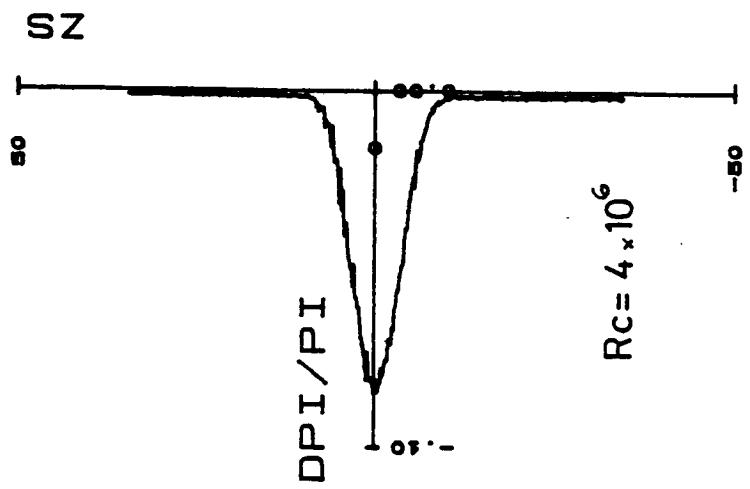
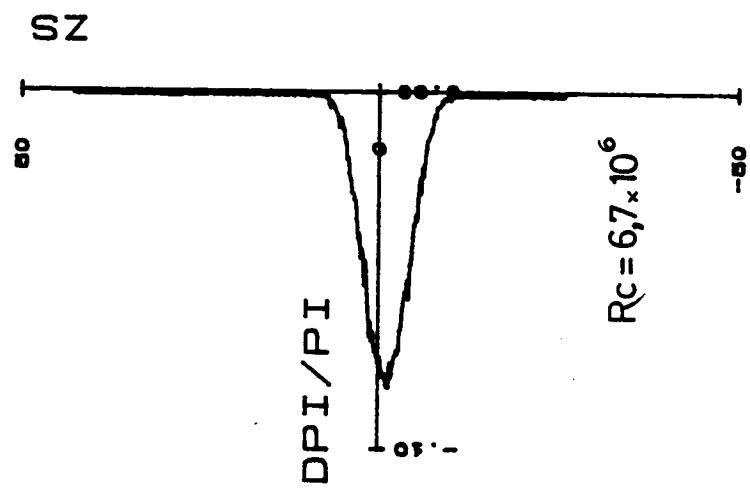
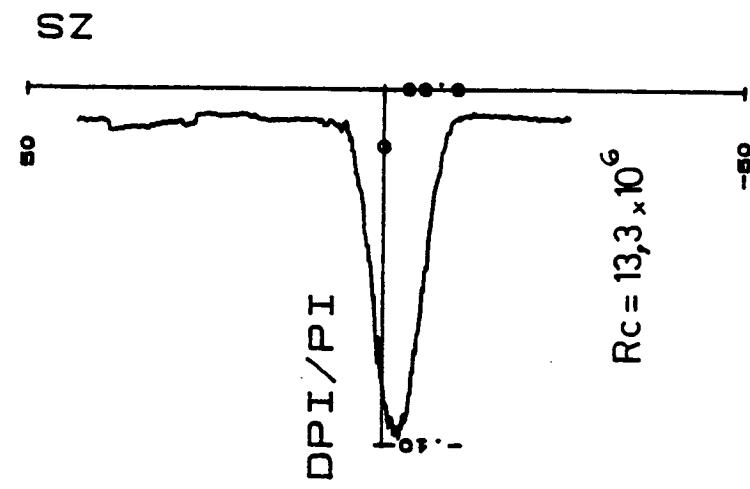
SN



$\alpha = 1^\circ \quad M = 0,7 \quad T.D.$

SONDAGES DES SILLAGES





$\alpha = -0,25^\circ \quad M = 0,73 \quad T.D.$

SONDAGES DES SILLAGES

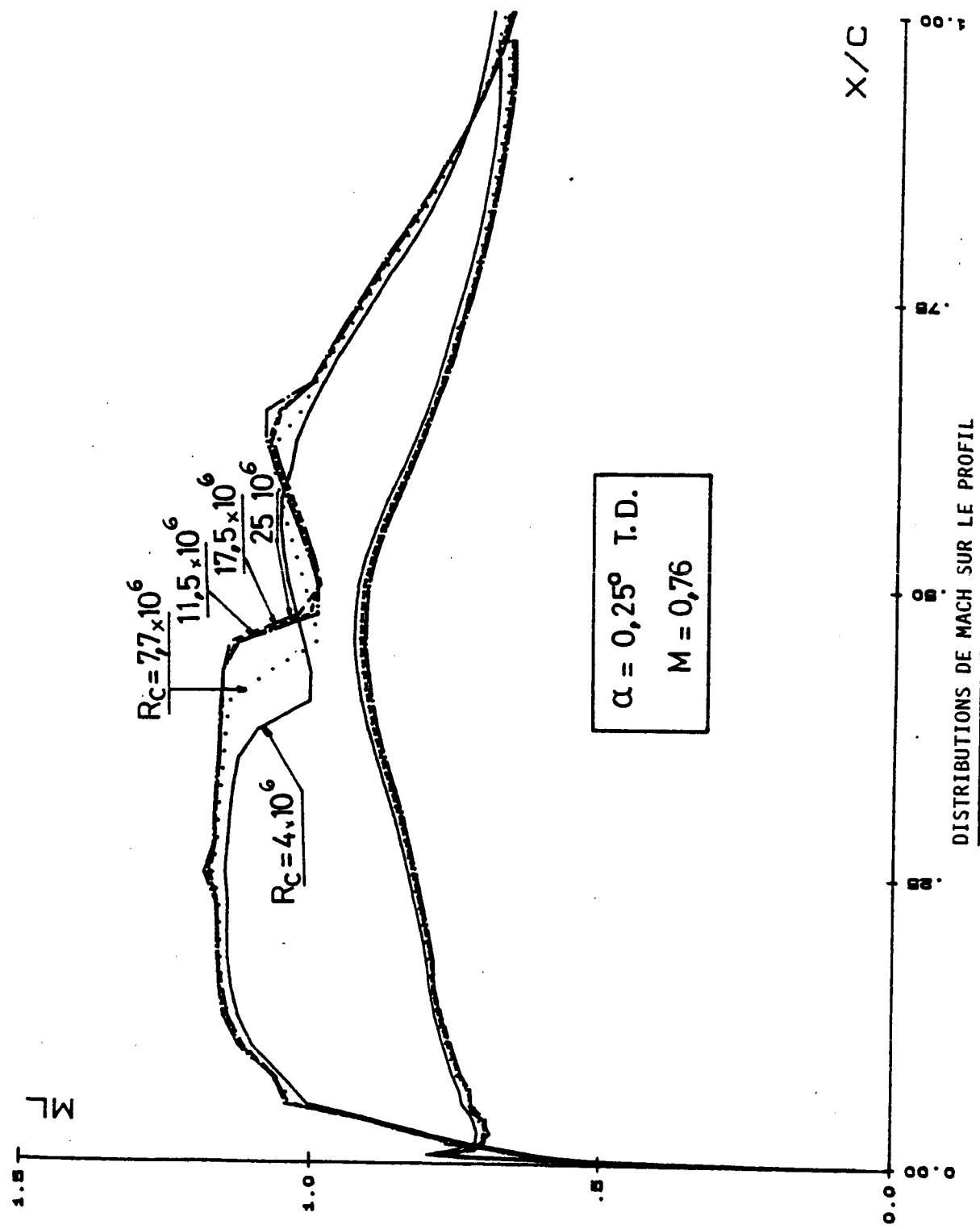
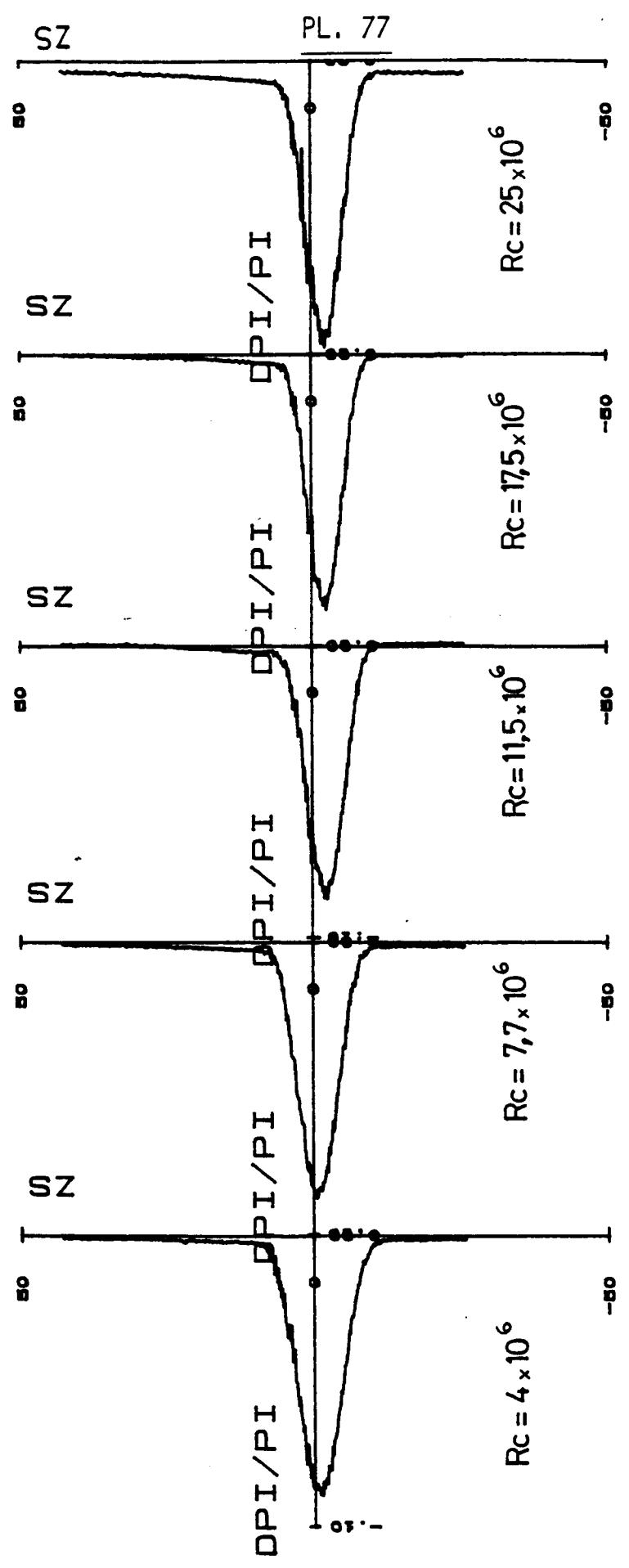
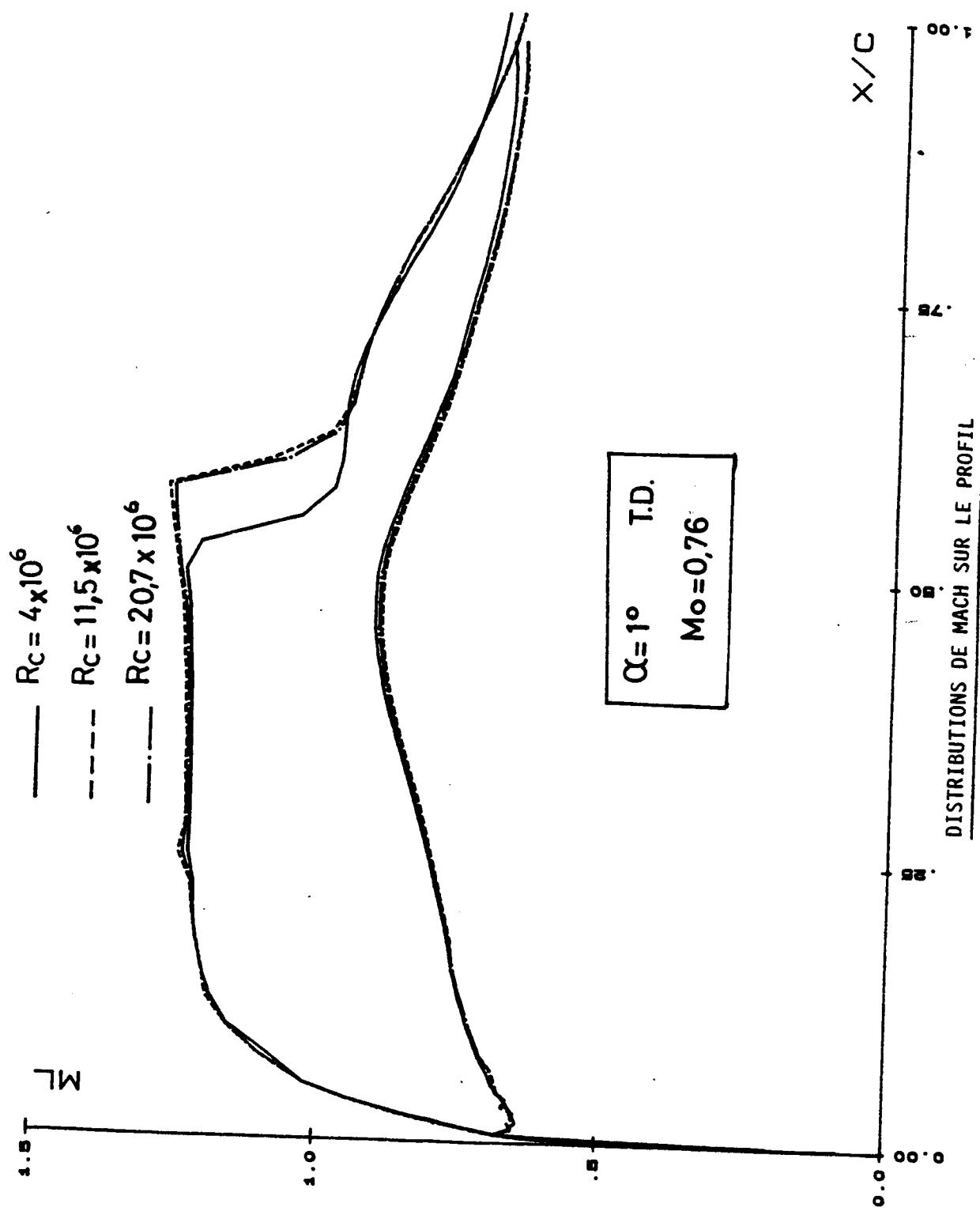


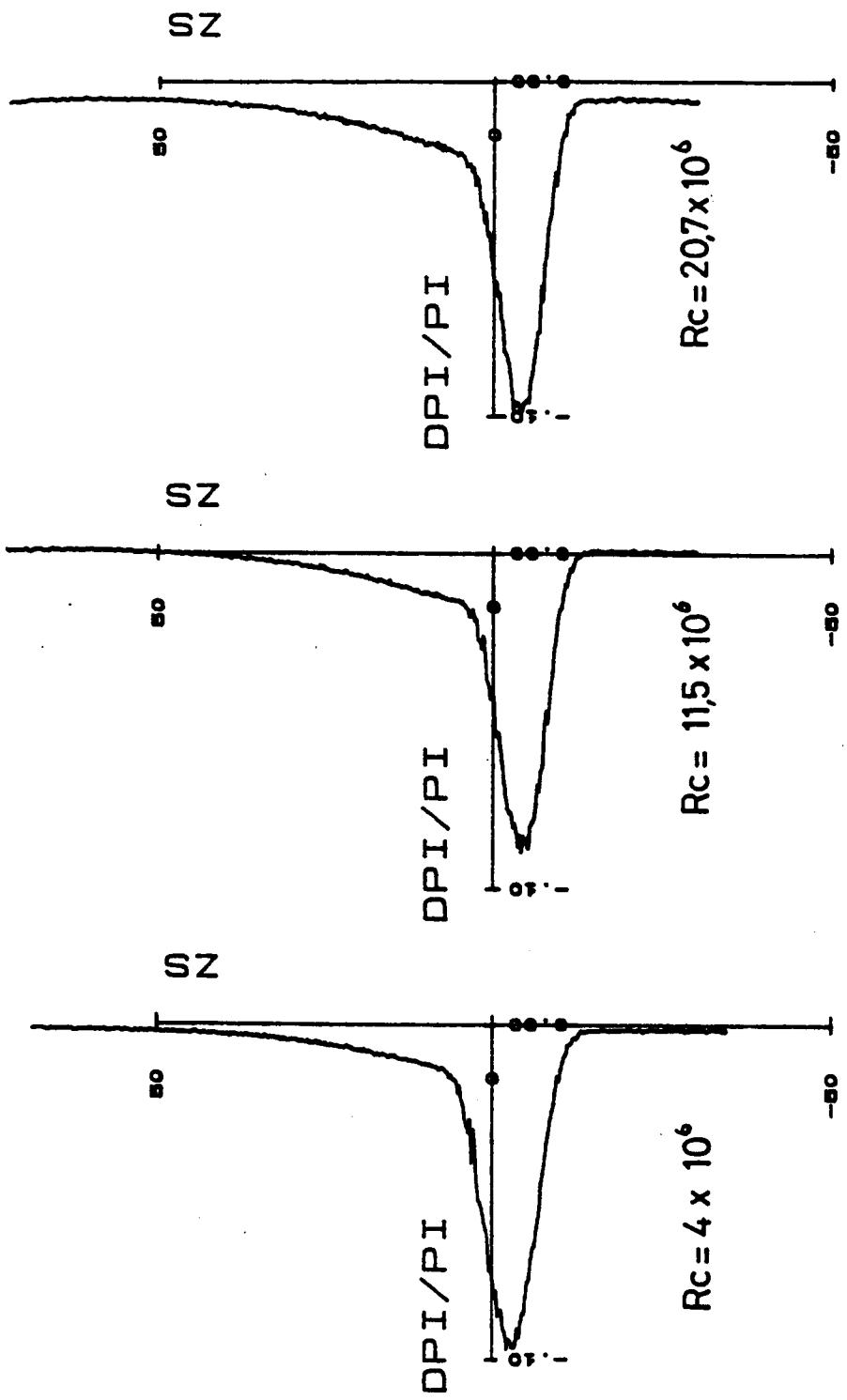
Fig. 77



$\alpha = 0,25^\circ$ $M = 0,76$ T.D.

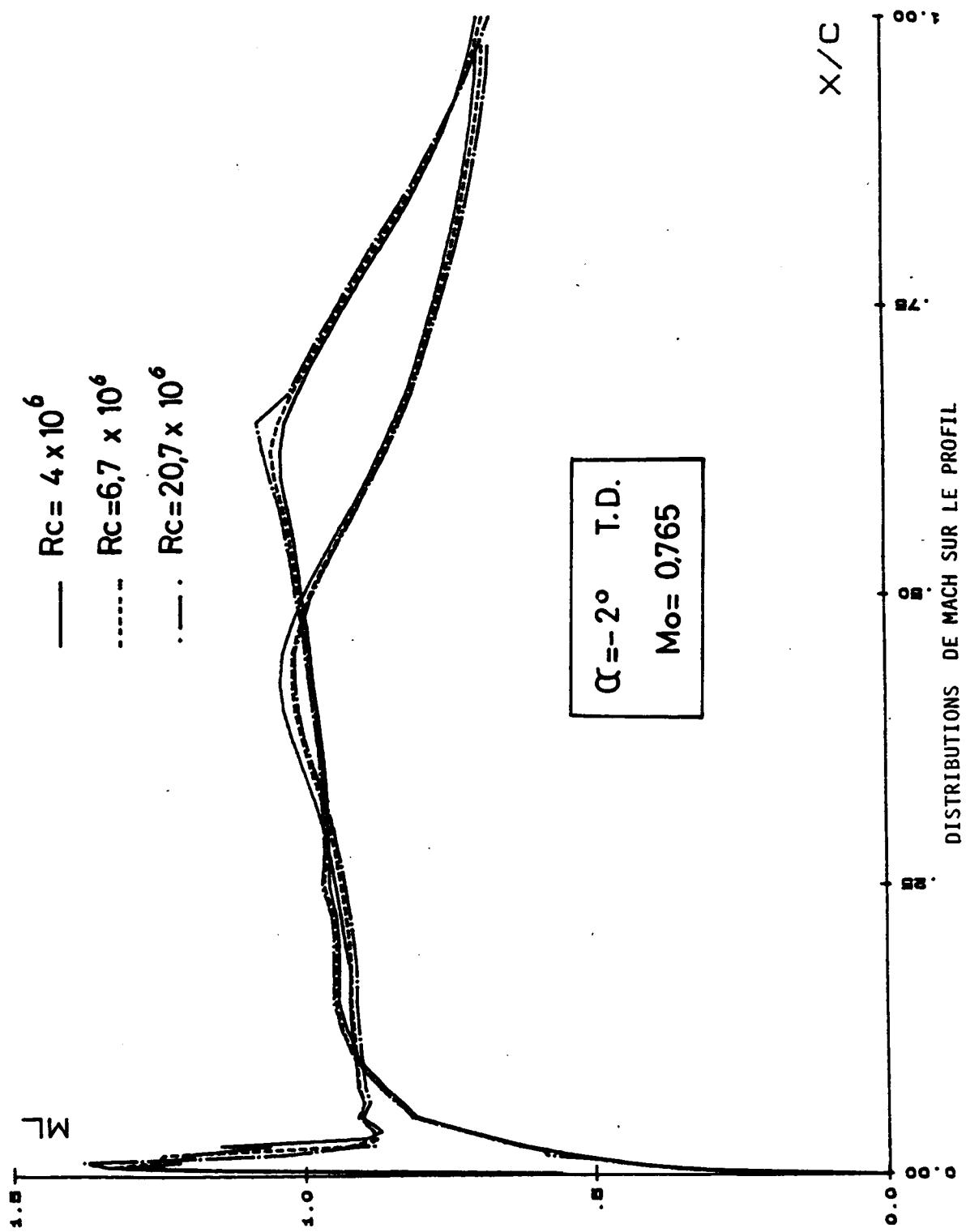
SONDAGES DES SILLAGES

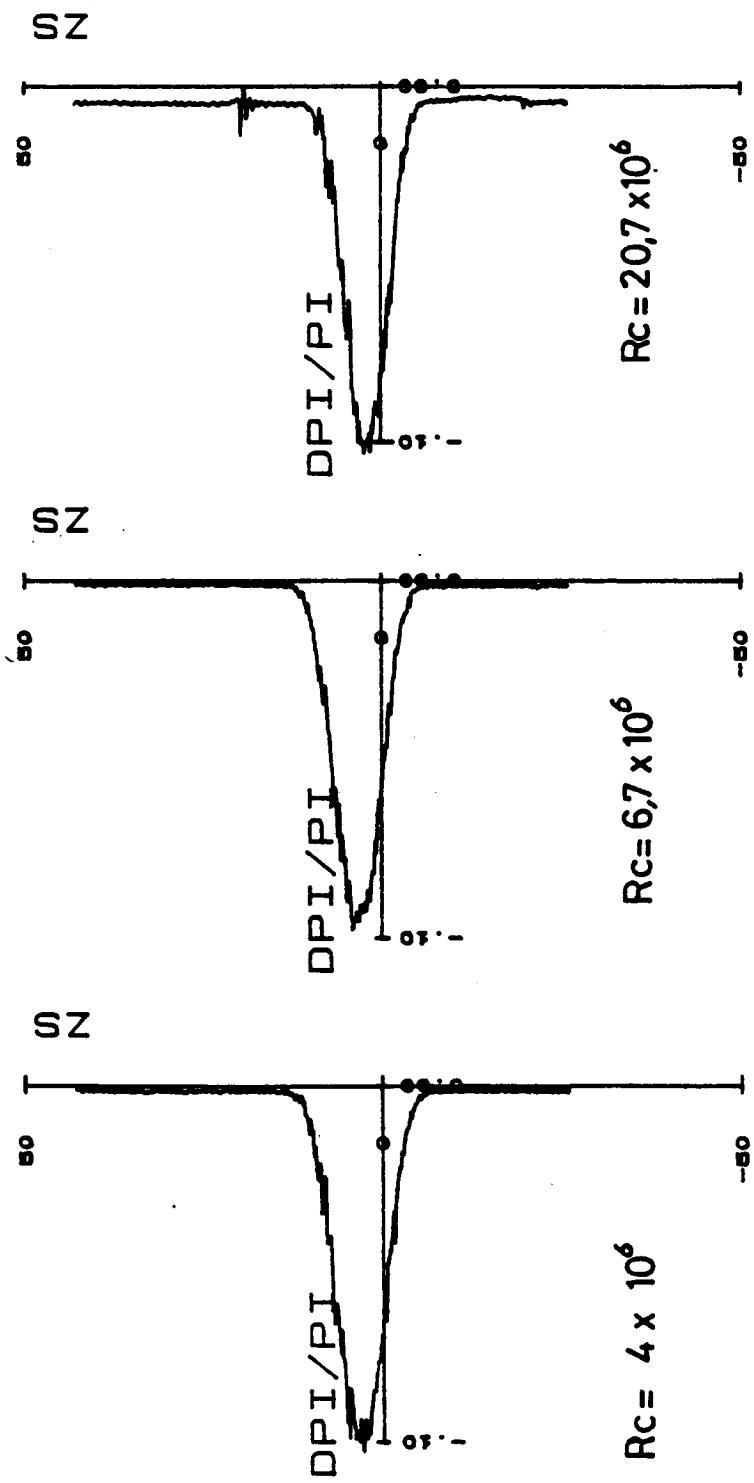




$\alpha = 1^\circ$ $M_0 = 0,76$ T.D.

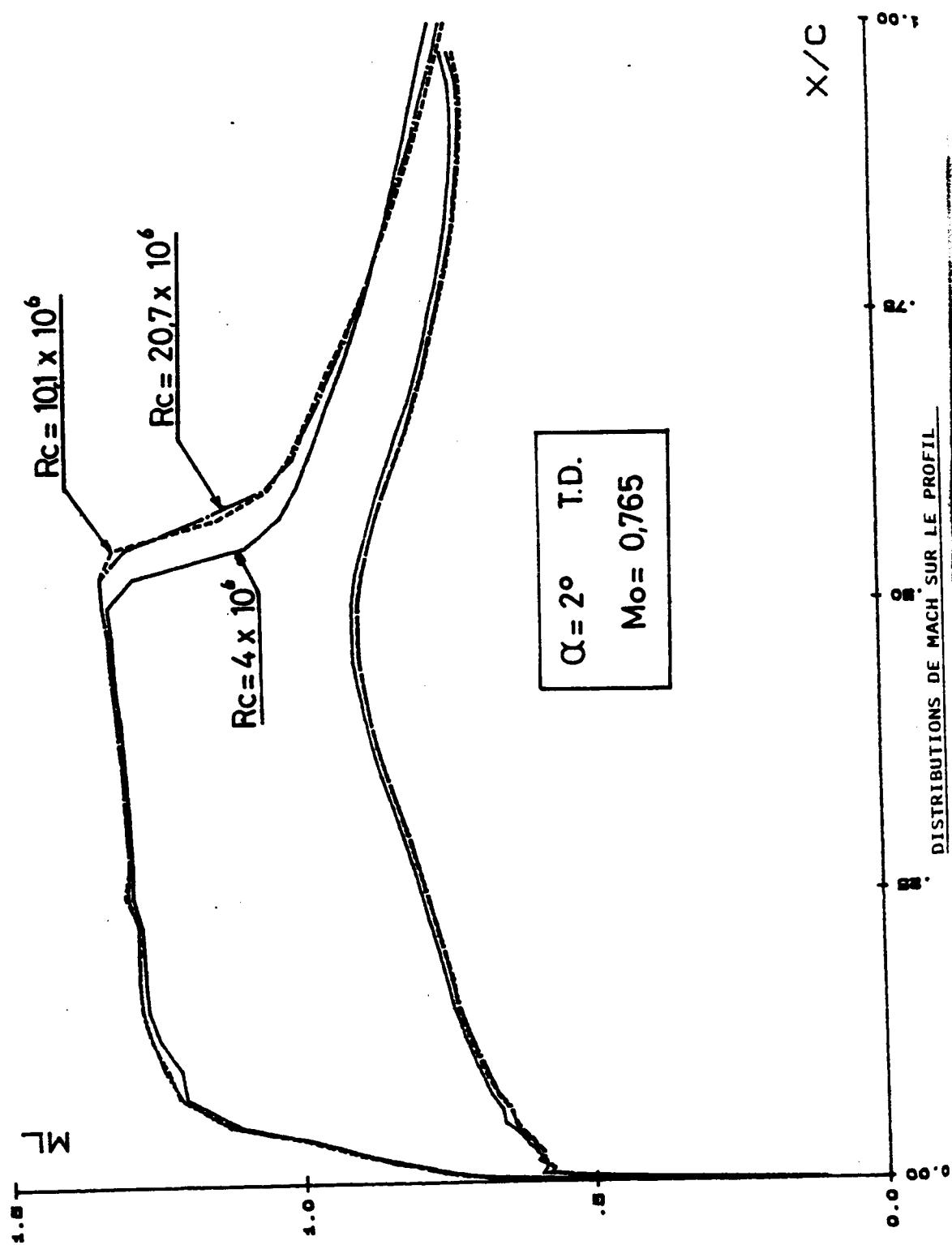
SONDAGES DES SILLAGES

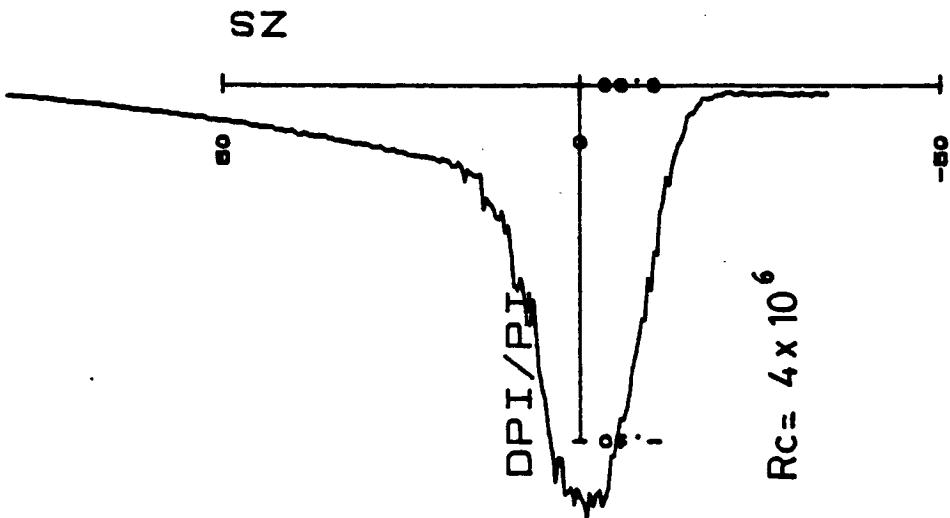
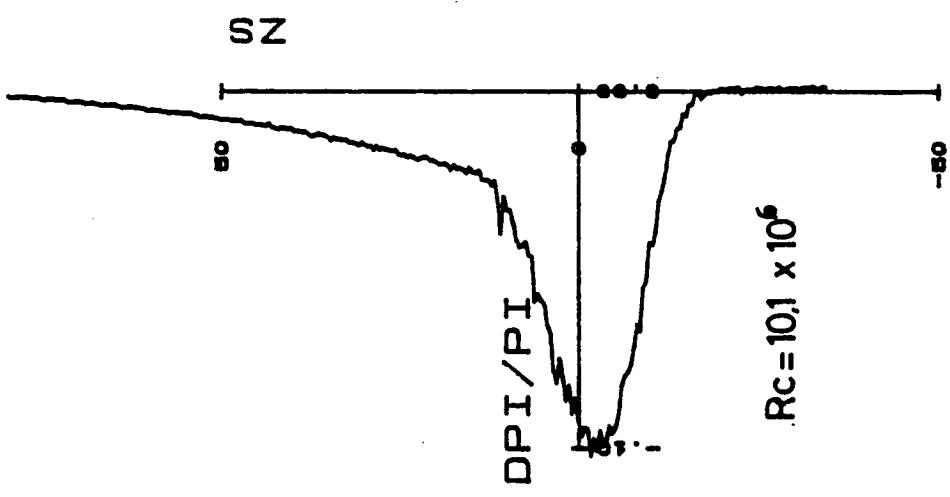
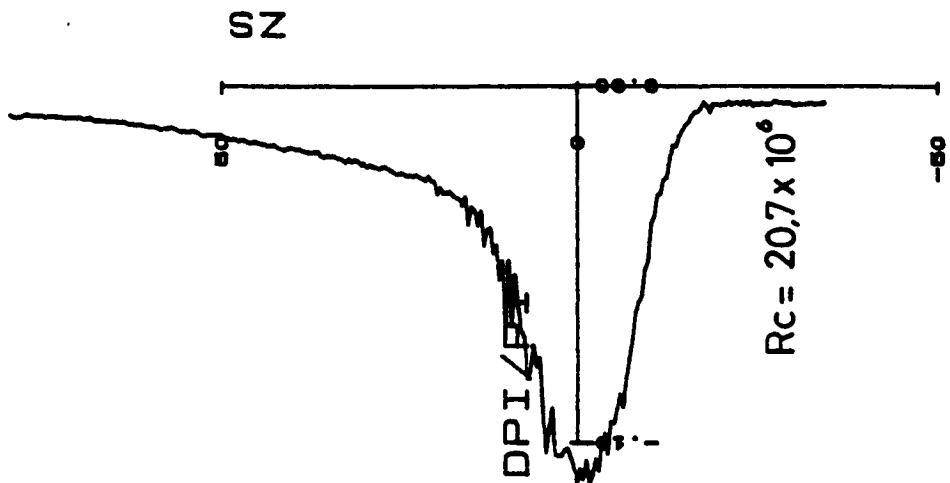




$\alpha = -2^\circ$ $M_o = 0,765$ T.D.

SONDAGES DES SILLAGES





$\alpha = 2^\circ \quad M_o = 0,765 \text{ T.D.}$

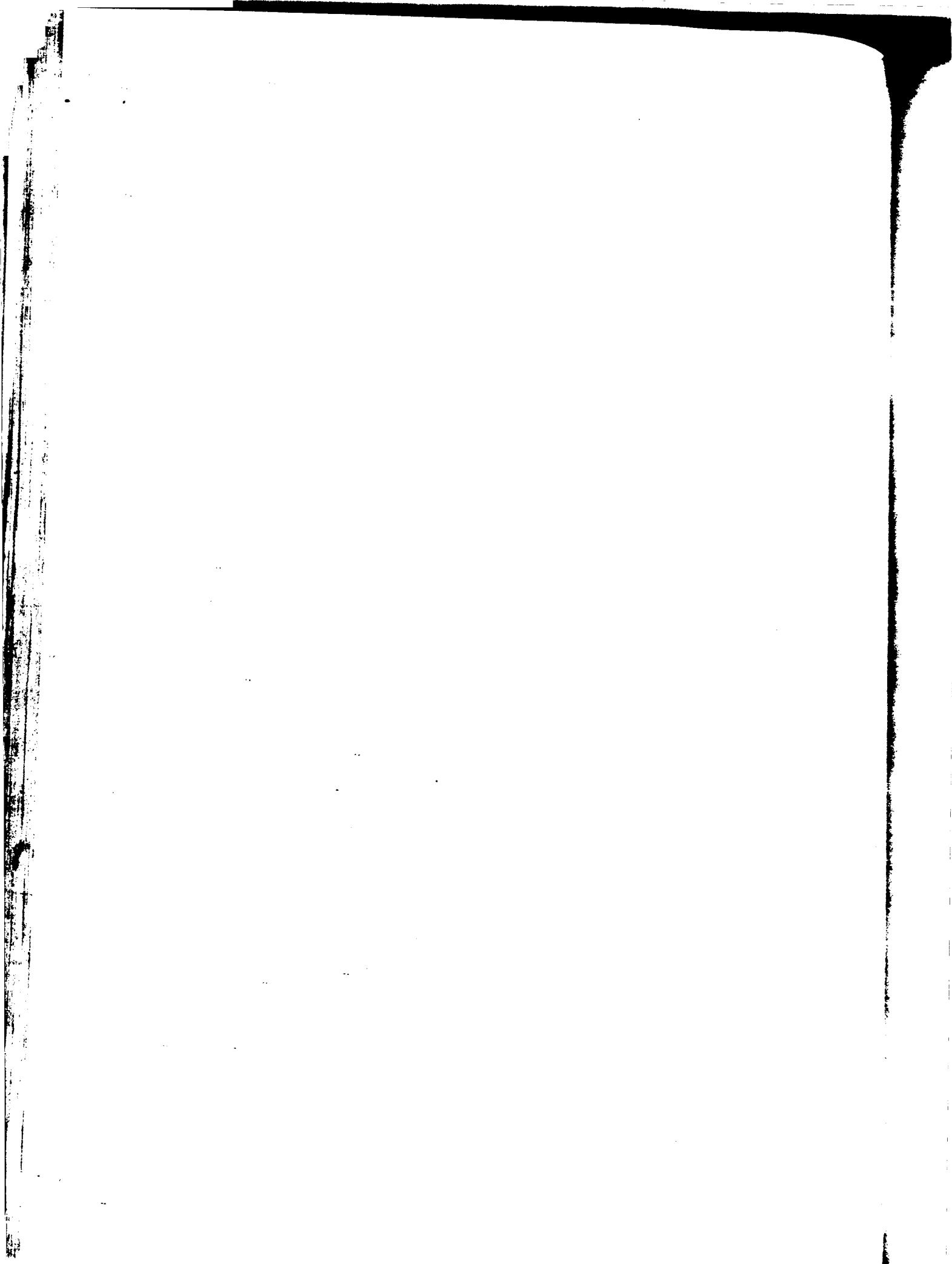
SONDAGES DES SILLAGES

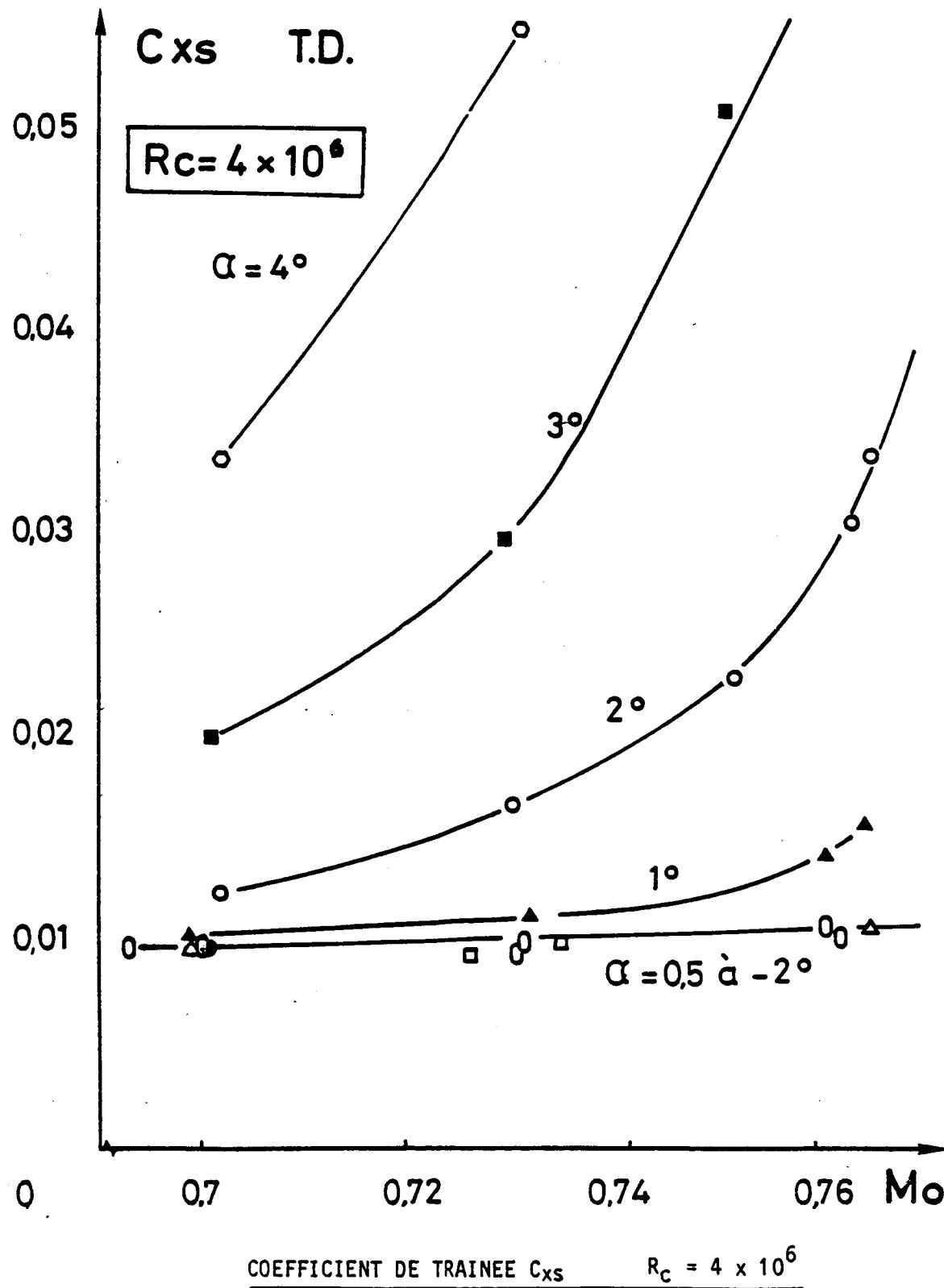
T.D.

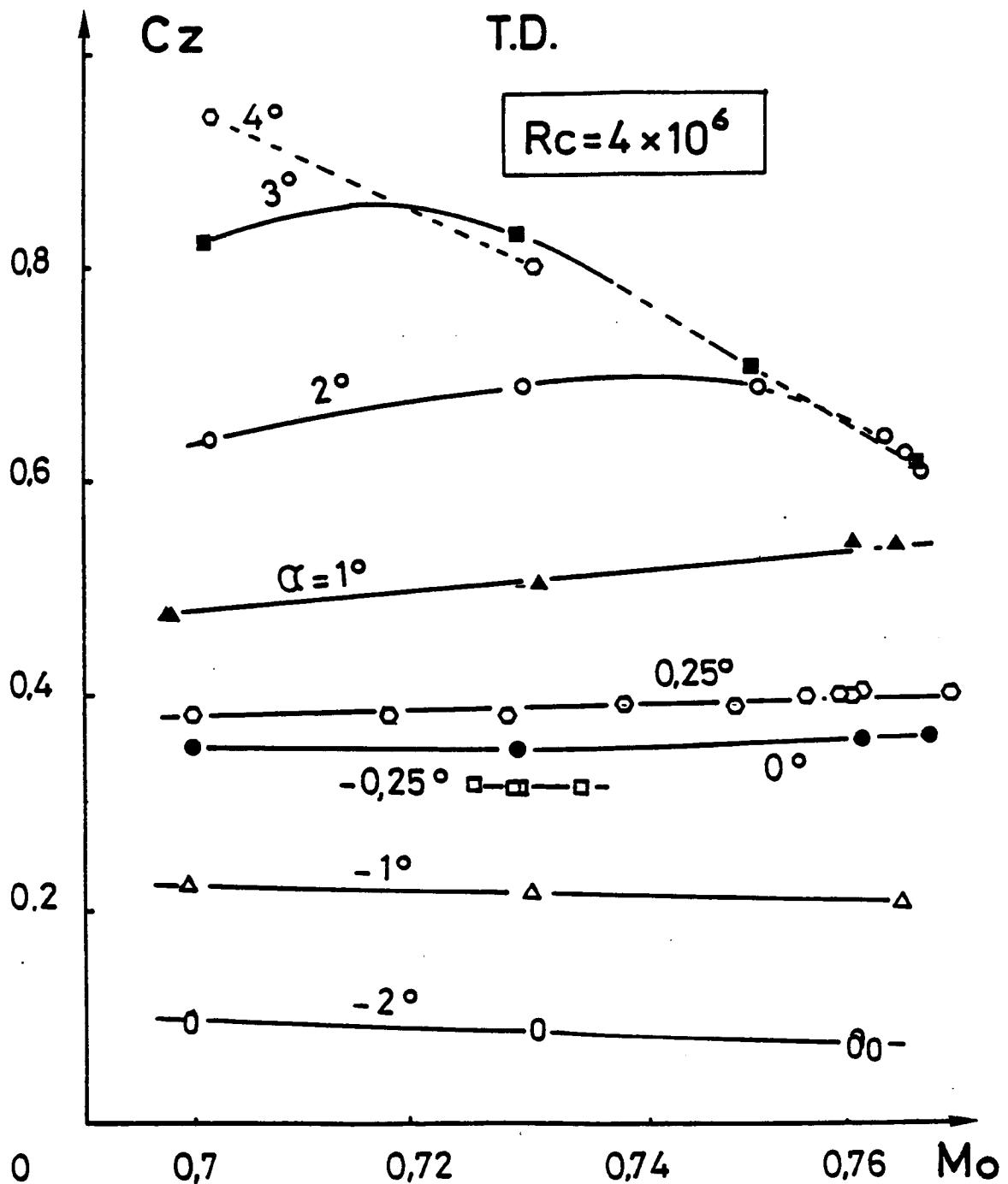
COEFFICIENTS AÉRODYNAMIQUES EN FONCTION DU NOMBRE DE MACH

$$R_C = 4 \cdot 10^6$$

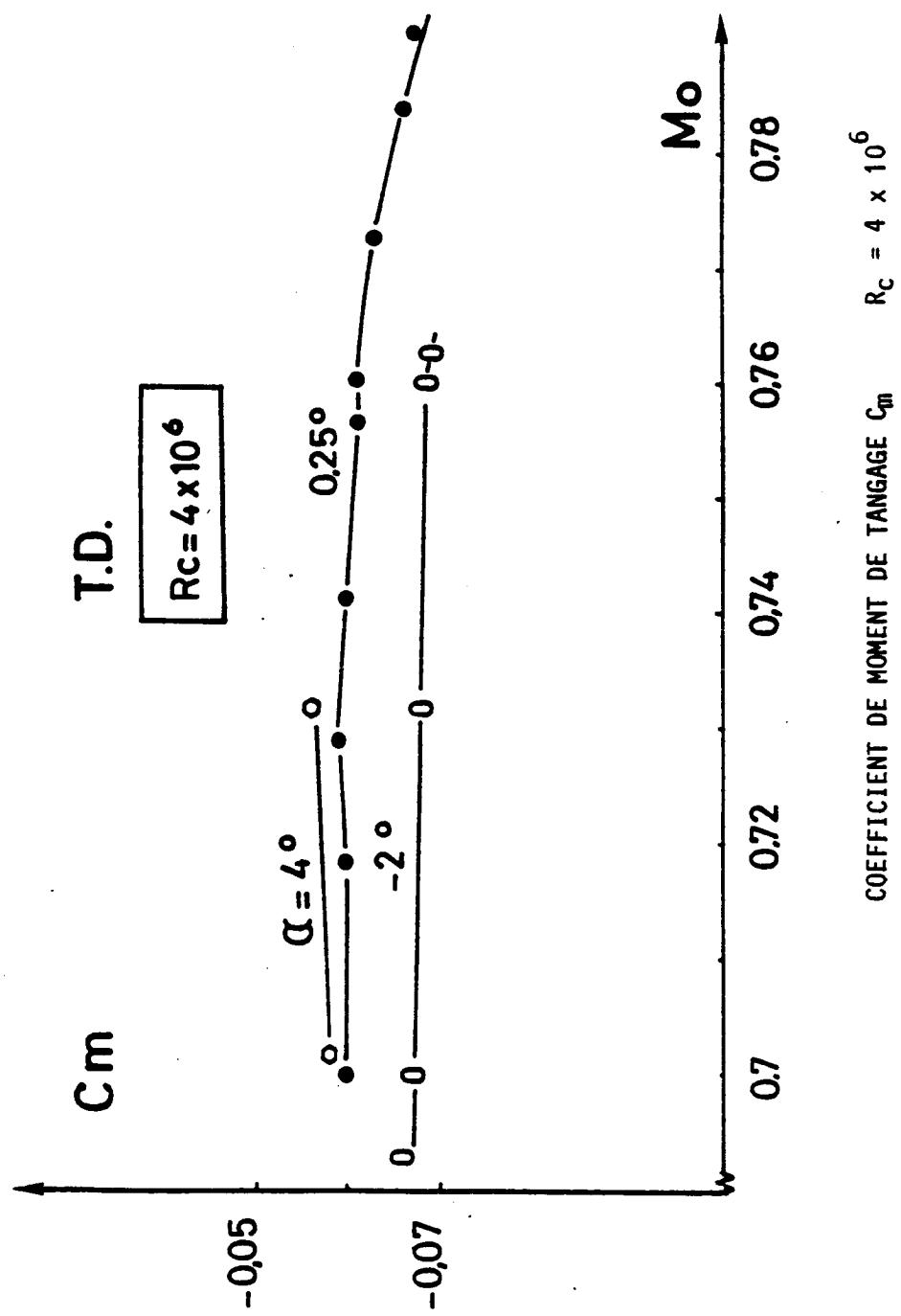
$C_{xs} (M_o)$	PL. 84
$C_z (M_o)$	PL. 85
$C_m (M_o)$	PL. 86





COEFFICIENT DE PORTANCE C_z $R_c = 4 \times 10^6$

PL. 86

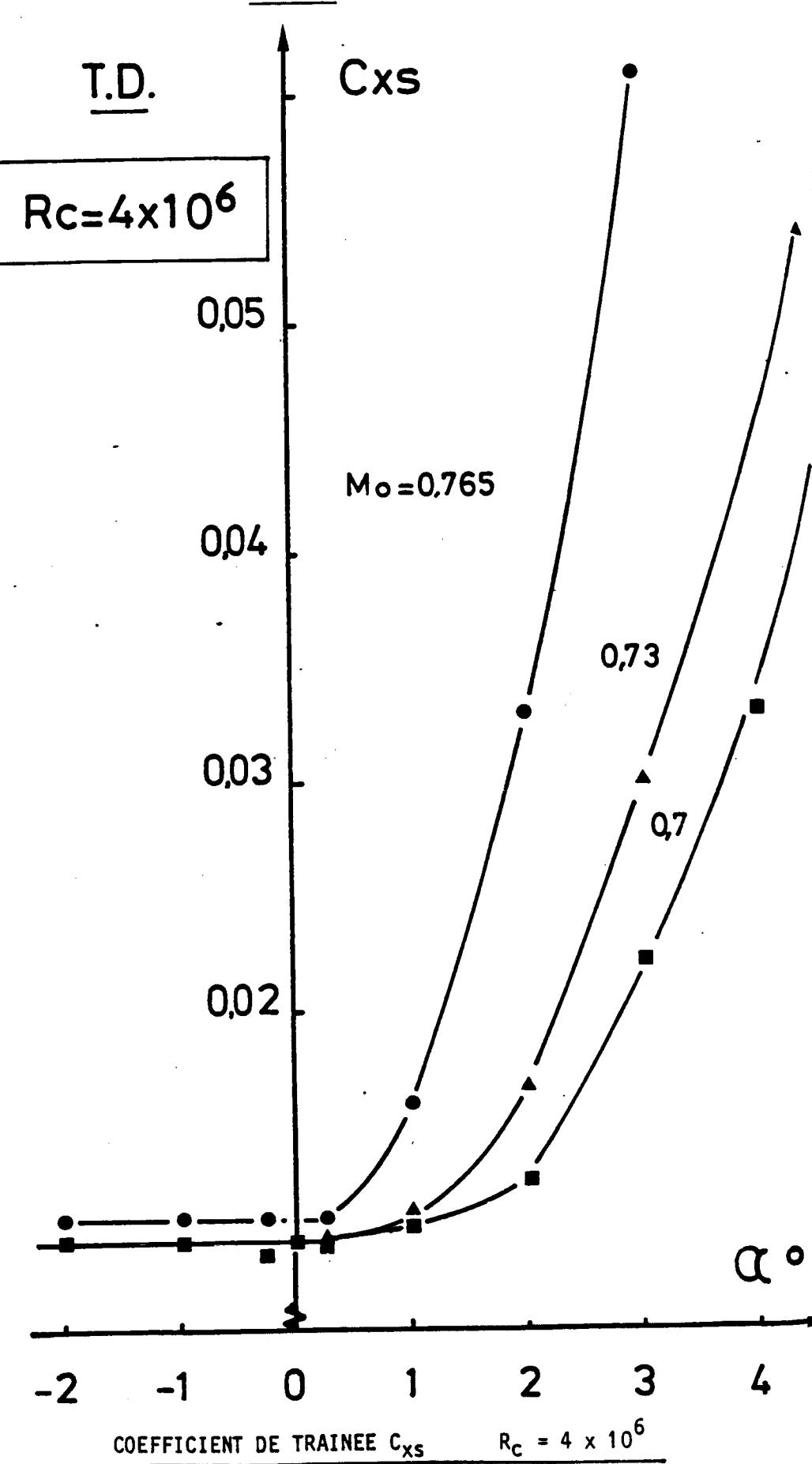


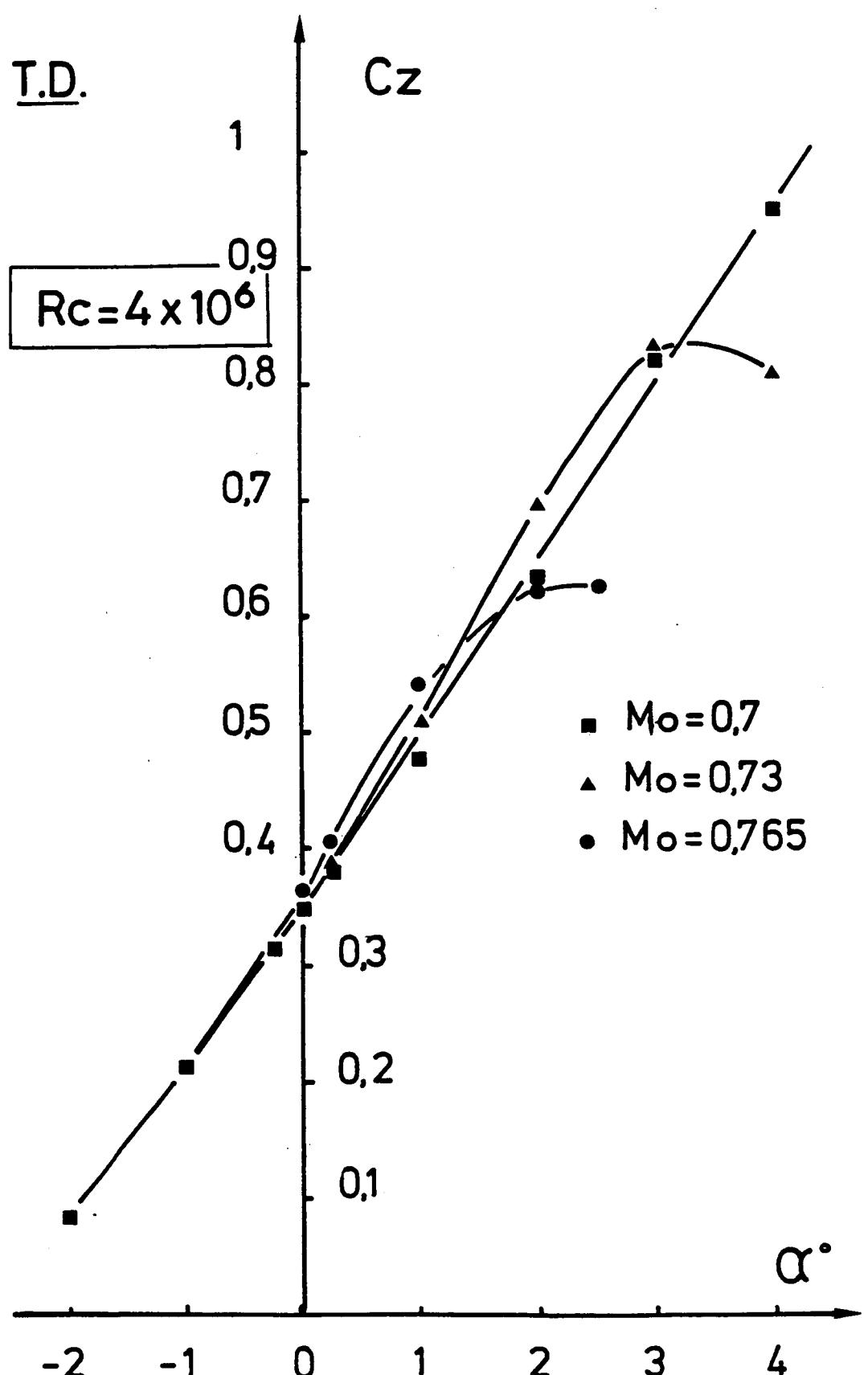
T.D.

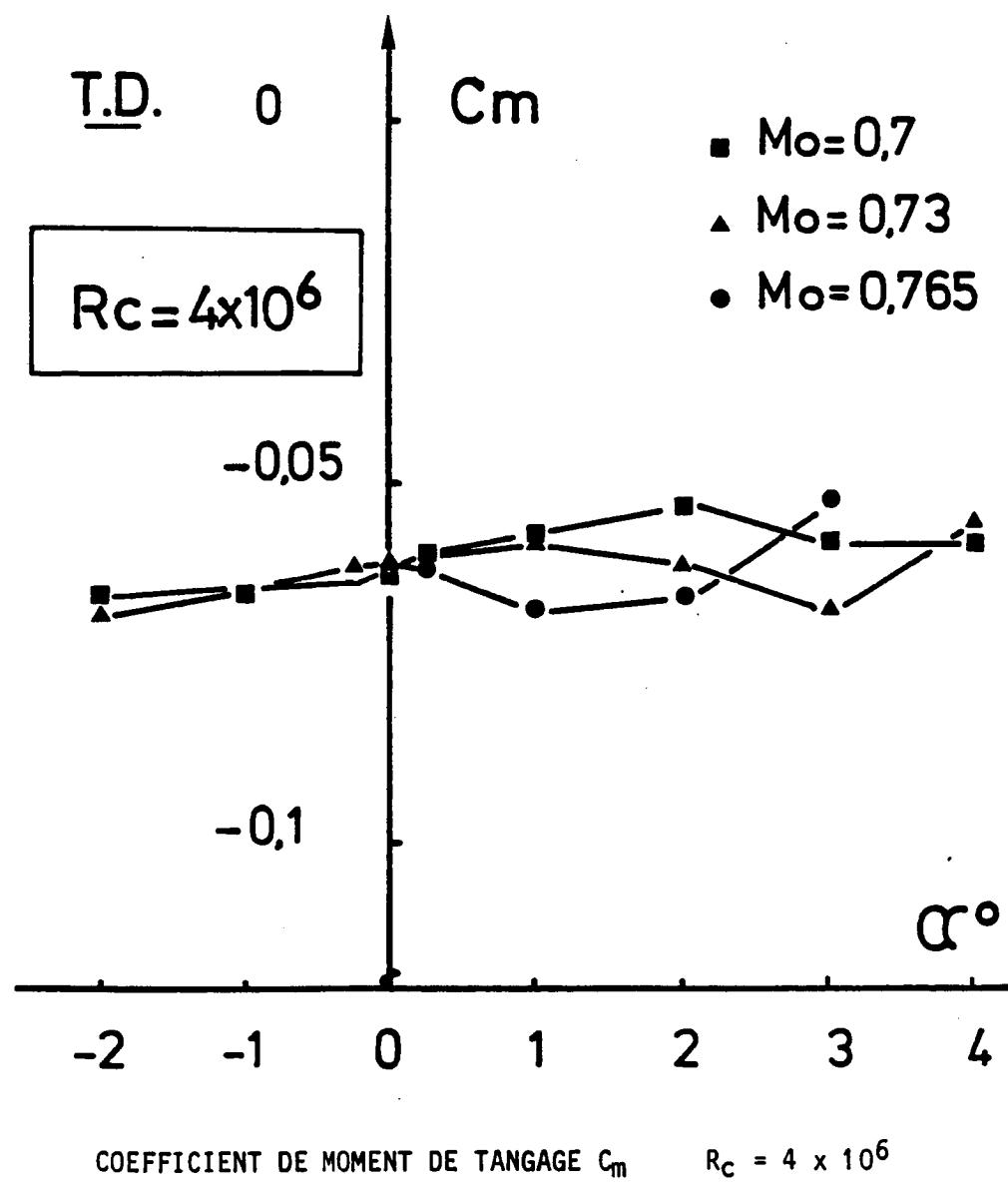
COEFFICIENTS AERODYNAMIQUES EN FONCTION DE L'INCIDENCE

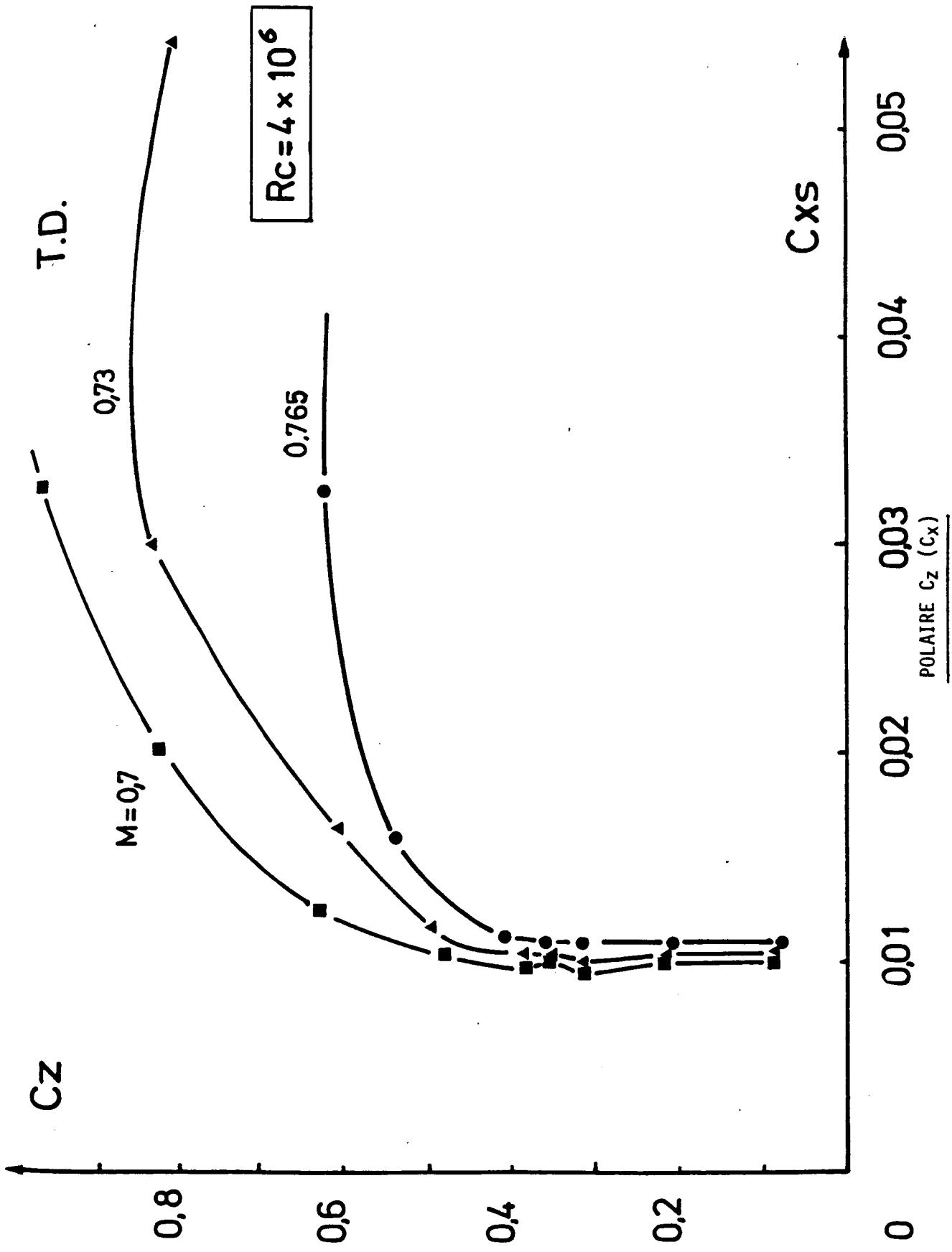
$$R_C = 4 \cdot 10^6$$

C_{xs} (α)	PL. 87
C_z (α)	PL. 88
C_m (α)	PL. 89
Polaire C_z (C_x)	PL. 90



T.D.





T.D.

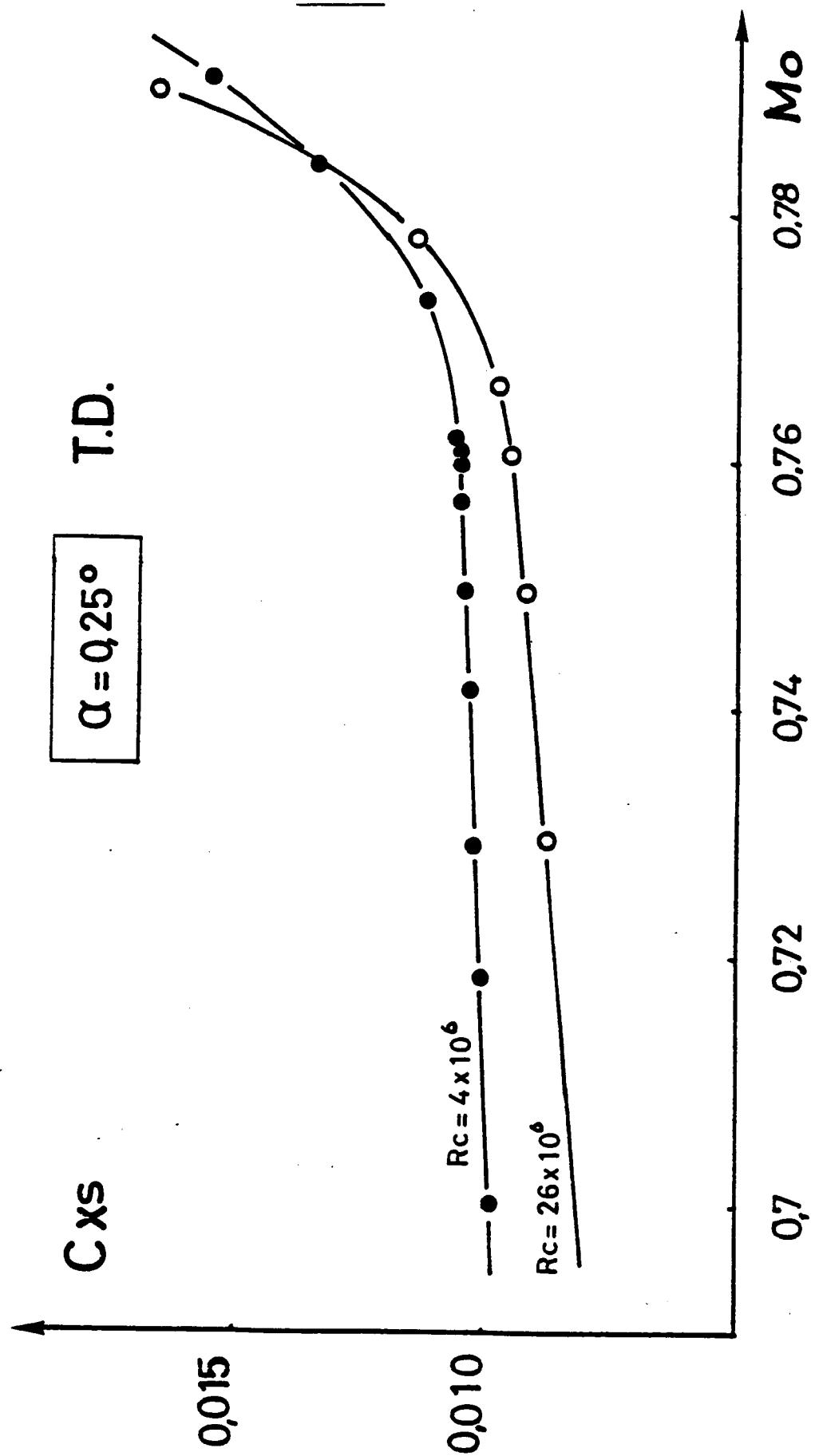
EVOLUTION DES COEFFICIENTS AERODYNAMIQUES EN FONCTION DU NOMBRE DE MACH

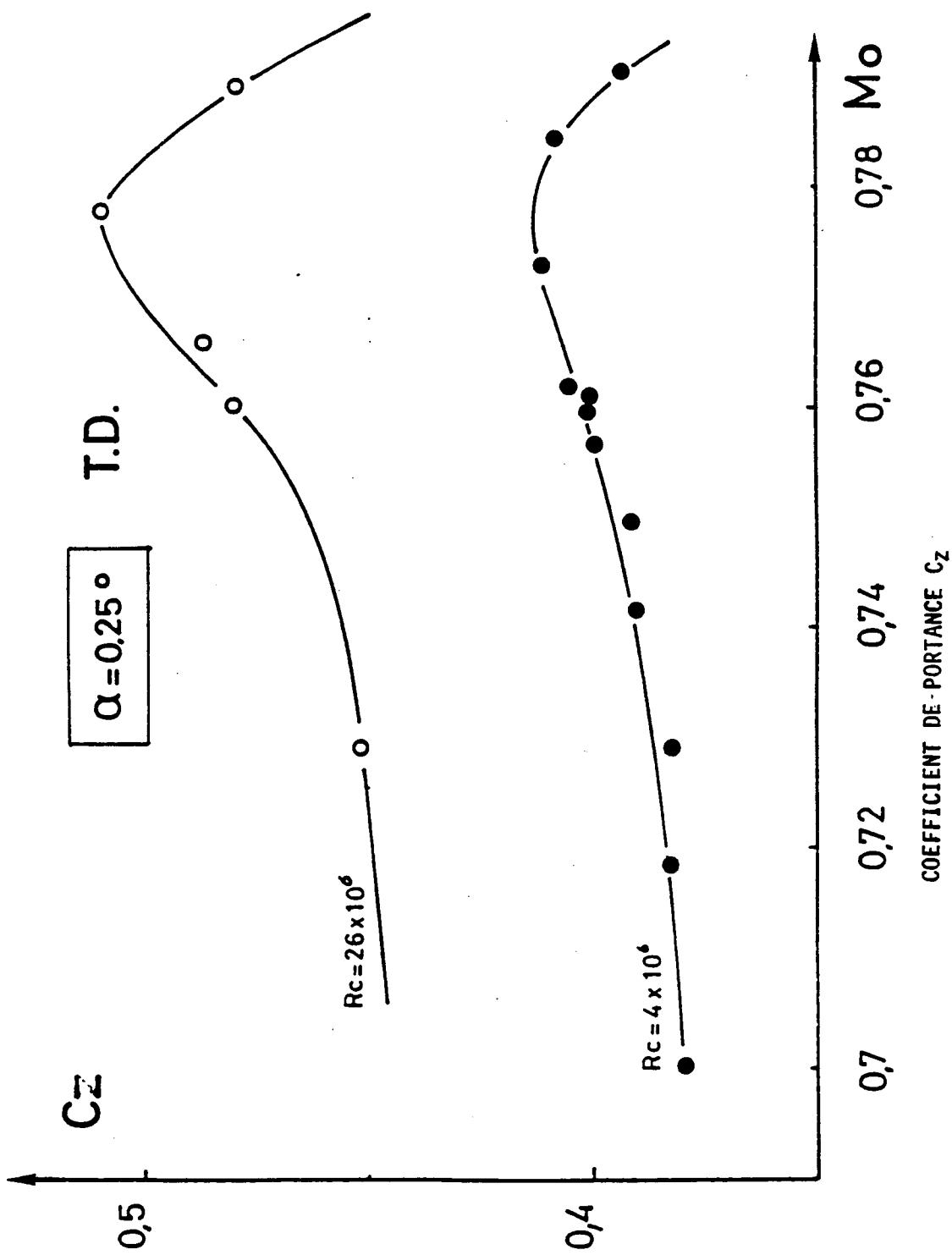
$\alpha = + 0,25^\circ$
pour
 $R_C = 4 \cdot 10^6$ et $R_C = 26 \cdot 10^6$

$C_{xs} (M_\infty)$ PL. 91

$C_z (M_\infty)$ PL. 92

PL. 91





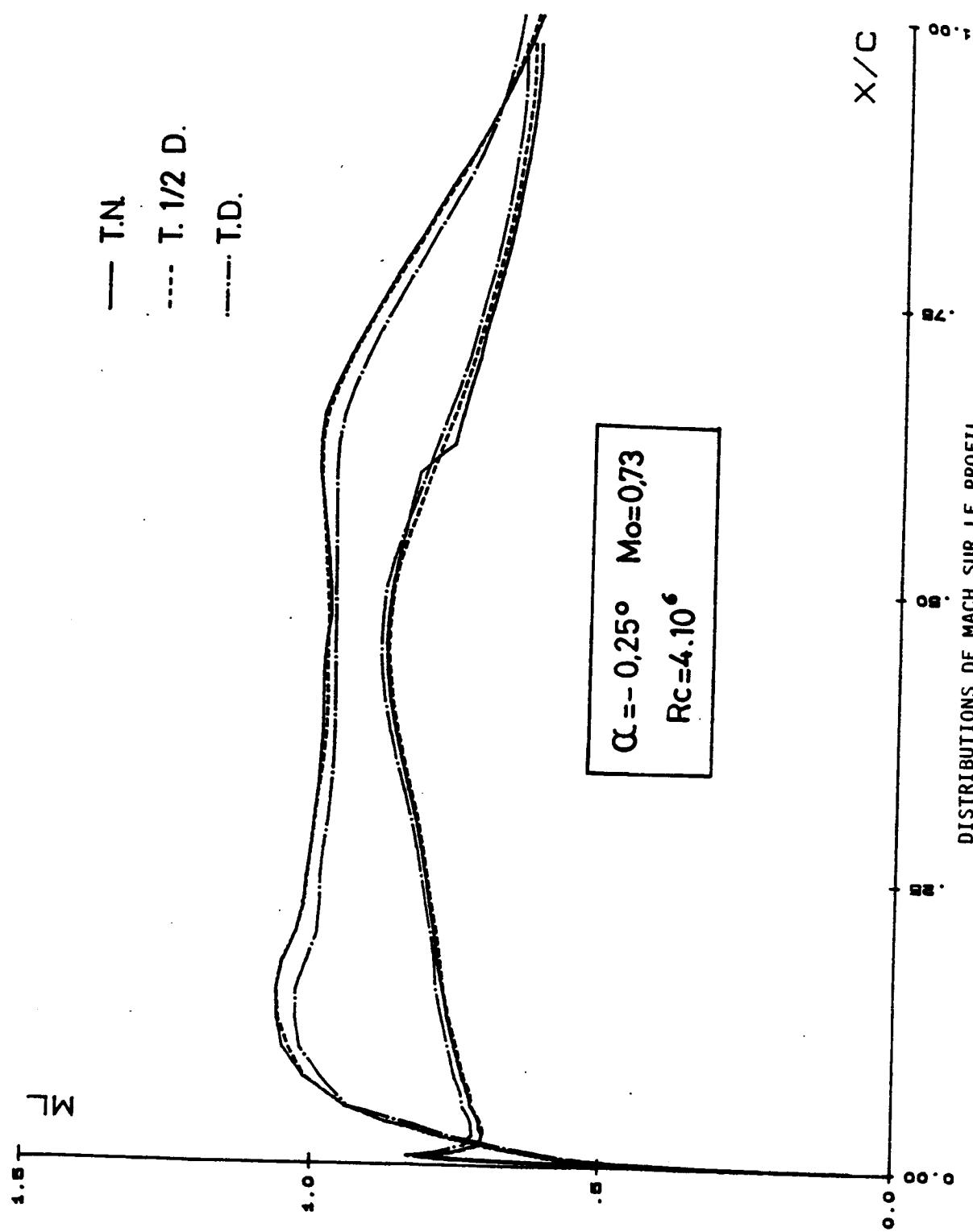
**EFFETS
DU NOMBRE DE REYNOLDS
COMPARATIVEMENT
T.N. T.1/2D. T.D.**

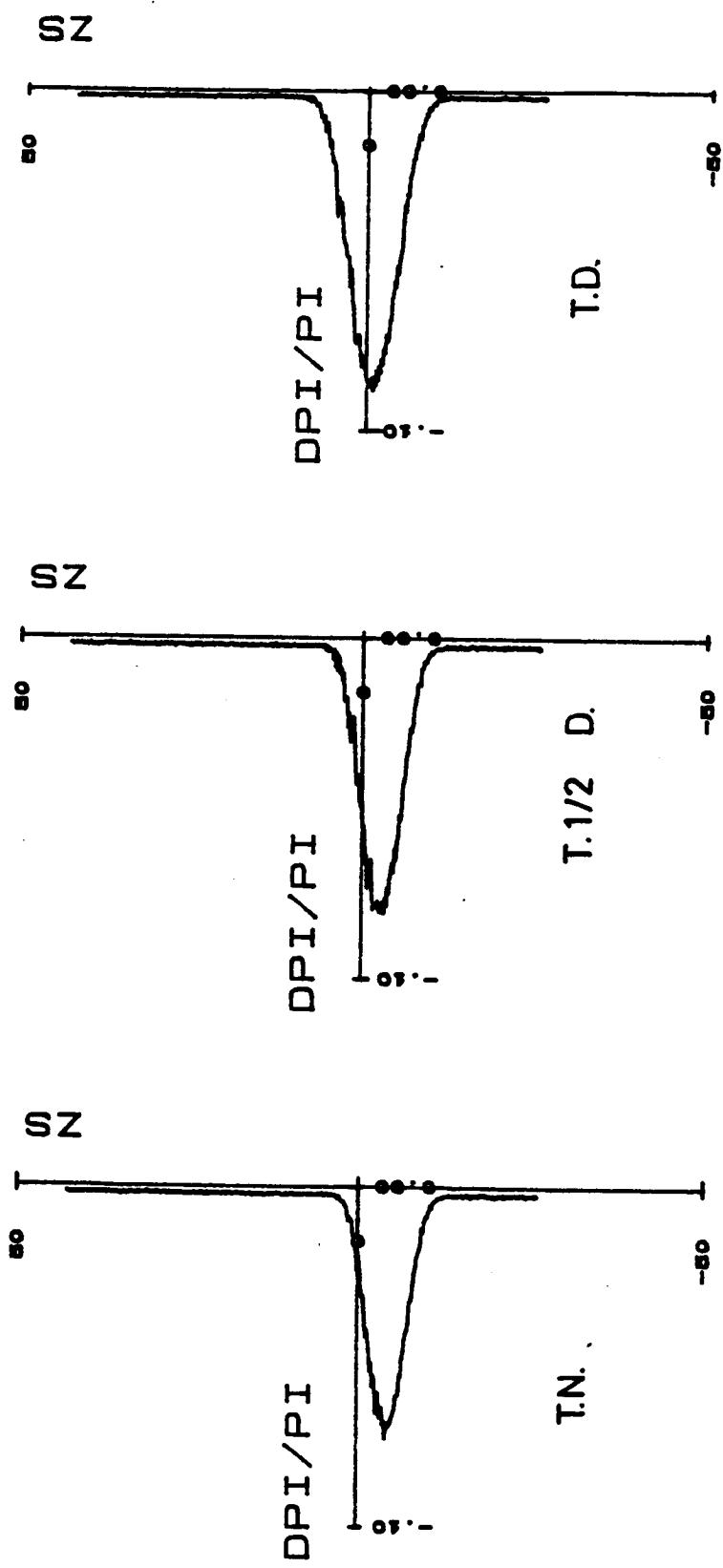
PLANCHES 93 à 122

COMPARAISONS T.N. - T. 1/2 D. - T.D.

DISTRIBUTIONS DE MACH ET DE SILLAGES

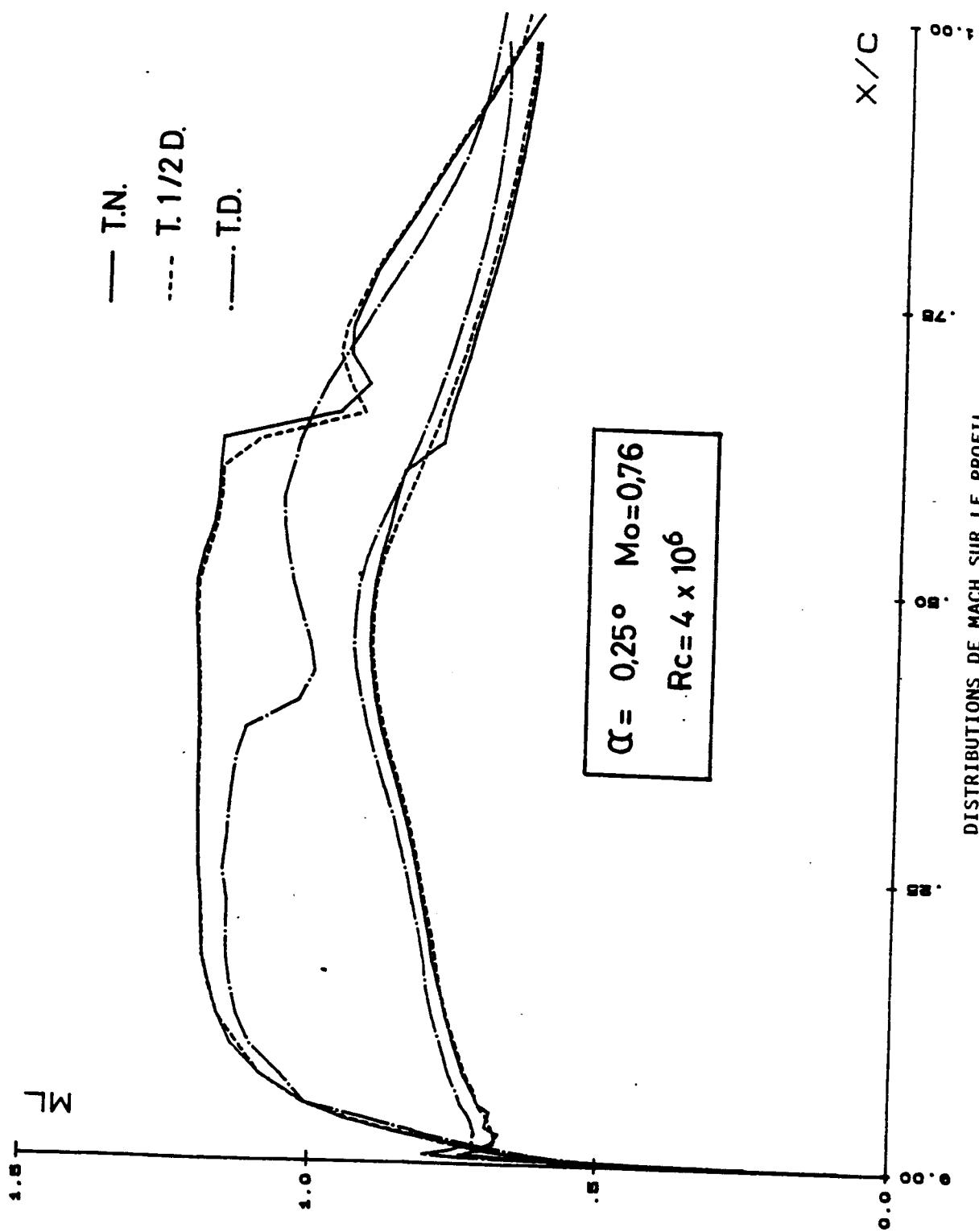
$M_o = 0,73$ et $\alpha = - 0,25^\circ$	$R_C = 4 \cdot 10^6$	PL. 93 et 94
$M_o = 0,76$ et $\alpha = + 0,25^\circ$	$R_e = 4 \cdot 10^6$	PL. 95 et 96
$M_o = 0,76$ et $\alpha = + 0,25^\circ$	$R_C = 7,8 \cdot 10^6$	PL. 97 et 98
$M_o = 0,76$ et $\alpha = + 0,25^\circ$	$R_C = 13 \cdot 10^6$	PL. 99 et 100
$M_o = 0,765$ et $\alpha = + 0,25^\circ$	$R_C = 25 \cdot 10^6$	PL. 101

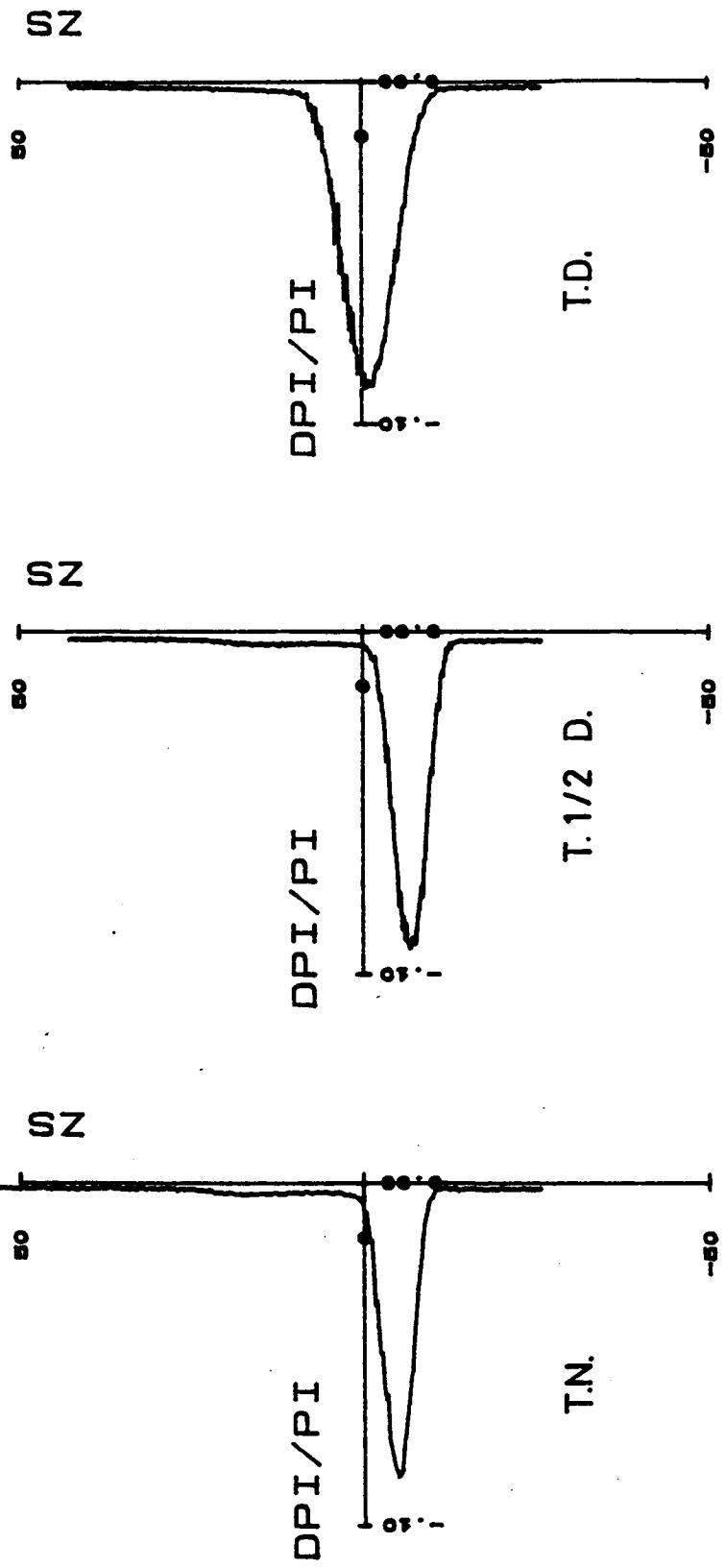




$M_o = 0.73 \quad \Omega = -025^\circ \quad R_c = 4 \times 10^6$

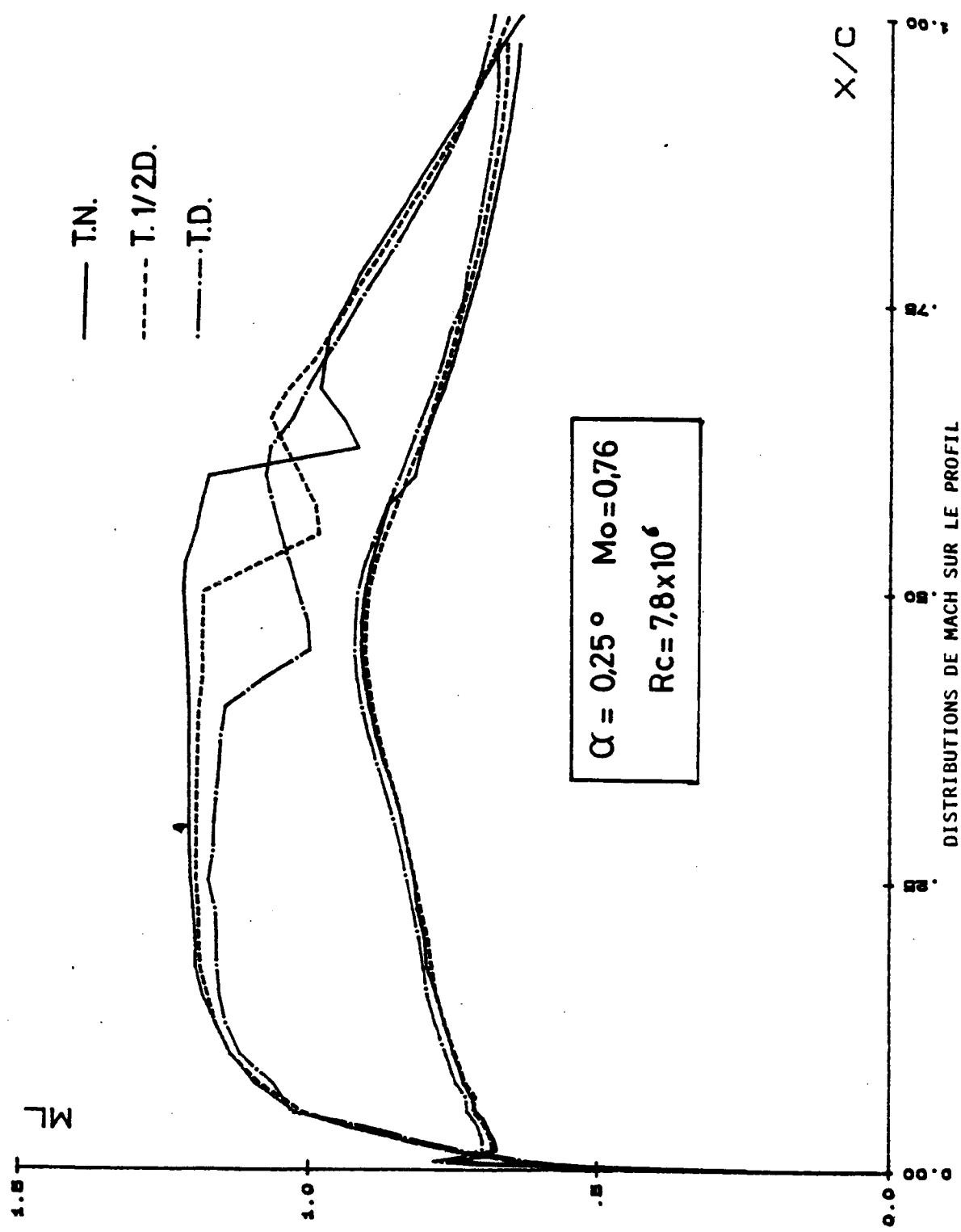
SONDAGES DES SILLAGES

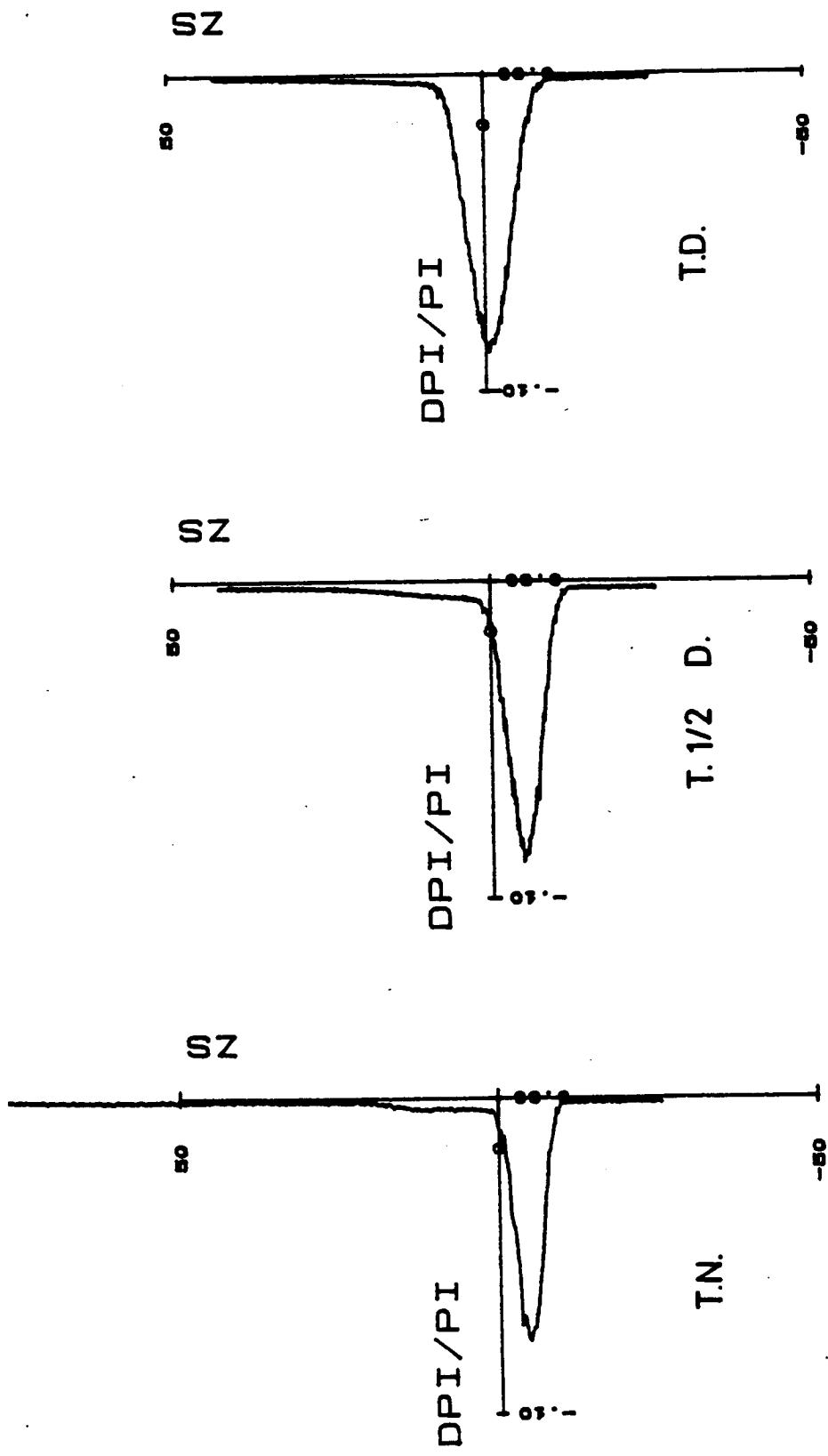




$Mo=0,76 \quad \alpha=0,25^\circ \quad Rc=4 \times 10^6$

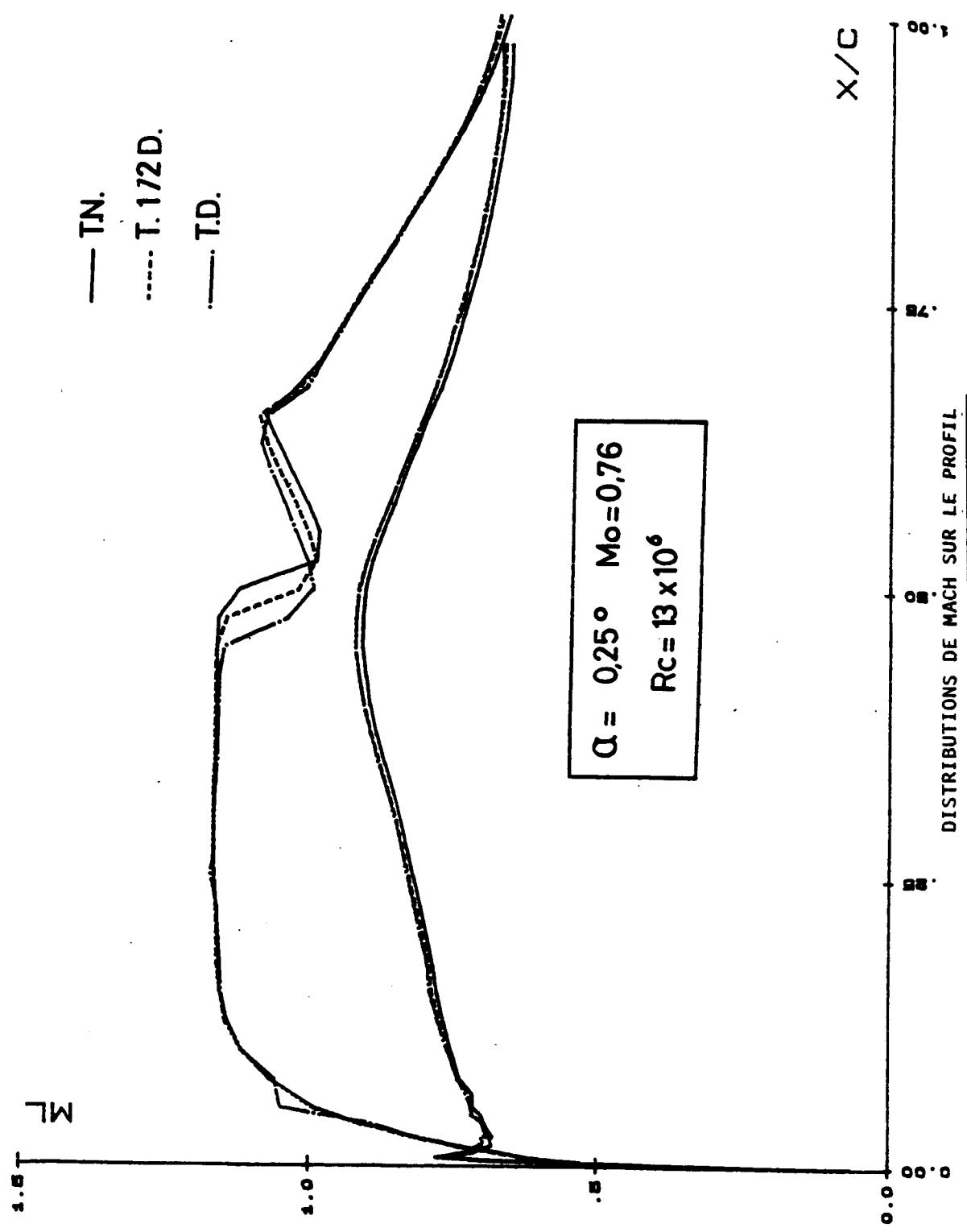
SONDAGES DES SILLAGES

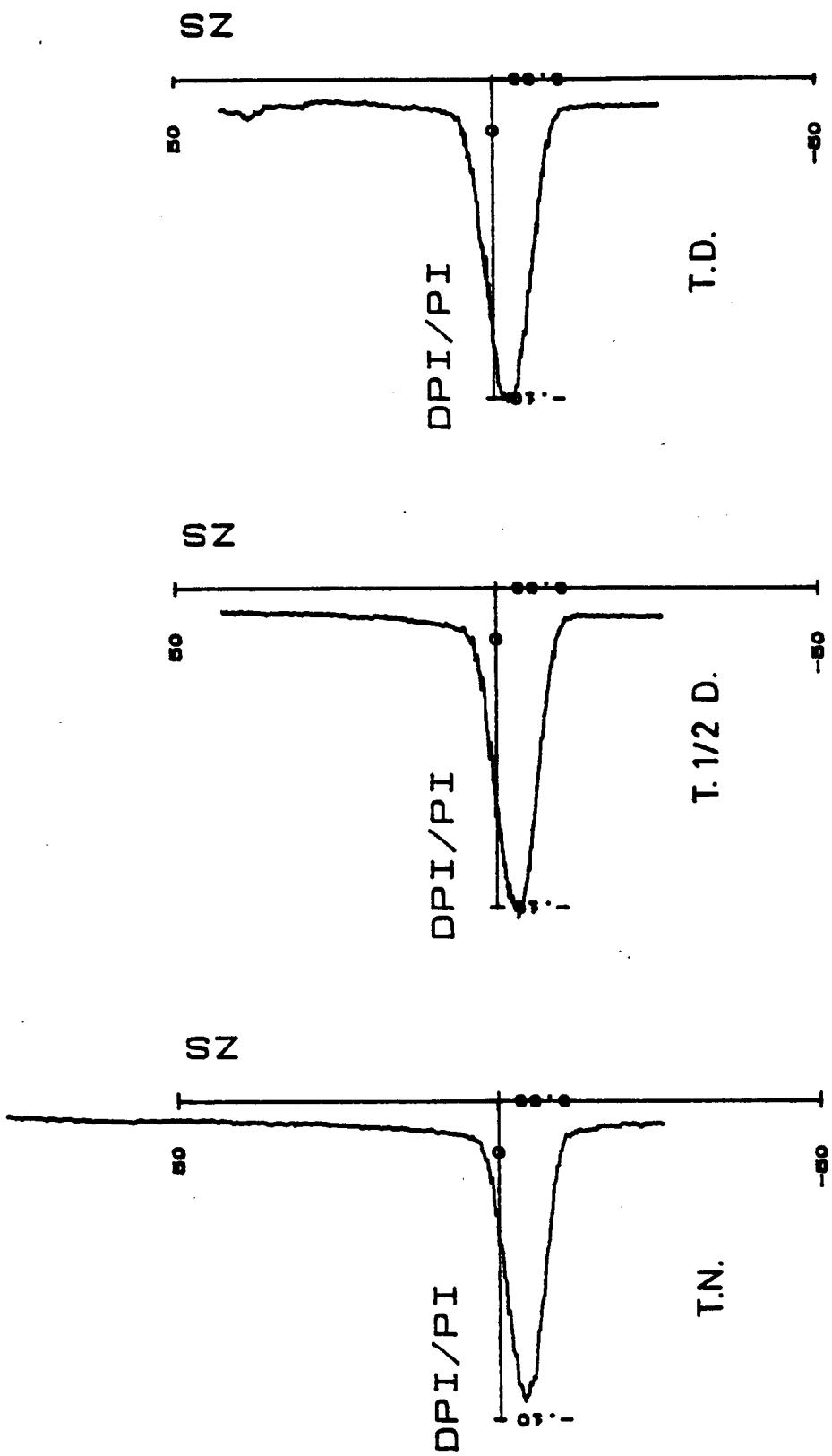




$M_0 = 0.76 \quad \alpha = 0.25^\circ \quad R_c = 7.8 \times 10^6$

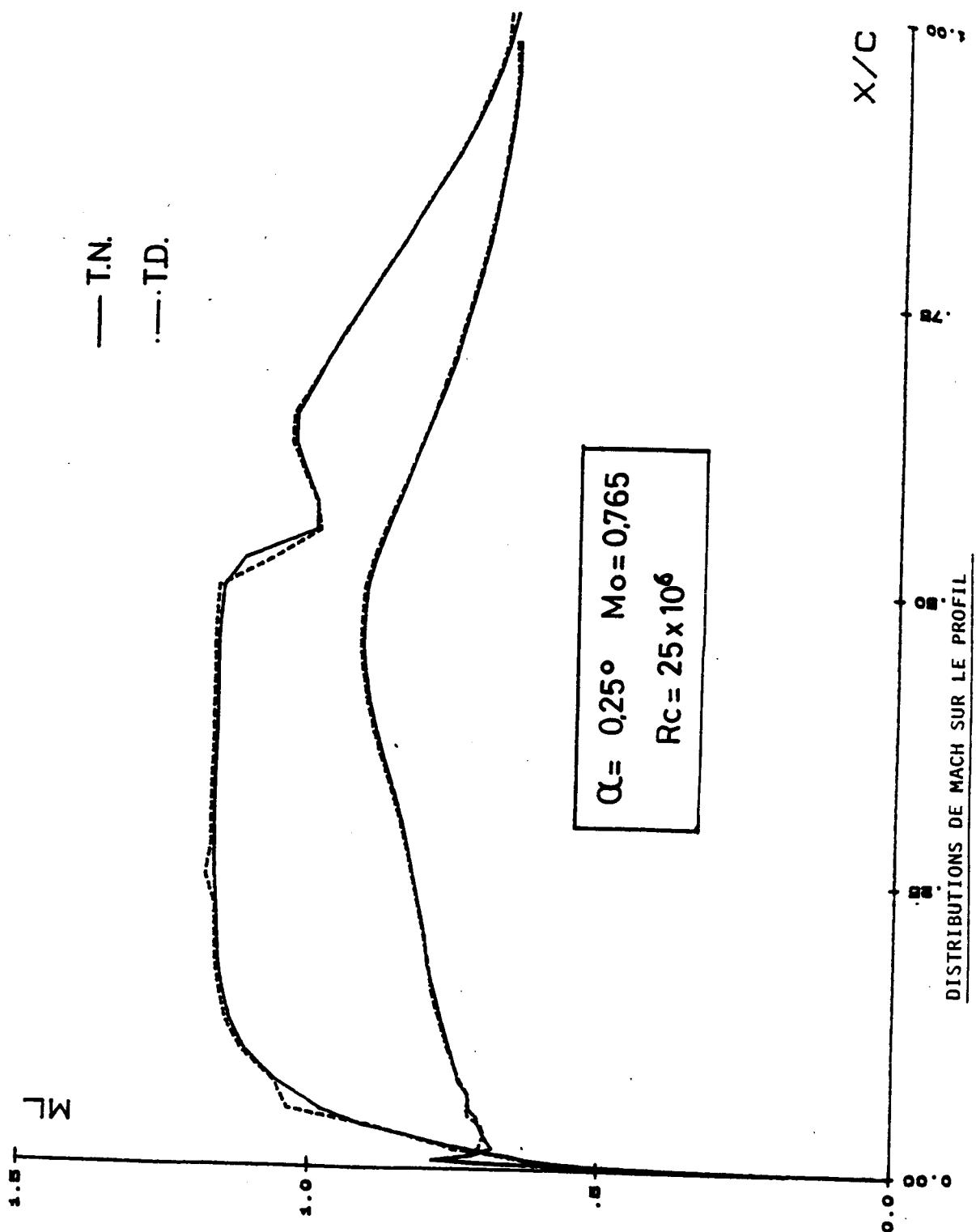
SONDAGES DES SILLAGES





$M_0 = 0,76 \quad \alpha = 0,25^\circ \quad R_c = 13 \times 10^6$

SONDAGES DES SILLAGES



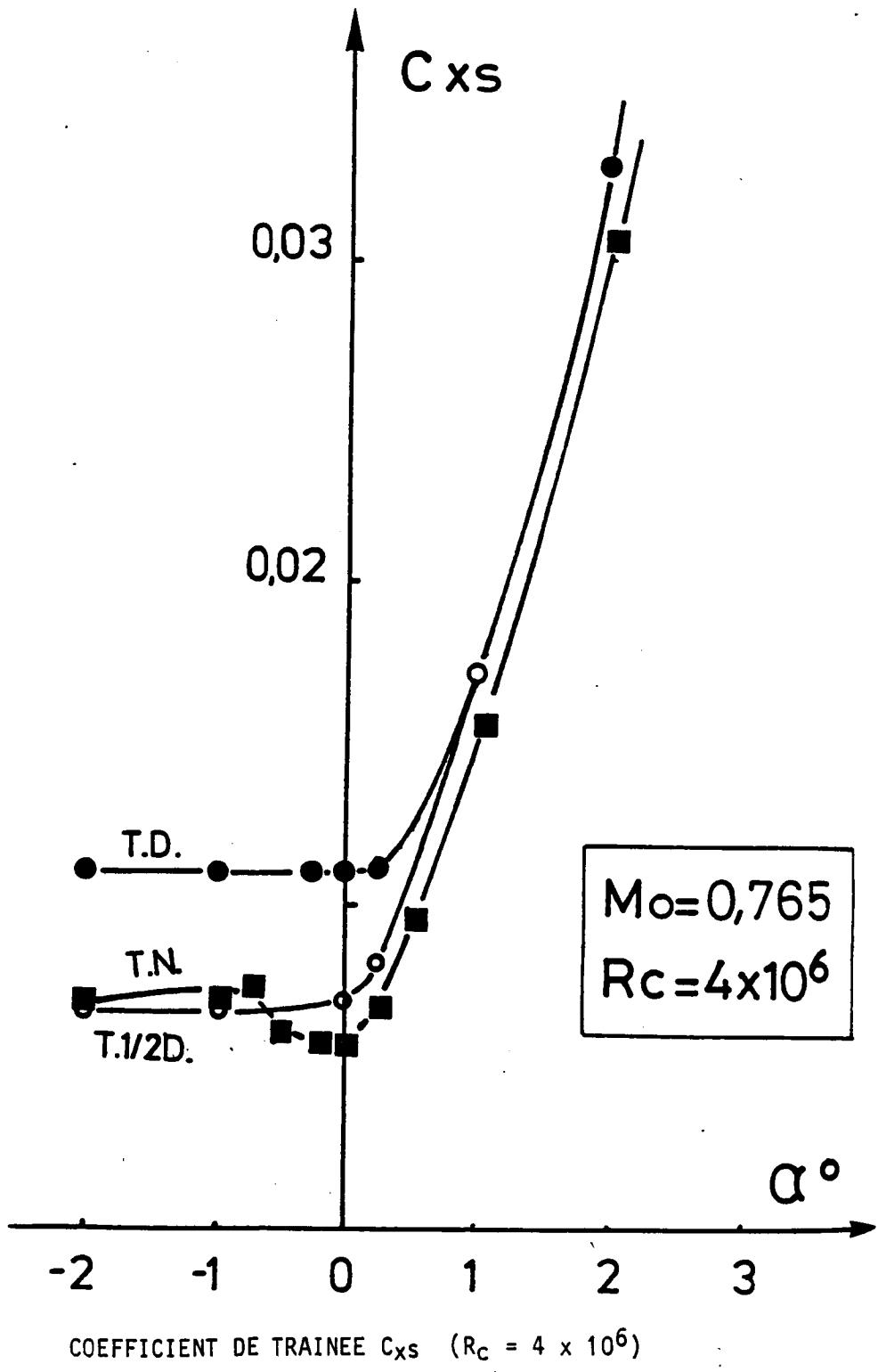
COMPARAISONS T.N. - T. 1/2 D. - T.D.

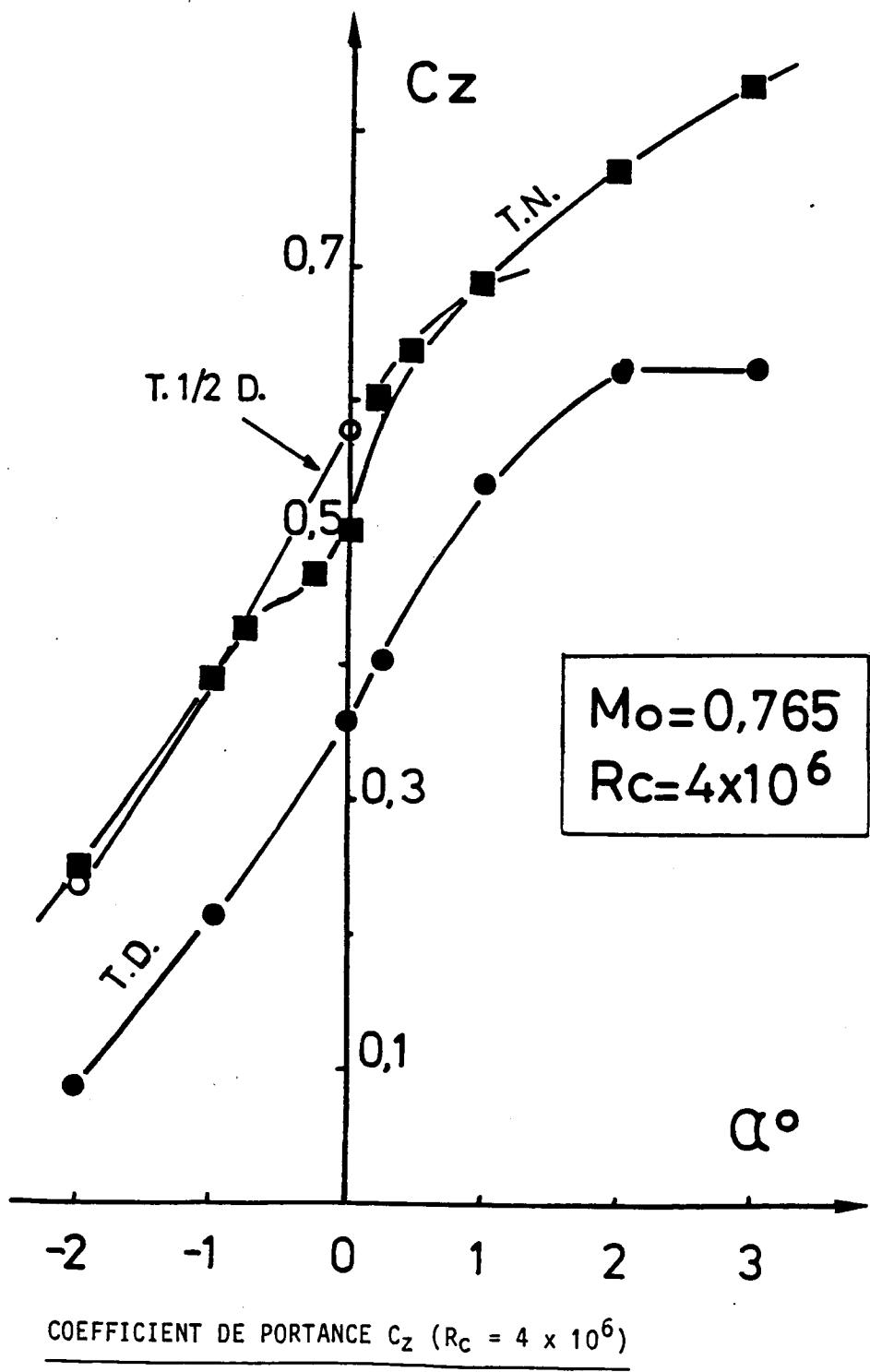
COEFFICIENTS AERODYNAMIQUES

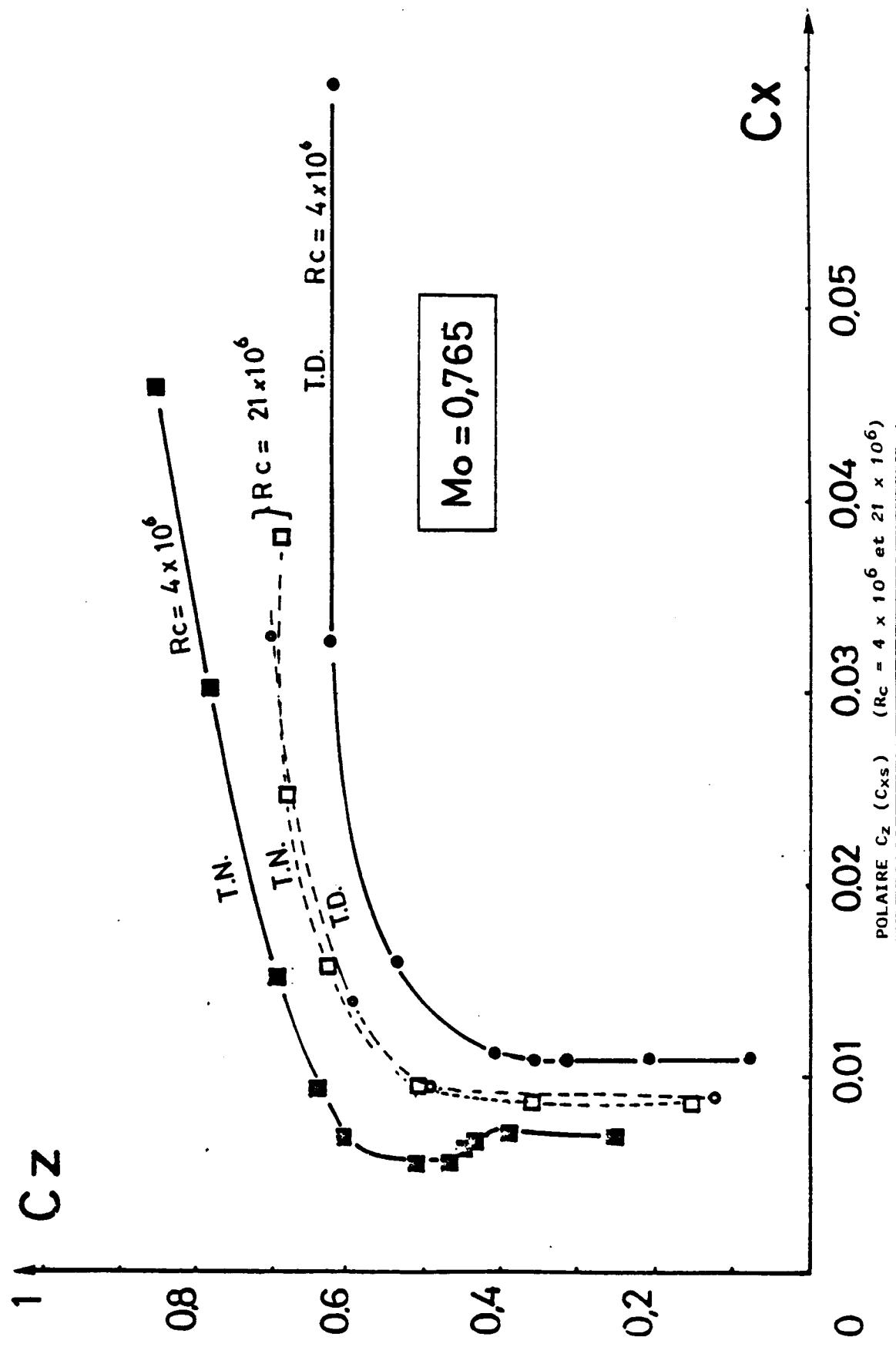
$C_{xs} (\alpha)$ à $R_C = 4 \cdot 10^6$ PL. 102

$C_z (\alpha)$ à $R_C = 4 \cdot 10^6$ PL. 103

Polaire à $R_C = 4 \cdot 10^6$ et $21 \cdot 10^6$ PL. 104





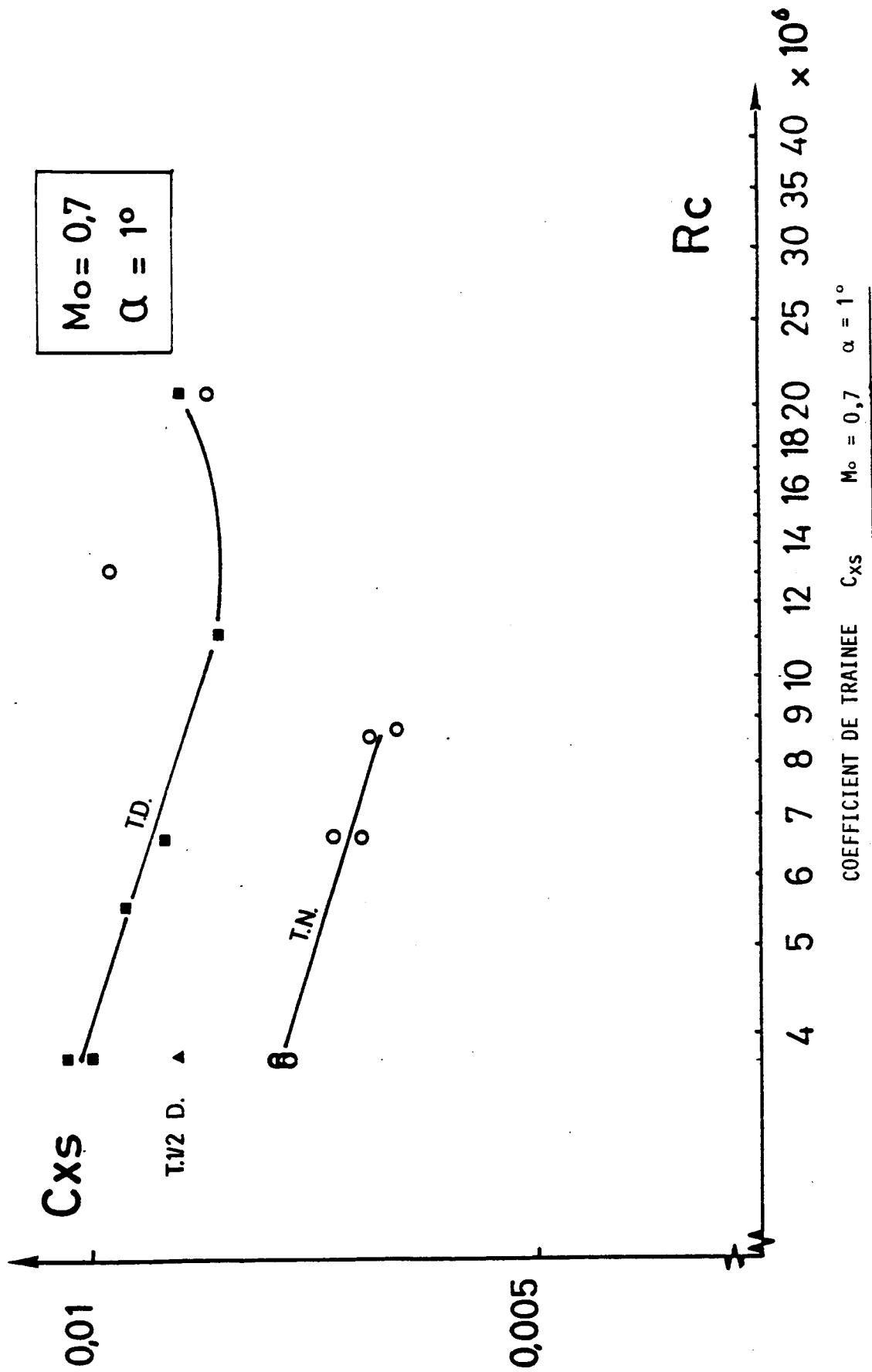


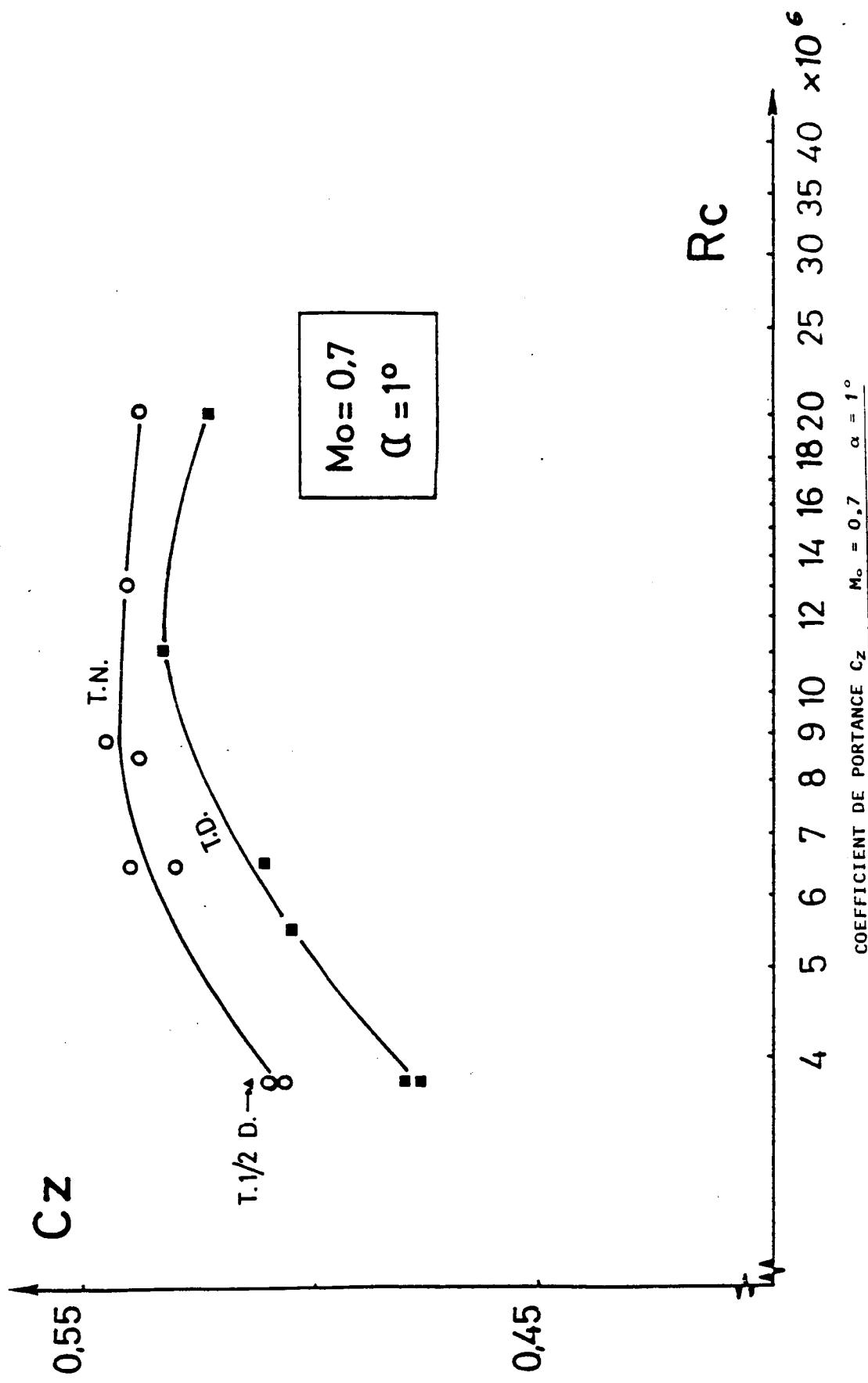
COMPARAISONS T.N. - T. 1.2 D. - T.D.

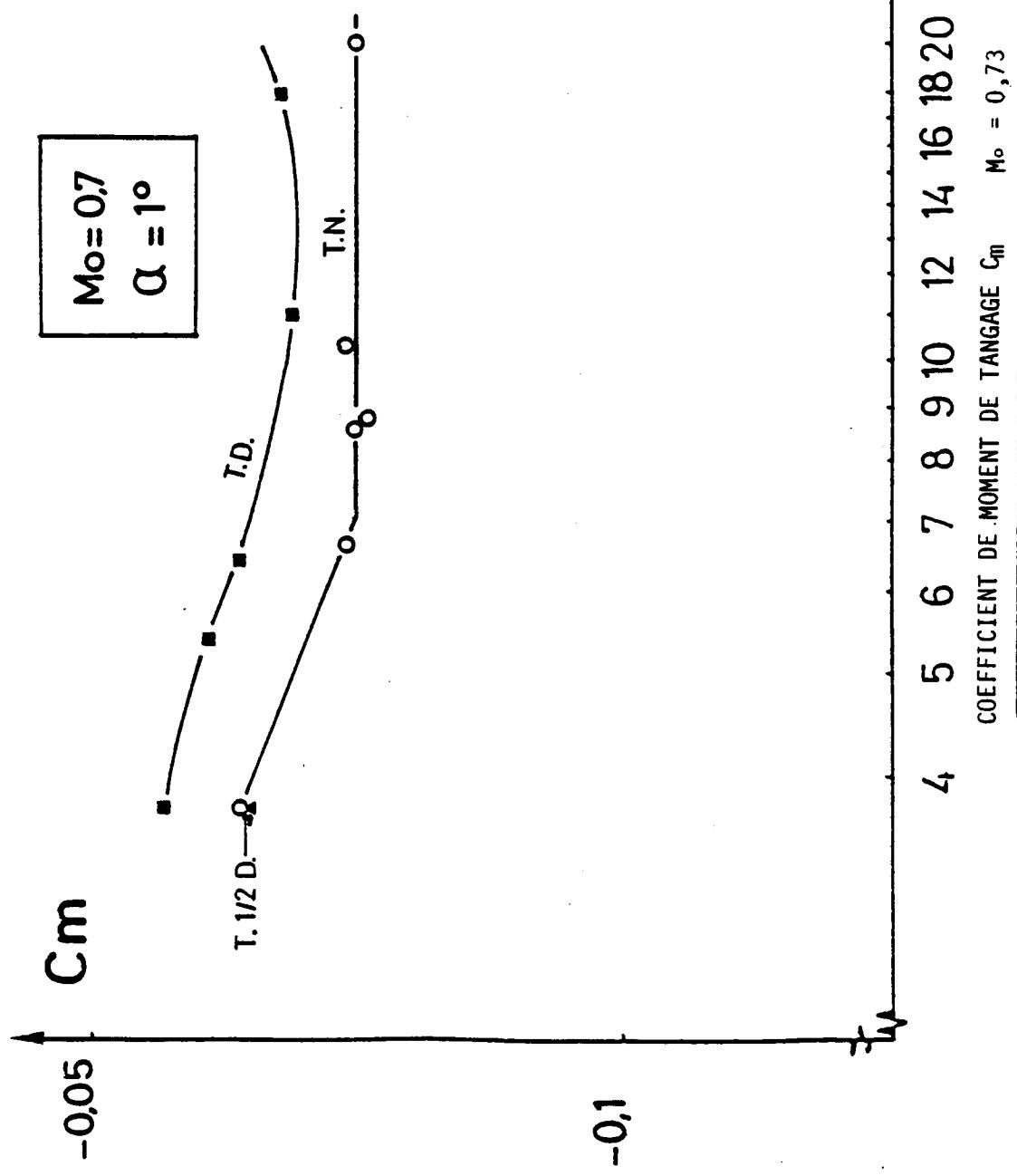
EVOLUTIONS DES COEFFICIENTS AERODYNAMIQUES EN FONCTION DU NOMBRE DE REYNOLDS

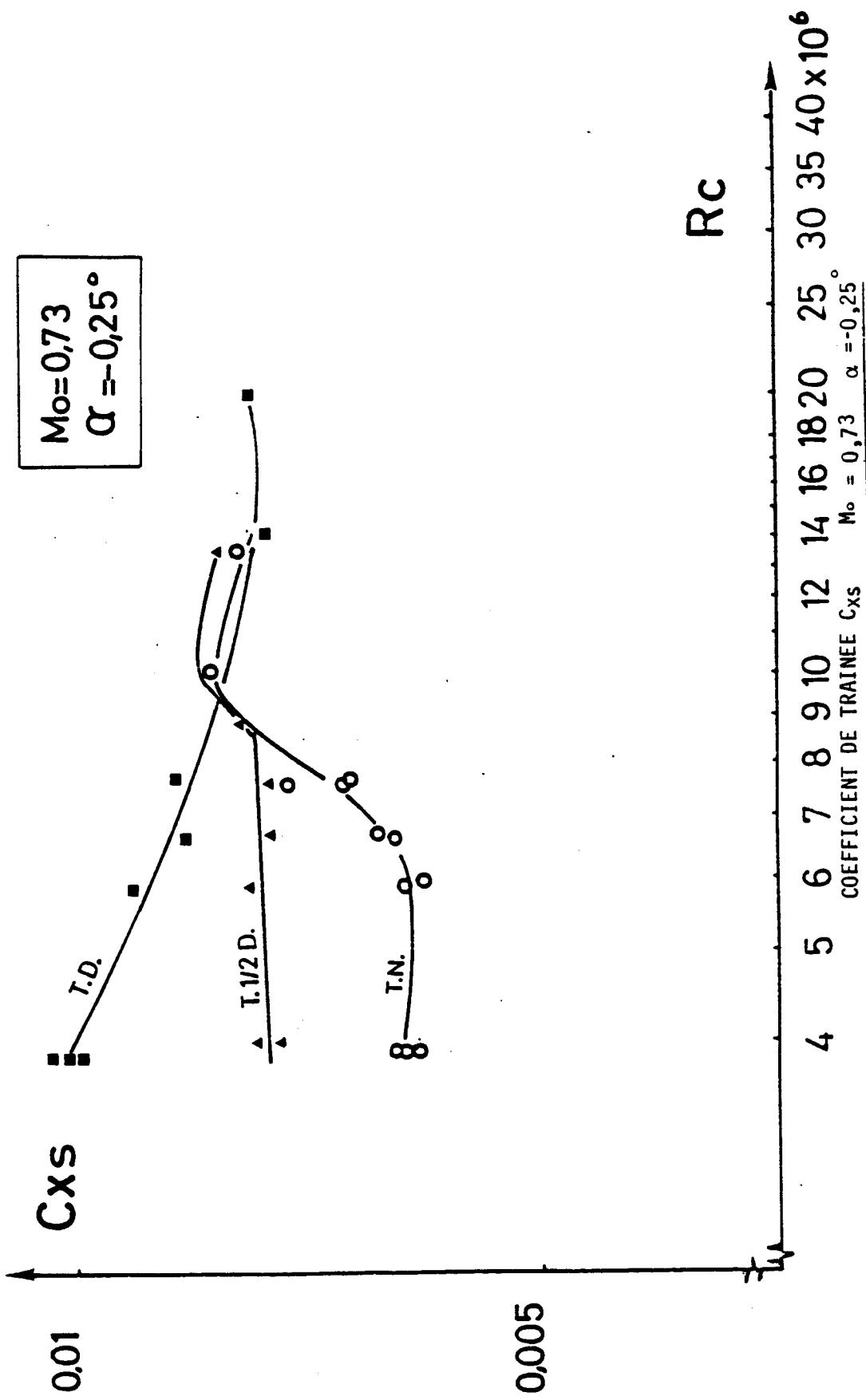
$C_{xs}(R_c)$, $C_z(R_c)$, $C_m(R_c)$

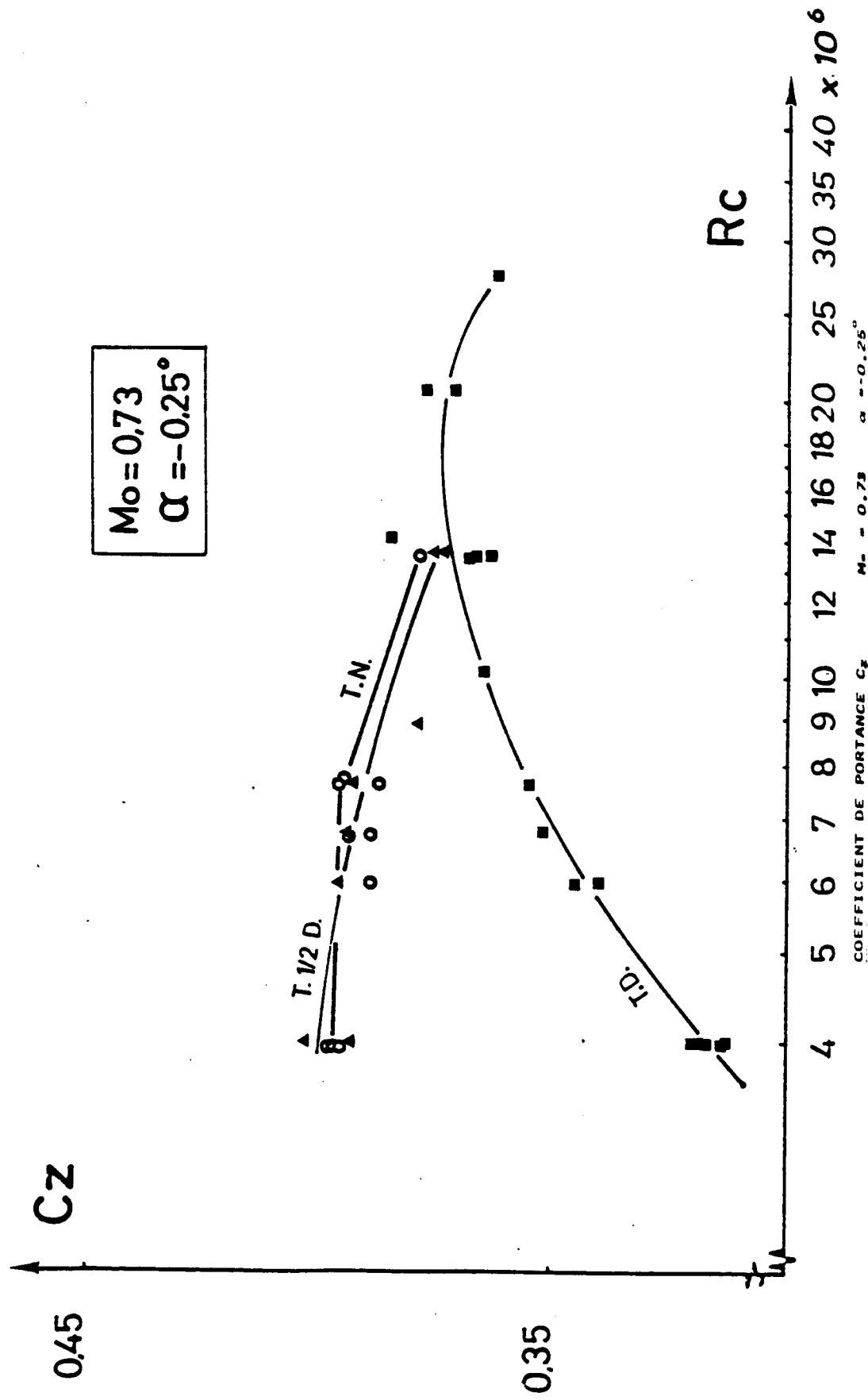
$M_\infty = 0,7$ et $\alpha = + 1^\circ$	PL. 105 à 107
$M_\infty = 0,73$ et $\alpha = - 0,25^\circ$	PL. 108 à 110
$M_\infty = 0,76$ et $\alpha = + 0,25^\circ$	PL. 111 à 113
$M_\infty = 0,76$ et $\alpha = + 1^\circ$	PL. 114 à 116
$M_\infty = 0,765$ et $\alpha = - 2^\circ$	PL. 117 à 119
$M_\infty = 0,765$ et $\alpha = + 2^\circ$	PL. 120 à 122



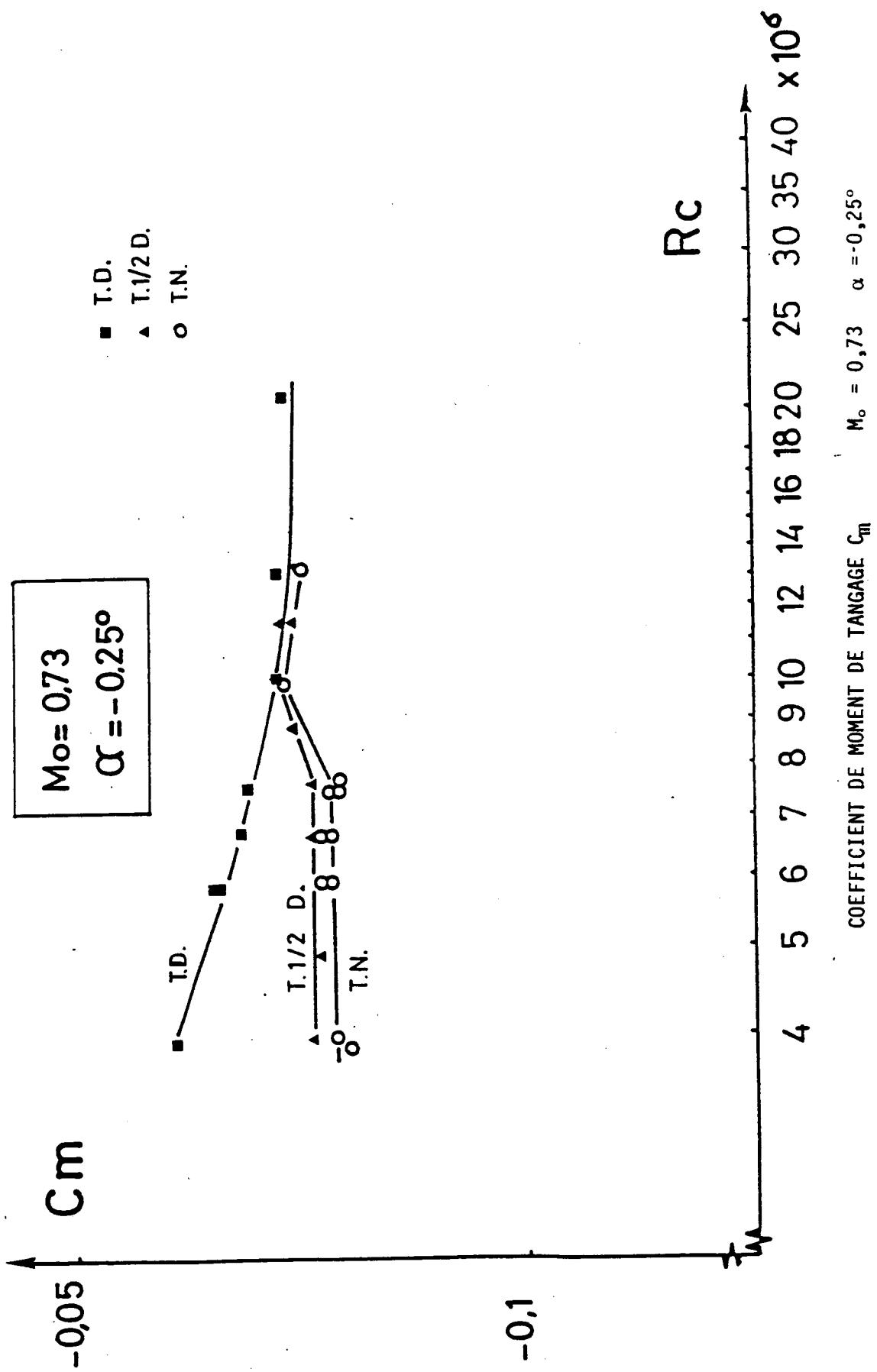


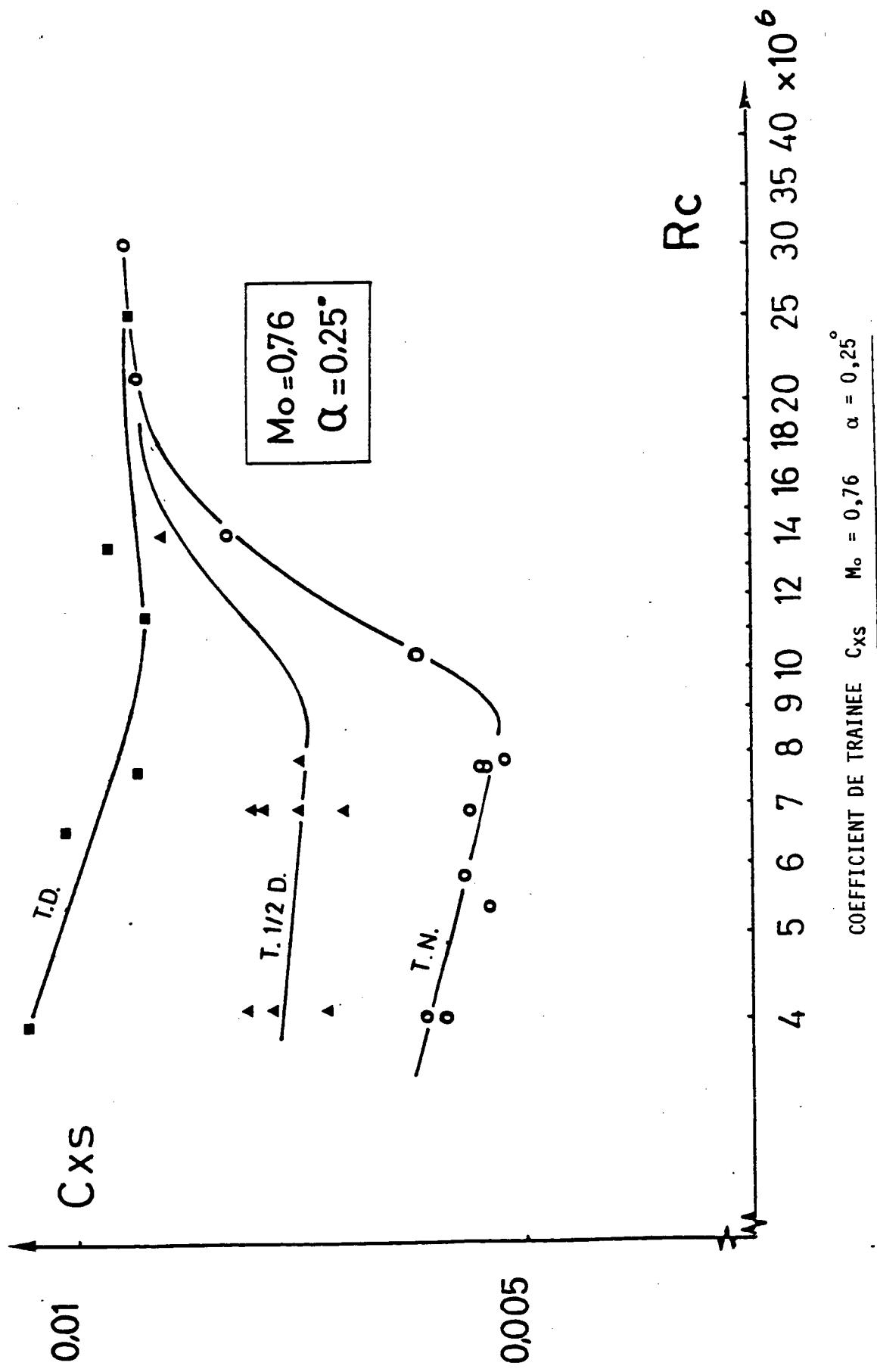


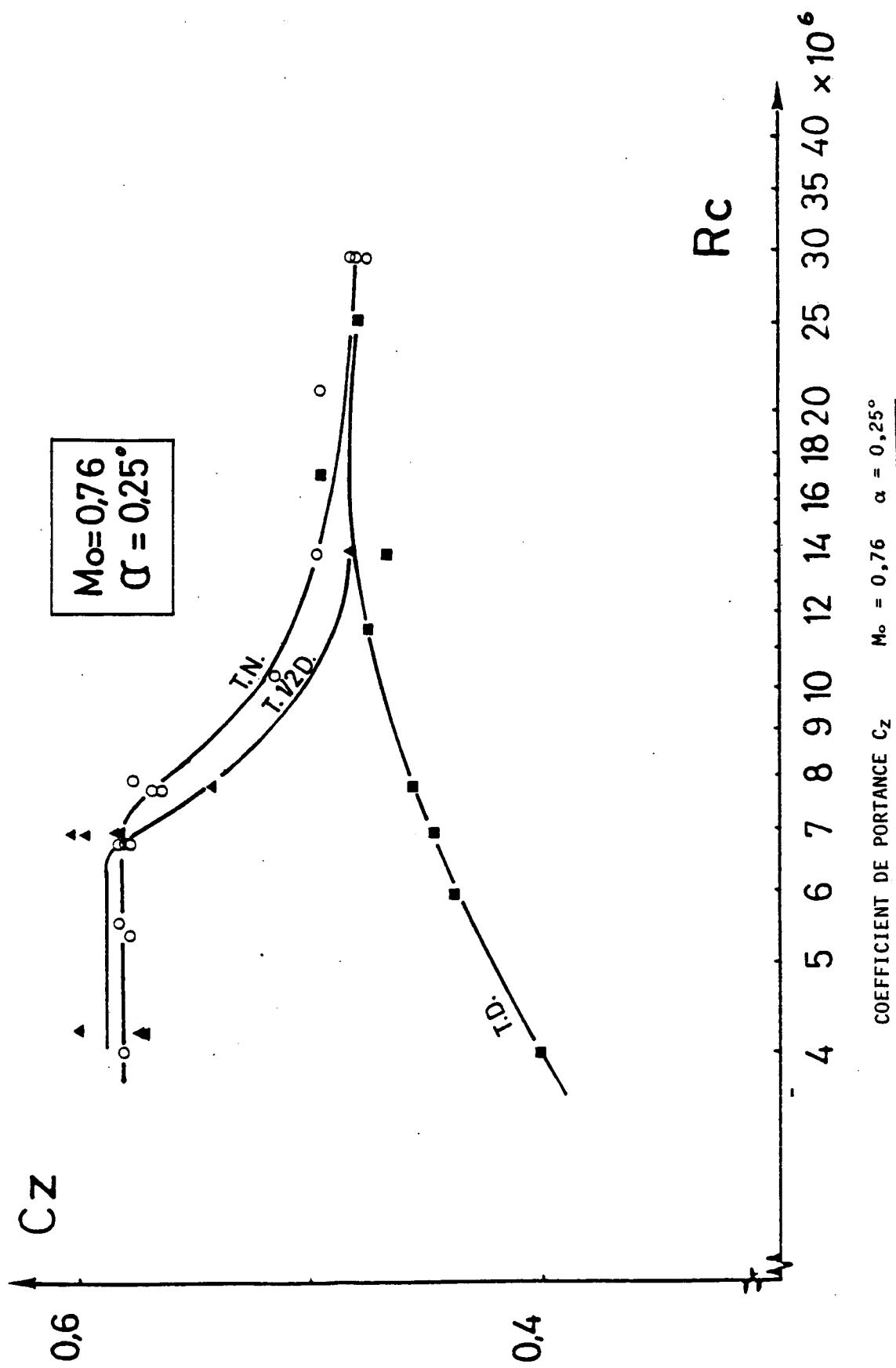


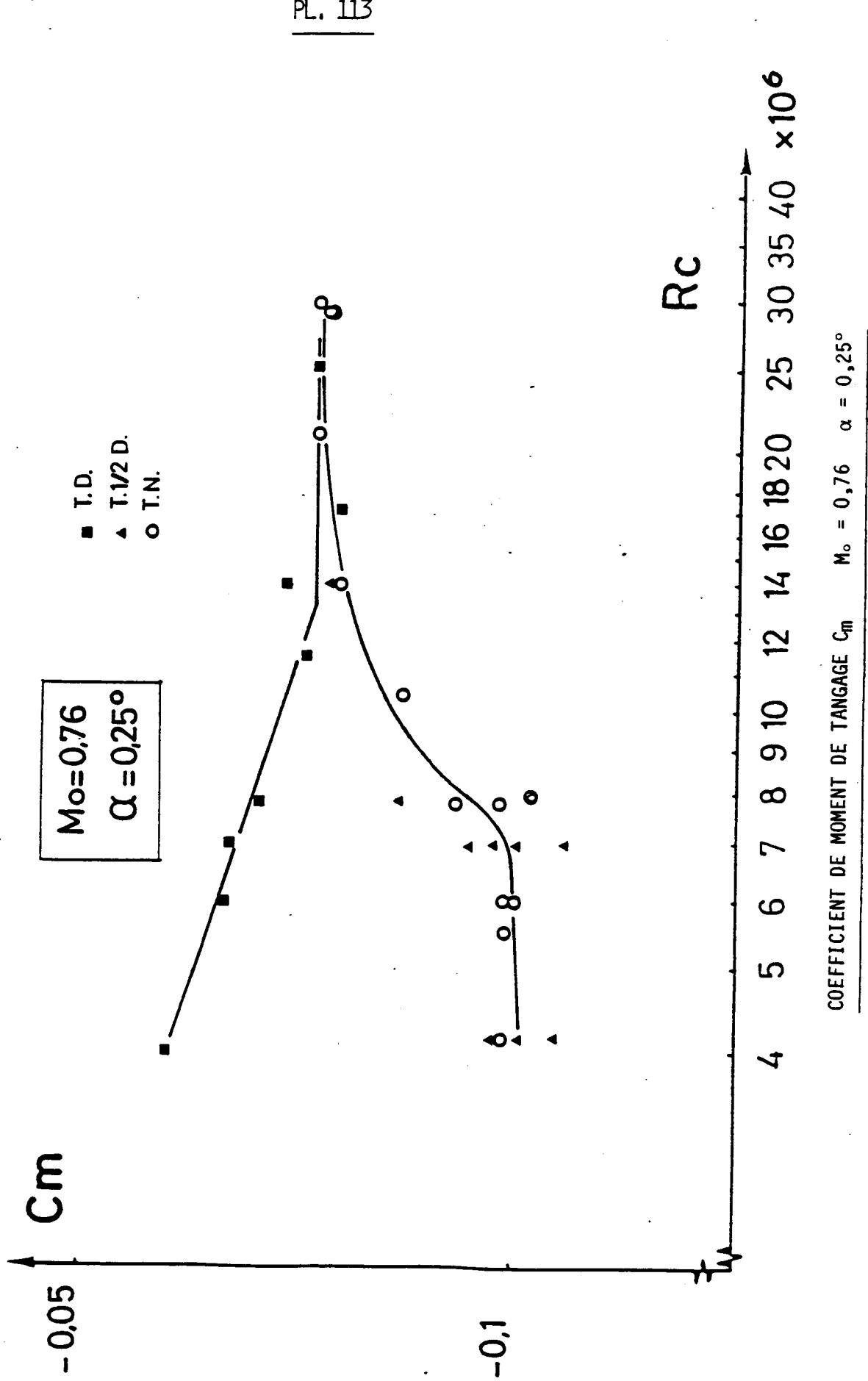


PL. 110

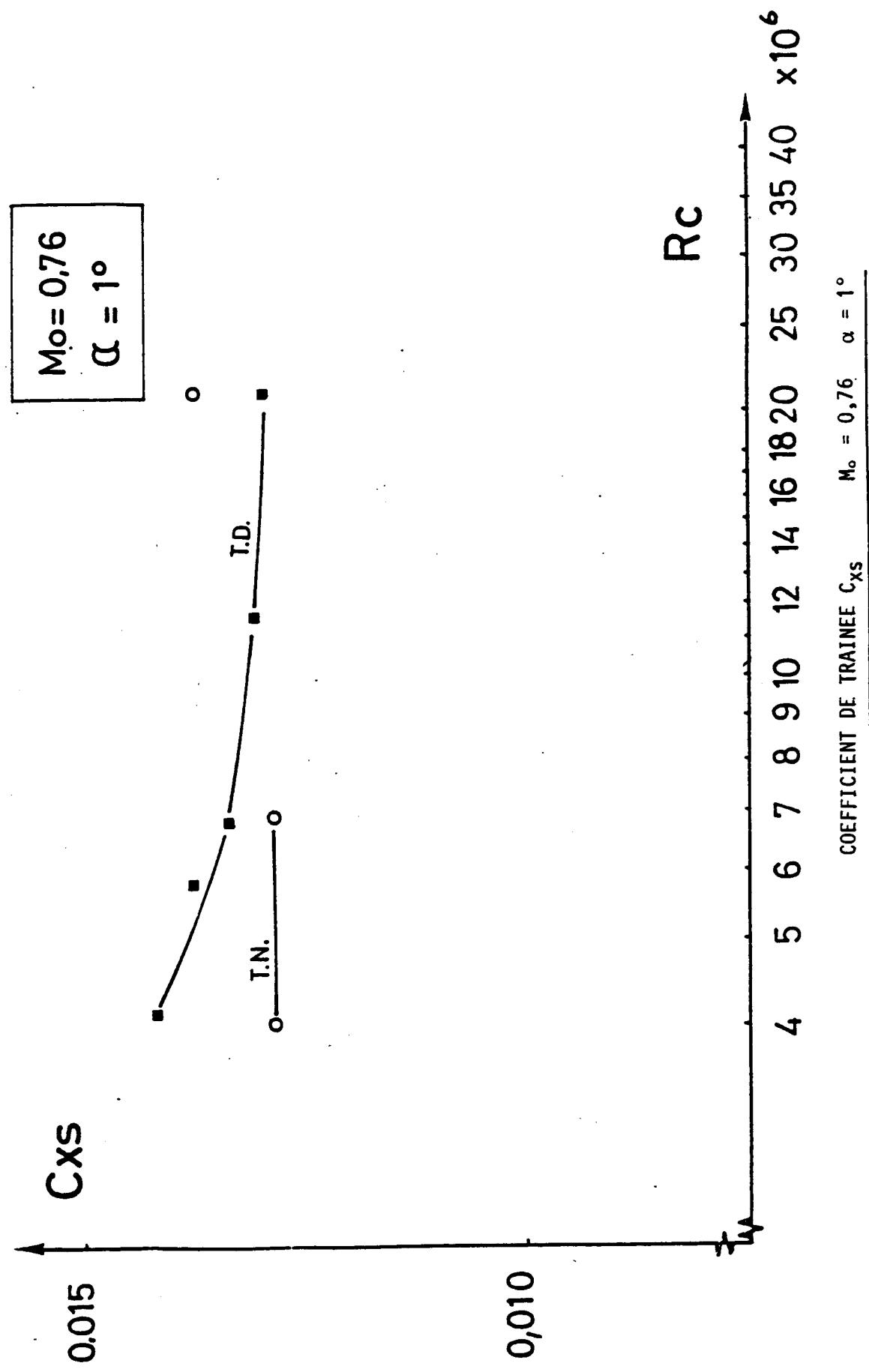




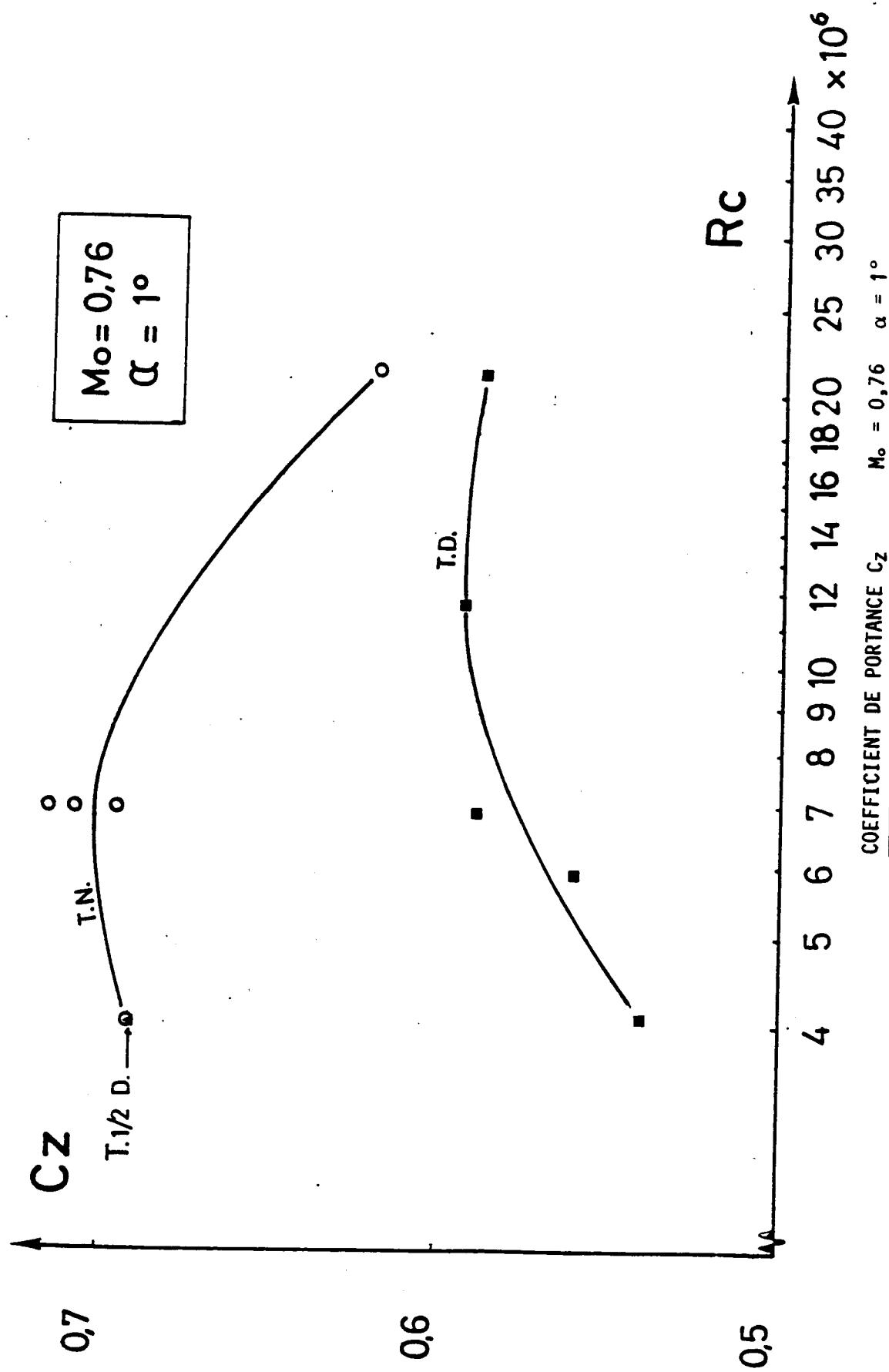


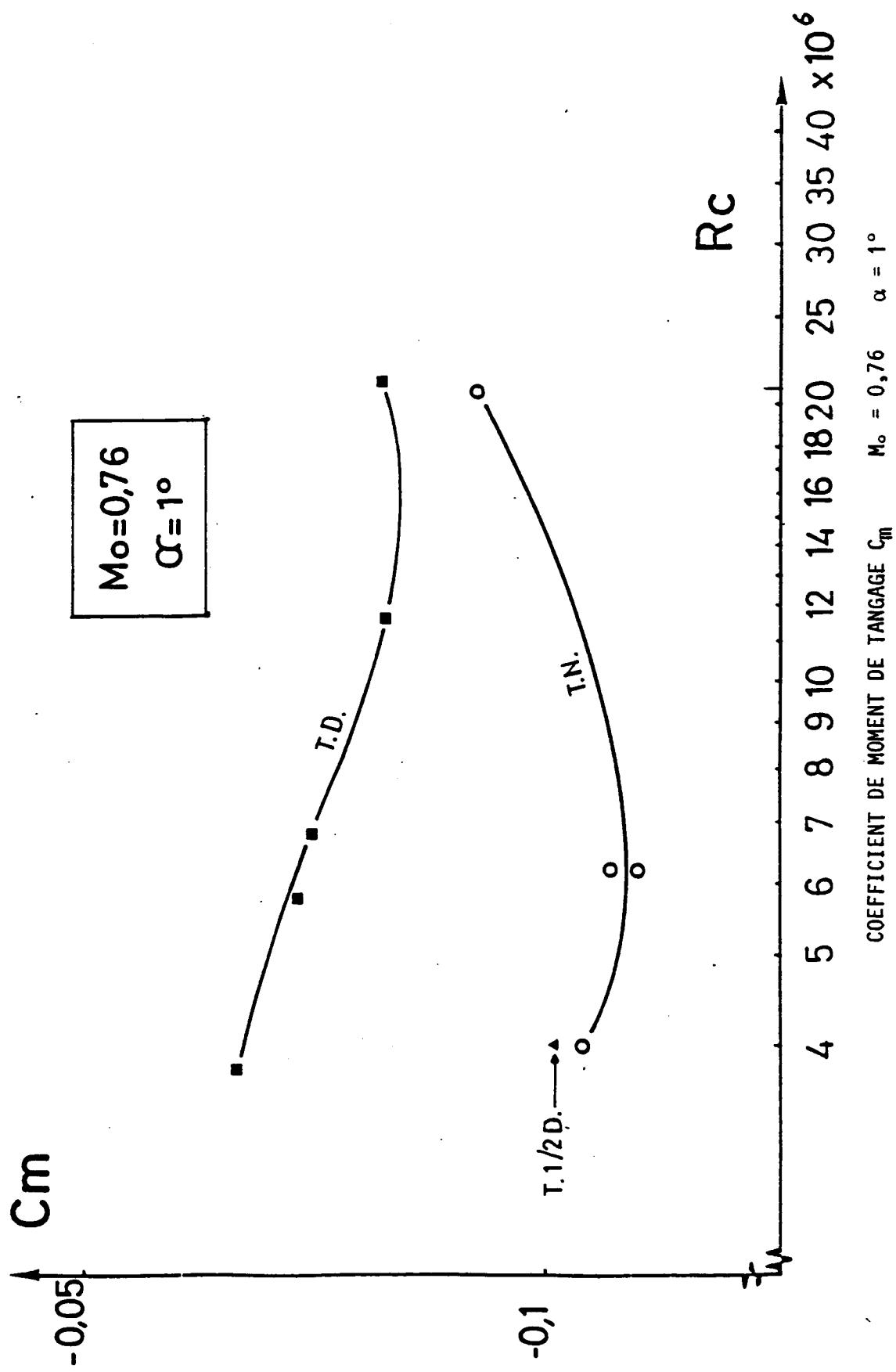


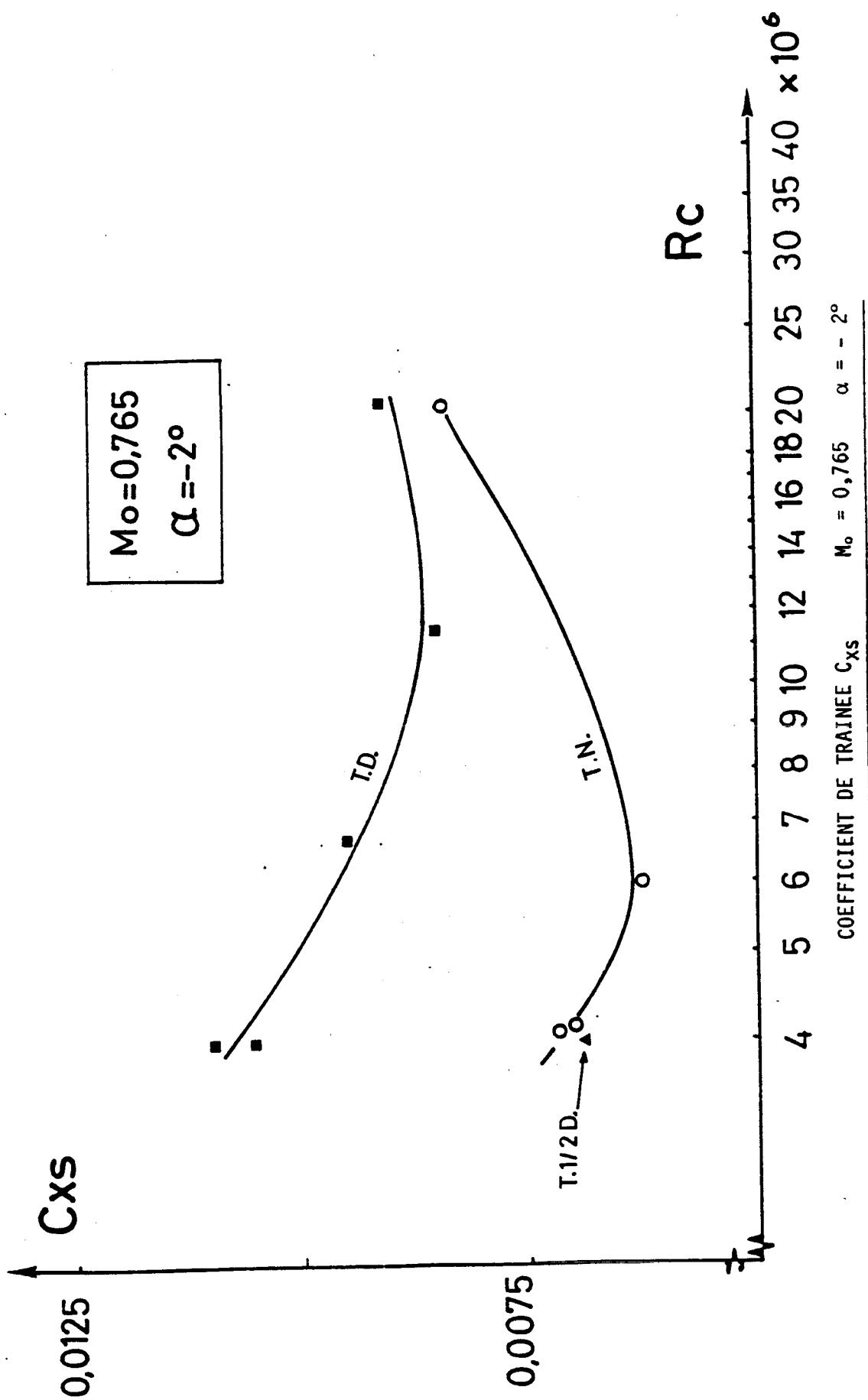
PL. 114

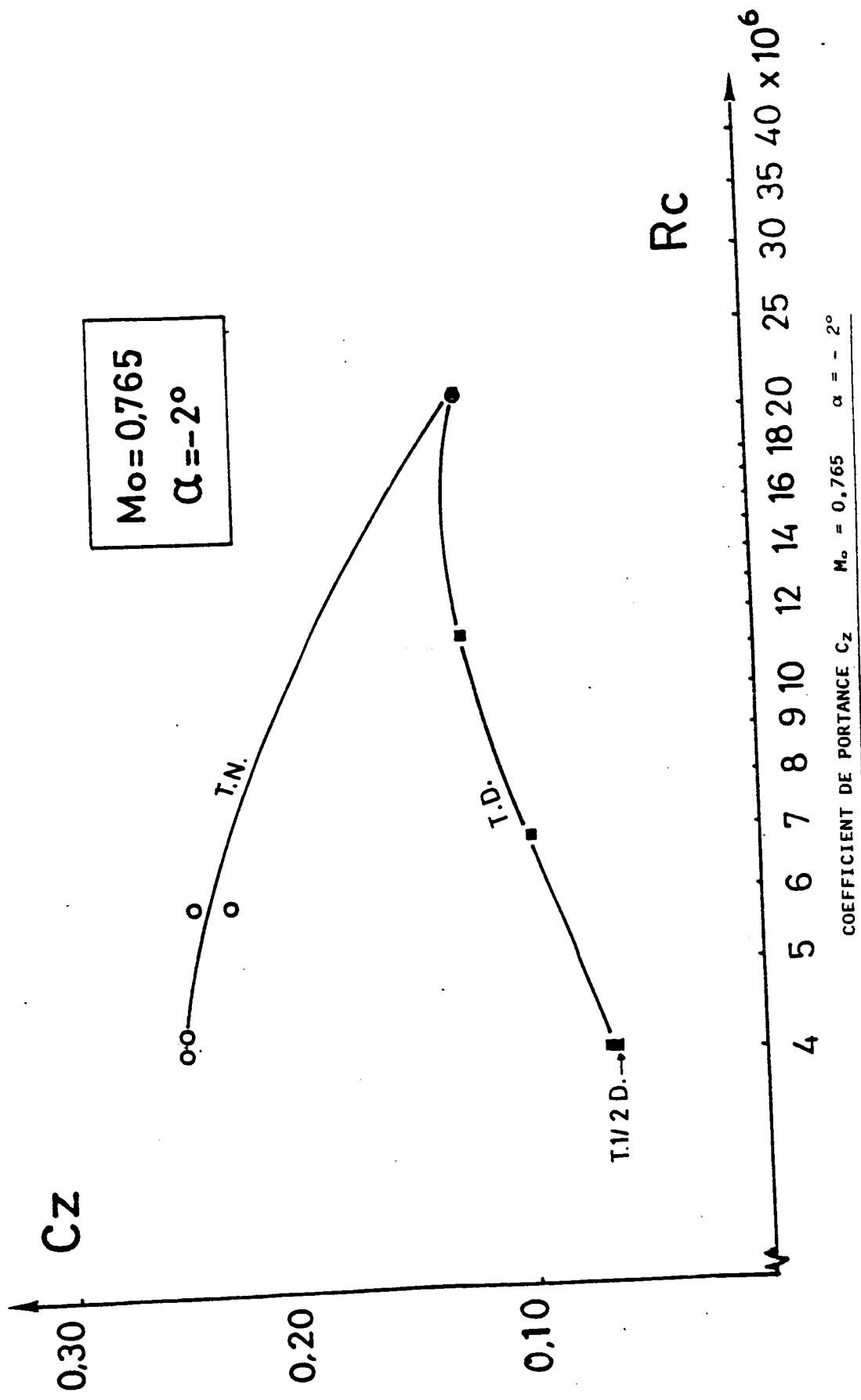


PL. 115

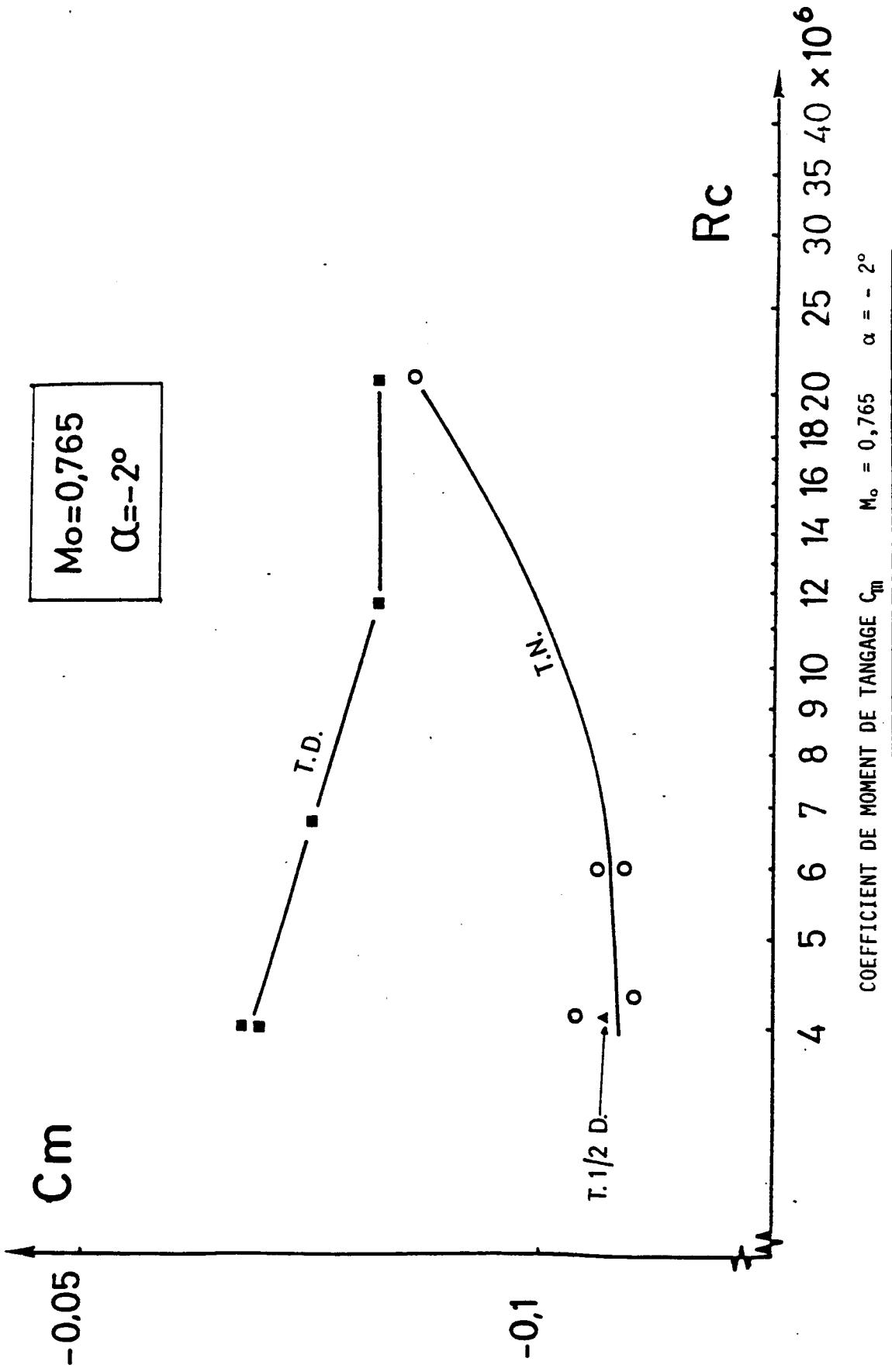




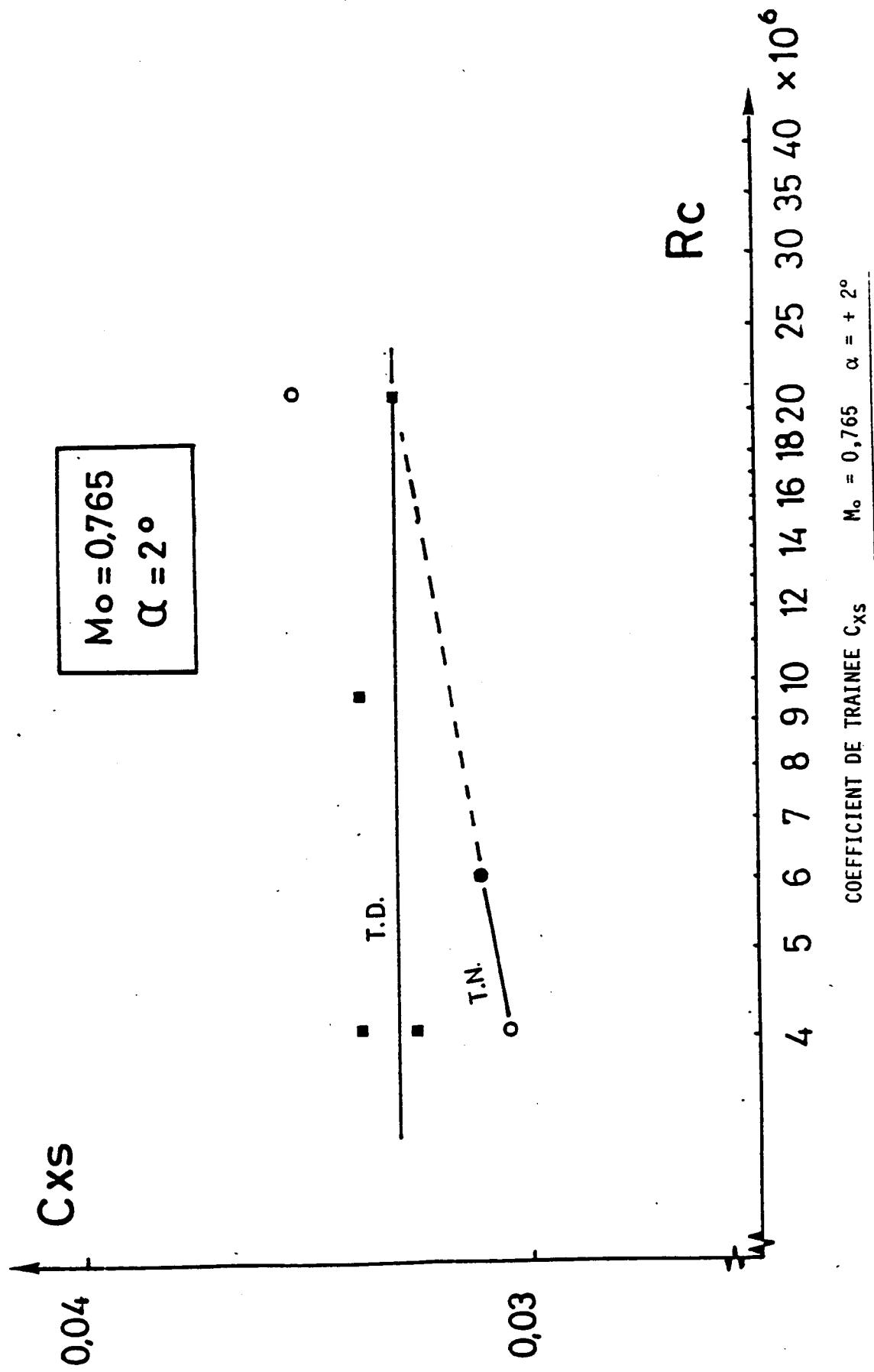




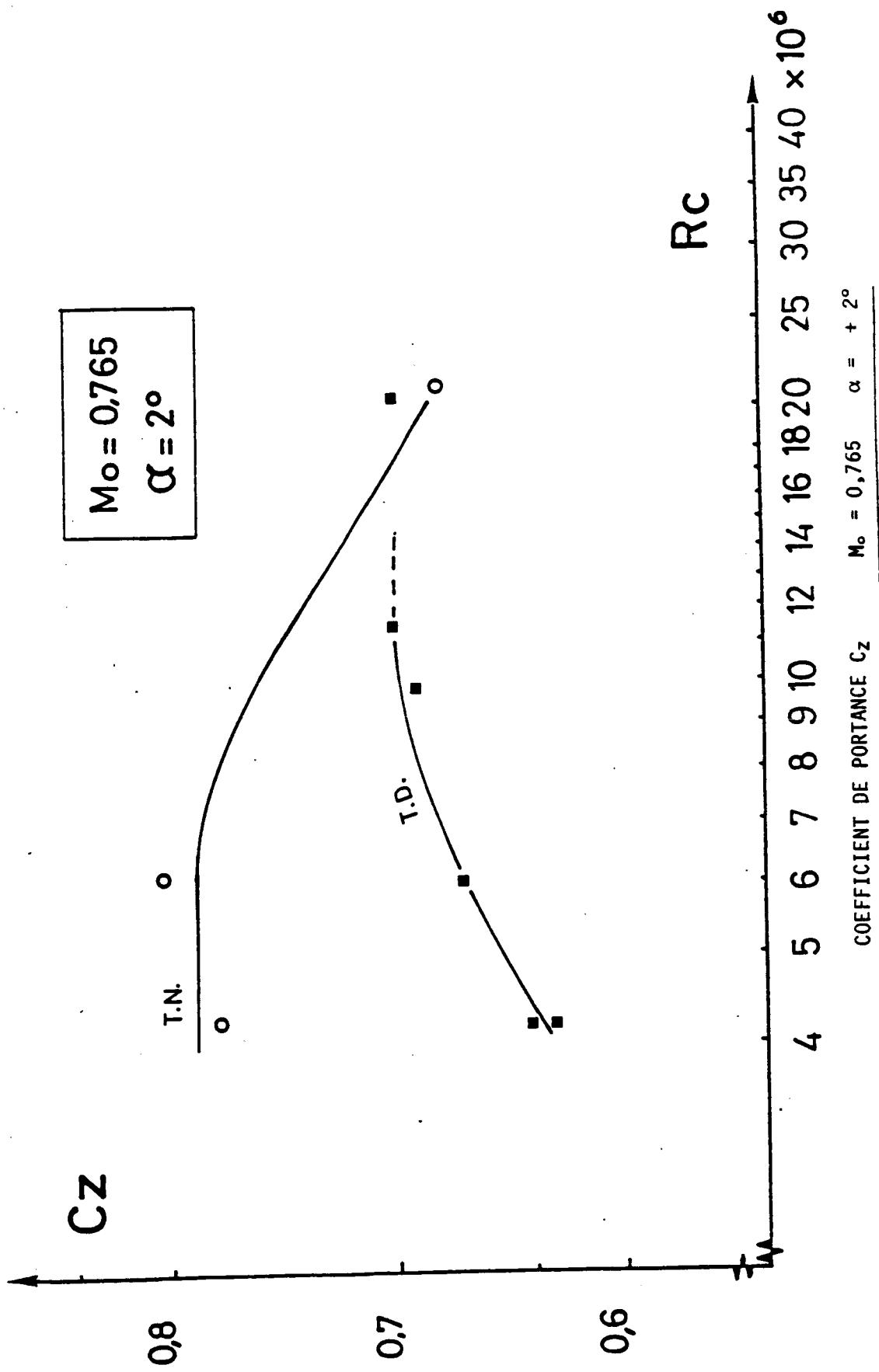
PL. 119



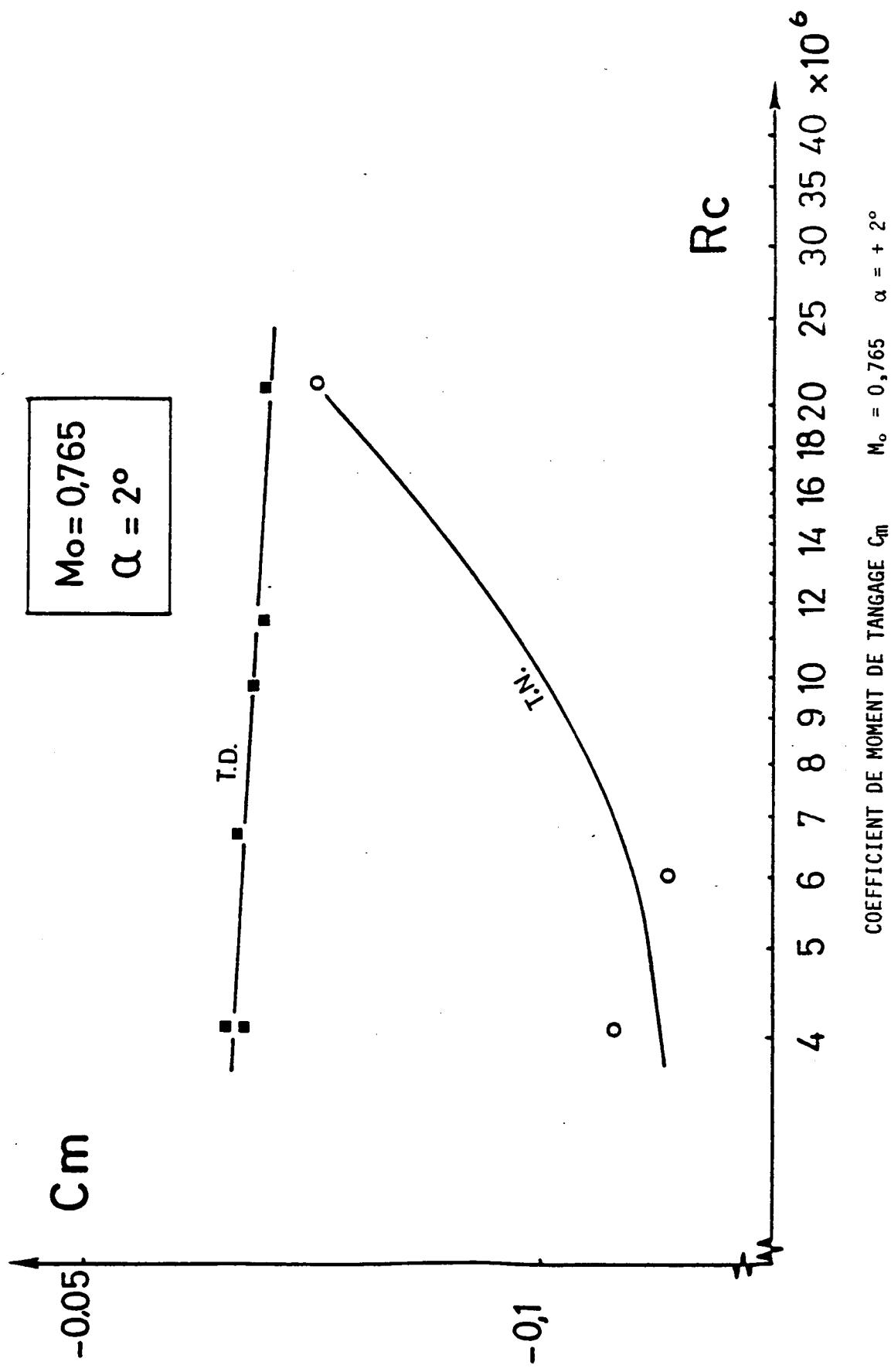
PL. 120



PL. 121



PL. 122



ANNEXE

LISTINGS A LA DERNIERE ITERATION DES ESSAIS VALIDES

***** FICHIER RD204 NO(IT)= 4
 1/3/84 15H30=.725 PI=1.7 TI=TA I=+0.00 (RM) RD204
 DE AD 203 4IEME ITE

MACH DE REFERENCE=.7294 UINF= 238.233 M/S
 TIV=293.6 K PIV= 1673 MB

I	MACH PAROIS			*	MACH PROFIL			*	I	TPR
	HAUT	BAS	I		HAUT	BAS	I	EXT	I	INT
1	.732	.724	*	PRISES DOUBLES	*	*	1	.033	53	.653
2	.731	.727	*		*	*	2	.217	54	.653
3	.731	.724	*	59	.728	.722	3	.329	55	.657
4	.730	.725	*	60	.733	.731	4	.439	56	.662
5	.730	.726	*	61	.735	.724	5	.524	57	.669
6	.728	.725	*				6	.578	58	.676
7	.728	.724	*	PRISES LAT. GAUCHE	*	*	7	.619	59	.684
8	.729	.724	*		*	*	8	.648	60	.694
9	.730	.731	*	62	.730	.728	9	.679	61	.705
10	.731	.724	*	63	.729	.731	10	.717	62	.718
11	.731	.728	*	64	.732	.720	11	.752	63	.730
12	.729	.728	*	65	.740	.705	12	.791	64	.743
13	.732	.723	*	66	.760	.703	13	.892	65	.758
14	.729	.721	*	67	.777	.732	14	.962	66	.773
15	.730	.721	*	68	.776	.741	15	1.034	67	.791
16	.731	.721	*	69	.769	.731	16	1.071	68	.810
17	.732	.719	*	70	.757	.712	17	1.085	69	.828
18	.733	.716	*	71	.742	.712	18	1.092	70	.845
19	.733	.714	*	72	.733	.722	19	1.084	71	.861
20	.736	.711	*	73	.732	.731	20	1.054	72	.870
21	.742	.707	*				21	1.037	73	.873
22	.747	.704	*	PRISES LAT. DROITES	*	*	22	1.026	74	.875
23	.752	.699	*				23	1.020	75	.870
24	.756	.700	*	74	.730	.726	24	1.014	76	.862
25	.761	.705	*	75	.729	.725	25	1.006	77	.854
26	.765	.710	*	76	.729	.726	26	.995	78	.843
27	.769	.716	*	77	.730	.721	27	.974	79	.830
28	.774	.727	*	78	.732	.717	28	.973	80	.813
29	.776	.734	*	79	.735	.713	29	.987	81	.807
30	.776	.739	*	80	.741	.706	30	.991	82	.796
31	.778	.738	*	81	.753	.702	31	.994	83	.786
32	.777	.744	*	82	.758	.704	32	.999	84	.775
33	.775	.744	*	83	.768	.716	33	.999	85	.766
34	.773	.739	*	84	.776	.731	34	1.002	86	.760
35	.771	.737	*	85	.778	.740	35	1.005	87	.748
36	.770	.734	*	86	.774	.742	36	1.008	88	.734
37	.768	.728	*	87	.771	.738	37	1.003	89	.721
38	.766	.722	*	88	.769	.730	38	.996	90	.708
39	.764	.717	*	89	.763	.719	39	.976	91	.699
40	.760	.714	*	90	.755	.713	40	.953	92	.695
41	.757	.710	*	91	.746	.709	41	.928	93	.688
42	.756	.709	*	92	.744	.713	42	.900	94	.683
43	.751	.705	*	93	.736	.718	43	.872	95	.679
44	.745	.706	*	94	.736	.722	44	.841	96	.682
45	.742	.706	*	95	.734	.726	45	.810	97	.682
46	.742	.708	*	96	.732	.726	46	.781	98	.715
47	.744	.713	*				47	.752	99	.760
48	.741	.716	*				48	.725	100	.782
49	.739	.718	*				49	.702	101	.568
50	.733	.720	*				50	.683	102	.410
51	.733	.722	*				51	.666	103	.282
52	.735	.726	*		PRISES COL	*	52	.653		
53	.736	.727	*						REFERENCE PROFIL	
54	.735	.727	*		.794	1.181	*		.731	
55	.735	.726	*		.838	.959	*		.730	
56	.733	.725	*		.899	.859	*		.729	
57	.731	.724	*		.952	.806	*		.728	
58	.727	.722	*		1.122	.765	*			

**ORIGINAL PAGE IS
OF POOR QUALITY**

***** FICHIER AD205 NO(IT)= 4
5/3/85 11H25 M=.76 PI=1.7 TI=TR I=+0.00 (RM) AD205
DE AD204 4 IEME ITE

MACH DE REFERENCE= .7637 UINF= 248.458 M/S
TIV=294.0 K PIV= 17227 MB

***** FICHIER AD206 NO(IT)= 4
5/3/85 15H 0 M=.695 PI=1.7 TI=TA I=+0.00 (RM) AD206
DE AD204 4 IEME ITE

MACH DE REFERENCE= .6984 UINF= 228.830 M/S
TIV=293.1 K PIV= 1629 MB

***** FICHIER AD207 NO(IT)= 4
5/3/84 15H40 M=.695 PI=1.7 TI=TA I=-1.00 (RM) AD207
DE AD125 4 IEME ITE

MACH DE REFERENCE= .7016 UINF= 230.318 M/S
TIV=294.5 K PIV= 1632 MB

***** FICHIER AD208 NO(IT)= 5
5/3/84 15H60 M=.755 PI=1.7 TI=TA I=-1.00 (RM) AD208
DE AD24 4 IEME ITE

MACH DE REFERENCE= .7554 UINF= 246.754 M/S
TIV=295.7 K PIV= 1721 MB

***** FICHIER AD209 NO(IT)= 4
 5/3/84 16H20 M=.760 PI=1.7 TI=TA I=-1.00 (RM) AD209
 DE AD209 5 IEME ITE

MACH DE REFERENCE= .7667 UINF= 250.229 M/S
 TIV=296.1 K PIV= 1730 MB

I	MACH PAROIS				MACH PROFIL				T(K)				
	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPG
1	.769	.759	*	PRISES DOUBLES	*	*	1	.109	53	.652	*	1	292.0
2	.767	.763	*	*	*	*	2	.129	54	.658	*	2	290.1
3	.767	.761	*	59	.764	.760	*	.239	55	.666	*	3	299.7
4	.765	.762	*	60	.770	.767	*	.358	56	.675	*	4	299.3
5	.764	.764	*	61	.770	.759	*	.437	57	.684	*	5	299.7
6	.764	.763	*	*	*	*	6	.497	58	.695	*	6	299.3
7	.765	.762	*	PRISES LAT. GAUCHE	*	*	7	.543	59	.706	*	7	299.7
8	.766	.761	*	*	*	*	8	.580	60	.718	*	8	290.1
9	.768	.768	*	62	.765	.764	*	.615	61	.731	*	9	292.7
10	.768	.759	*	63	.764	.767	*	.656	62	.745	*	10	292.3
11	.766	.763	*	64	.769	.758	*	.694	63	.761	*	11	291.8
12	.762	.762	*	65	.772	.741	*	.735	64	.776	*	12	291.6
13	.766	.757	*	66	.795	.745	*	.840	65	.794	*	13	291.9
14	.763	.756	*	67	.816	.784	*	.916	66	.813	*	14	292.3
15	.765	.758	*	68	.819	.792	*	.995	67	.834	*	15	292.3
16	.766	.759	*	69	.814	.772	*	1.039	68	.858	*	16	290.3
17	.768	.757	*	70	.802	.744	*	1.063	69	.882	*	17	289.0
18	.771	.754	*	71	.777	.745	*	1.078	70	.905	*	18	290.0
19	.769	.750	*	72	.769	.758	*	1.089	71	.928	*	19	290.3
20	.769	.747	*	73	.769	.768	*	1.090	72	.944	*	20	290.3
21	.774	.743	*	*	*	*	21	1.082	73	.954	*	I	TPG
22	.781	.741	*	PRISES LAT. DROITES	*	*	22	1.076	74	.959	*		
23	.788	.738	*	*	*	*	23	1.073	75	.955	*	1	296.2
24	.792	.740	*	74	.766	.764	*	1.072	76	.946	*	2	296.2
25	.795	.748	*	75	.765	.762	*	1.067	77	.938	*	3	296.1
26	.800	.755	*	76	.766	.761	*	1.061	78	.925	*	4	296.1
27	.806	.765	*	77	.764	.755	*	1.055	79	.909	*	5	296.1
28	.813	.779	*	78	.768	.757	*	1.054	80	.894	*		
29	.816	.789	*	79	.769	.749	*	1.059	81	.883	*		
30	.817	.794	*	80	.774	.741	*	1.066	82	.873	*		
31	.820	.793	*	81	.788	.740	*	1.073	83	.862	*		
32	.820	.799	*	82	.792	.747	*	1.082	84	.852	*		
33	.819	.797	*	83	.804	.764	*	1.093	85	.843	*		
34	.817	.788	*	84	.815	.785	*	1.104	86	.839	*		
35	.815	.784	*	85	.818	.794	*	1.118	87	.828	*		
36	.815	.777	*	86	.816	.794	*	1.136	88	.817	*		
37	.813	.768	*	87	.815	.786	*	1.152	89	.808	*		
38	.811	.757	*	88	.813	.772	*	1.157	90	.794	*		
39	.811	.749	*	89	.808	.753	*	1.137	91	.788	*		
40	.806	.745	*	90	.799	.745	*	1.131	92	.785	*		
41	.802	.740	*	91	.788	.746	*	1.131	93	.774	*		
42	.801	.739	*	92	.779	.748	*	1.199	94	.769	*		
43	.794	.738	*	93	.771	.753	*	.894	95	.759	*		
44	.787	.740	*	94	.772	.758	*	.856	96	.782	*		
45	.783	.741	*	95	.769	.763	*	.844	97	.837	*		
46	.780	.744	*	96	.768	.764	*	.822	98	.872	*		
47	.779	.747	*	*	*	*	47	.797	99	.952	*		
48	.777	.750	*	*	*	*	48	.770	100	.892	*		
49	.774	.754	*	*	*	*	49	.739	101	.721	*		
50	.770	.758	*	*	*	*	50	.712	102	.540	*		
51	.772	.759	*	*	*	*	51	.683	103	.405	*		
52	.770	.761	*	PRISES COL	*	*	52	.648					
53	.771	.762	*										
54	.771	.763	*		.833	1.296	*			REFERENCE PROFIL			
55	.771	.763	*		.872	.905	*			.765			
56	.770	.763	*		.926	.856	*			.766			
57	.768	.761	*		.973	.821	*			.765			
58	.763	.759	*		1.141	.790	*			.765			

***** FICHIER AD210 NO(IT)= 5
5/ 3/84 17H10 M=.695 PI=1.7 TI=TA I=-0.50 (RM) AD210
DE AD129 4 IEME ITE

MACH DE REFERENCE= .7011 UINF= 230.629 M/S
TIV=295.6 K PIV= 1635 MB

***** FICHIER AD211 NO(IT)= 4
5 / 3/84 17H35 M=.725 PI=1.7 TI=TA I=-0.50 (RM) AD211
DE AD210 5 IEME ITE

MACH DE REFERENCE= .7291 UINF= 239.140 M/S
TIV=296.1 K PIV= 1674 MB

***** FICHIER AD213 NO(IT)= 5
6/ 3/84 11H10 M=.695 PI=1.7 TI=TA I=+1.00 (RM) AD213
DE AD107 4 IEME ITE

MACH DE REFERENCE= .6832 UINF= 224.234 M/S
TIV=293.0 K PIV= 1622 MB

MACH PAROIS						MACH PROFIL						T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.686	.675	*	PRISES DOUBLES	*	*	1	.127	53	.620	*	1	299.2	
2	.684	.677	*			*	2	.329	54	.619	*	2	288.2	
3	.684	.677	*	59	.682	.675	*	.438	55	.619	*	3	288.6	
4	.685	.681	*	60	.687	.681	*	.553	56	.623	*	4	288.6	
5	.684	.683	*	61	.689	.679	*	.637	57	.628	*	5	288.7	
6	.682	.680	*			*	6	.681	58	.634	*	6	288.3	
7	.682	.676	*	PRISES LAT. GAUCHE	*	*	7	.710	59	.641	*	7	288.9	
8	.684	.676	*			*	8	.733	60	.649	*	8	299.3	
9	.686	.683	*	62	.684	.682	*	.757	61	.658	*	9	290.3	
10	.684	.674	*	63	.685	.679	*	10	.788	62	.668	*	10	290.0
11	.684	.678	*	64	.690	.676	*	11	.819	63	.678	*	11	289.3
12	.682	.680	*	65	.698	.658	*	12	.855	64	.689	*	12	289.7
13	.685	.676	*	66	.713	.652	*	13	.952	65	.701	*	13	290.0
14	.684	.676	*	67	.727	.670	*	14	1.014	66	.713	*	14	290.3
15	.686	.677	*	68	.728	.681	*	15	1.071	67	.727	*	15	290.2
16	.688	.677	*	69	.723	.676	*	16	1.081	68	.742	*	16	289.5
17	.690	.675	*	70	.710	.662	*	17	1.063	69	.755	*	17	289.2
18	.691	.670	*	71	.694	.667	*	18	1.037	70	.767	*	18	289.5
19	.692	.667	*	72	.689	.677	*	19	1.014	71	.777	*	19	289.7
20	.695	.665	*	73	.688	.684	*	20	.995	72	.783	*		
21	.700	.661	*			*	21	.980	73	.784	*	I	TPG	
22	.703	.654	*	PRISES LAT. DROITES	*	*	22	.942	74	.784	*			
23	.707	.648	*			*	23	.937	75	.779	*	1	293.0	
24	.710	.649	*	74	.684	.681	*	24	.935	76	.771	*	2	293.0
25	.714	.654	*	75	.683	.676	*	25	.928	77	.764	*	3	293.0
26	.717	.657	*	76	.683	.676	*	26	.924	78	.755	*	4	293.0
27	.720	.660	*	77	.683	.674	*	27	.922	79	.743	*	5	293.0
28	.725	.667	*	78	.690	.675	*	28	.921	80	.732	*		
29	.726	.672	*	79	.692	.666	*	29	.920	81	.721	*		
30	.727	.676	*	80	.698	.660	*	30	.919	82	.711	*		
31	.729	.675	*	81	.707	.650	*	31	.915	83	.701	*		
32	.728	.682	*	82	.712	.653	*	32	.916	84	.691	*		
33	.727	.683	*	83	.719	.660	*	33	.915	85	.682	*		
34	.725	.680	*	84	.726	.670	*	34	.914	86	.674	*		
35	.724	.681	*	85	.728	.678	*	35	.913	87	.659	*		
36	.724	.678	*	86	.726	.682	*	36	.913	88	.643	*		
37	.721	.674	*	87	.725	.682	*	37	.909	89	.625	*		
38	.719	.669	*	88	.722	.676	*	38	.903	90	.611	*		
39	.717	.665	*	89	.716	.666	*	39	.891	91	.598	*		
40	.714	.663	*	90	.709	.663	*	40	.876	92	.592	*		
41	.711	.660	*	91	.701	.664	*	41	.856	93	.581	*		
42	.710	.659	*	92	.696	.668	*	42	.832	94	.573	*		
43	.705	.659	*	93	.692	.674	*	43	.810	95	.564	*		
44	.701	.660	*	94	.691	.676	*	44	.783	96	.565	*		
45	.697	.662	*	95	.685	.685	*	45	.756	97	.551	*		
46	.696	.664	*	96	.688	.685	*	46	.729	98	.554	*		
47	.696	.669	*			*	47	.704	99	.562	*			
48	.695	.671	*			*	48	.681	100	.505	*			
49	.694	.674	*			*	49	.661	101	.392	*			
50	.692	.677	*			*	50	.646	102	.254	*			
51	.692	.677	*			*	51	.634	103	.136	*			
52	.688	.680	*	PRISES COL	*	*	52	.624						
53	.688	.680	*											
54	.687	.679	*		.746	1.144	*							
55	.687	.680	*		.795	1.257	*							
56	.687	.681	*		.865	.887	*							
57	.686	.682	*		.923	.793	*							
58	.685	.687	*		1.096	.739	*							
								REFERENCE PROFIL						

10 ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD214 NO(IT)= 4
6/3/84 11H55 M=.730 PI=1.7 TI=TA I=+1.00 (RM) AD214
DE AD213 4 IEME ITE

MACH DE REFERENCE= .7345 UINF= 240.112 M/S
TIV=294.5 K PIV= 1680 MB

MACH PAROIS						MACH PROFIL						T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.740	.724	*	PRISES DOUBLES		*	1	.111	53	.648	*	1	299.2	
2	.738	.729	*			*	2	.319	54	.648	*	2	297.9	
3	.737	.728	*	59	.734	.727	*	3	.433	55	.652	*	3	298.9
4	.734	.730	*	60	.740	.732	*	4	.551	56	.658	*	4	299.7
5	.733	.732	*	61	.740	.726	*	5	.640	57	.664	*	5	297.7
6	.733	.731	*			*	6	.687	58	.672	*	6	288.3	
7	.735	.729	*	PRISES LAT. GAUCHE	S	*	7	.718	59	.680	*	7	288.3	
8	.736	.727	*			*	8	.743	60	.690	*	8	299.7	
9	.737	.733	*	62	.735	.732	*	9	.770	61	.700	*	9	291.3
10	.737	.725	*	63	.735	.731	*	10	.803	62	.712	*	10	291.8
11	.736	.729	*	64	.742	.724	*	11	.837	63	.724	*	11	290.7
12	.731	.729	*	65	.752	.705	*	12	.876	64	.736	*	12	290.6
13	.735	.726	*	66	.777	.694	*	13	.981	65	.751	*	13	290.9
14	.734	.726	*	67	.800	.721	*	14	1.057	66	.765	*	14	291.3
15	.736	.728	*	68	.794	.732	*	15	1.131	67	.782	*	15	291.1
16	.737	.725	*	69	.783	.724	*	16	1.175	68	.800	*	16	289.3
17	.742	.722	*	70	.776	.710	*	17	1.202	69	.816	*	17	288.9
18	.746	.715	*	71	.747	.713	*	18	1.214	70	.831	*	18	289.2
19	.745	.713	*	72	.740	.724	*	19	1.223	71	.844	*	19	289.6
20	.747	.712	*	73	.735	.735	*	20	1.224	72	.852	*	20	289.6
21	.753	.707	*			*	21	1.223	73	.854	*	I	TPG	
22	.762	.697	*	PRISES LAT. DROITES	S	*	22	1.224	74	.854	*			
23	.769	.689	*			*	23	1.223	75	.847	*	1	294.5	
24	.773	.690	*	74	.735	.731	*	24	1.219	76	.837	*	2	294.5
25	.777	.696	*	75	.736	.728	*	25	1.204	77	.829	*	3	294.5
26	.783	.700	*	76	.736	.727	*	26	1.185	78	.817	*	4	294.5
27	.790	.706	*	77	.734	.724	*	27	1.173	79	.803	*	5	294.4
28	.797	.716	*	79	.742	.723	*	28	1.168	80	.799	*		
29	.800	.723	*	79	.746	.711	*	29	1.017	81	.777	*		
30	.800	.728	*	80	.752	.706	*	30	.898	82	.765	*		
31	.801	.728	*	81	.769	.692	*	31	.936	83	.753	*		
32	.797	.734	*	92	.775	.696	*	32	.966	84	.741	*		
33	.793	.734	*	83	.787	.705	*	33	.984	85	.731	*		
34	.788	.729	*	84	.799	.720	*	34	.999	86	.721	*		
35	.784	.727	*	85	.800	.729	*	35	1.011	87	.706	*		
36	.784	.724	*	86	.792	.731	*	36	1.021	88	.687	*		
37	.782	.719	*	87	.785	.728	*	37	1.019	89	.667	*		
38	.782	.714	*	88	.783	.721	*	38	1.011	90	.652	*		
39	.782	.711	*	89	.781	.713	*	39	.989	91	.643	*		
40	.779	.709	*	90	.773	.709	*	40	.966	92	.631	*		
41	.777	.706	*	91	.760	.709	*	41	.940	93	.620	*		
42	.775	.705	*	92	.749	.714	*	42	.912	94	.611	*		
43	.767	.705	*	93	.742	.720	*	43	.882	95	.601	*		
44	.759	.706	*	94	.743	.723	*	44	.852	96	.594	*		
45	.754	.706	*	95	.739	.734	*	45	.820	97	.590	*		
46	.751	.709	*	96	.734	.733	*	46	.790	98	.596	*		
47	.748	.715	*			*	47	.760	99	.588	*			
48	.746	.718	*			*	48	.733	100	.547	*			
49	.744	.720	*			*	49	.707	101	.426	*			
50	.741	.722	*			*	50	.685	102	.293	*			
51	.744	.724	*			*	51	.666	103	.156	*			
52	.741	.728	*	PRISES COL		*	52	.649						
53	.741	.730	*											
54	.741	.731	*		.800	1.188	*							
55	.740	.731	*		.844	.932	*							
56	.737	.731	*		.984	.855	*							
57	.734	.731	*		.955	.809	*							
58	.727	.732	*		1.127	.768	*							

REFERENCE PROFIL

.734

.734

.734

.734

.733

***** FICHIER RD215 NO(IT)= +
 6/ 3/84 12H20 M=.760 PI=1.7 TI=TA I=+1.00 (RM) RD215
 DE RD214 4 IEUME ITE

MACH DE REFERENCE= .7647 UINF= 249.292 M/S
 TIY=295.3 K PIV= 1730 MB

MACH PAROIS						MACH PROFIL						T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.774	.756	*	PRISES DOUBLES		*	1	.101	.53	.662	*	1	290.9	
2	.774	.762	*			*	2	.305	.54	.665	*	2	288.4	
3	.771	.759	*	59	.767	.759	*	3	.418	.55	.669	*	3	288.2
4	.765	.758	*	60	.771	.764	*	4	.538	.56	.676	*	4	288.4
5	.763	.760	*	61	.767	.753	*	5	.626	.57	.683	*	5	288.7
6	.765	.761	*			*	6	.675	.58	.691	*	6	289.1	
7	.767	.761	*	PRISES LAT. GAUCHE	S*	*	7	.709	.59	.700	*	7	288.2	
8	.766	.757	*			*	8	.735	.60	.711	*	8	287.6	
9	.766	.763	*	62	.768	.761	*	9	.763	.61	.723	*	9	291.7
10	.768	.756	*	63	.765	.764	*	10	.799	.62	.736	*	10	291.4
11	.767	.760	*	64	.774	.751	*	11	.833	.63	.750	*	11	291.0
12	.762	.759	*	65	.783	.729	*	12	.872	.64	.763	*	12	290.9
13	.767	.756	*	66	.818	.720	*	13	.981	.65	.779	*	13	291.3
14	.766	.757	*	67	.846	.753	*	14	1.055	.66	.794	*	14	291.7
15	.769	.758	*	68	.847	.768	*	15	1.137	.67	.814	*	15	291.6
16	.769	.754	*	69	.834	.757	*	16	1.187	.68	.835	*	16	289.3
17	.773	.749	*	70	.811	.738	*	17	1.215	.69	.854	*	17	288.9
18	.776	.742	*	71	.782	.741	*	18	1.232	.70	.872	*	18	289.1
19	.777	.739	*	72	.770	.753	*	19	1.243	.71	.888	*	19	289.6
20	.779	.737	*	73	.761	.767	*	20	1.248	.72	.898	*		
21	.784	.731	*			*	21	1.251	.73	.901	*	I	TPG	
22	.790	.721	*	PRISES LAT. DROITE	S*	22	1.257	.74	.901	*				
23	.799	.712	*			*	23	1.261	.75	.893	*	1	295.3	
24	.810	.713	*	74	.768	.762	*	24	1.264	.76	.882	*	2	295.3
25	.819	.721	*	75	.768	.761	*	25	1.266	.77	.872	*	3	295.3
26	.828	.726	*	76	.767	.758	*	26	1.269	.78	.858	*	4	295.2
27	.836	.733	*	77	.766	.755	*	27	1.271	.79	.841	*	5	295.3
28	.843	.746	*	78	.773	.750	*	28	1.274	.80	.826	*		
29	.847	.755	*	79	.778	.737	*	29	1.278	.81	.812	*		
30	.848	.761	*	80	.783	.731	*	30	1.282	.82	.799	*		
31	.852	.761	*	81	.801	.715	*	31	1.287	.83	.786	*		
32	.851	.769	*	82	.817	.721	*	32	1.293	.84	.772	*		
33	.848	.767	*	83	.833	.733	*	33	1.293	.85	.761	*		
34	.844	.762	*	84	.845	.752	*	34	1.275	.86	.751	*		
35	.840	.760	*	85	.849	.762	*	35	1.265	.87	.734	*		
36	.838	.757	*	86	.846	.766	*	36	1.264	.88	.715	*		
37	.833	.750	*	87	.841	.762	*	37	1.263	.89	.694	*		
38	.828	.743	*	88	.835	.753	*	38	1.230	.90	.679	*		
39	.823	.736	*	89	.822	.740	*	39	1.139	.91	.664	*		
40	.817	.734	*	90	.808	.735	*	40	.998	.92	.657	*		
41	.812	.731	*	91	.794	.736	*	41	.924	.93	.645	*		
42	.810	.731	*	92	.784	.741	*	42	.881	.94	.637	*		
43	.802	.730	*	93	.774	.743	*	43	.858	.95	.628	*		
44	.793	.733	*	94	.773	.752	*	44	.838	.96	.632	*		
45	.788	.734	*	95	.769	.757	*	45	.817	.97	.619	*		
46	.786	.737	*	96	.761	.756	*	46	.795	.98	.628	*		
47	.785	.742	*			*	47	.773	.99	.647	*			
48	.781	.746	*			*	48	.750	100	.585	*			
49	.778	.749	*			*	49	.737	101	.459	*			
50	.771	.750	*			*	50	.705	102	.311	*			
51	.773	.753	*			*	51	.684	103	.183	*			
52	.767	.754	*	PRISES COL		*	52	.664		REFERENCE PROFIL				
53	.770	.758	*											
54	.771	.762	*			*	53							
55	.771	.760	*			*	54							
56	.767	.759	*			*	55							
57	.762	.756	*			*	56							
58	.747	.747	*			*	57							

***** FICHIER AD216 NO(CT) = 5
5695626 35

MACH DE REFERENCE=.6996 UINF= 229.650 M/S
TIV=294.3 K PIV= 1594 MB

***** FICHIER AD217 NO(IT)= 4
6/ 3/84 16H50 M=.725 PI 1.7 TI=TA I=2.00 (RM) AD217
DE AD216 SITER.

MACH DE REFERENCE= .7324 UINF= 239.914 M/S
TIV=295.6 K PIV= 1679 MB

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OF POOR QUALITY

***** FICHIER AD218 NO(IT)= 5
6/ 3/84 17H45 M=.695 PI 1.7 TI=TA I=-2.00 (RM) AD218
DE AD207 4ITER.

MACH DE REFERENCE= .7010 UINF= 230.513 M/S
TIY=295.4 K PIY= 1640 MB

***** FICHIER AD219 NO(IT)= 4
 6/3/84 18H 5 M=.725 PI 1.7 TI=TA I=-2.00 (RM) AD219
 DE AD218 4ITER.

MACH DE REFERENCE= .7321 UINF= 240.053 M/S
 TIV=296.1 K PIV= 1682 MB

I	MACH PAROIS			MACH PROFIL			T(K)			TPG	
	HAUT	BAS	I	HAUT	BAS	I	EXT	I	INT	I	
1	.732	.726	*	PRISES DOUBLES	*	*	.193	.53	.628	*	1 291.3
2	.728	.728	*	*	*	2	.043	.54	.634	*	2 290.8
3	.728	.725	*	.59	.729	.727	*	.143	.55	.642	*
4	.729	.728	*	.60	.734	.732	*	.251	.56	.651	*
5	.729	.730	*	.61	.736	.726	*	.335	.57	.659	*
6	.728	.730	*	*	*	6	.399	.58	.669	*	6 290.4
7	.729	.728	*	PRISES LAT. GAUCHE	S	*	.449	.59	.681	*	7 290.6
8	.732	.728	*	*	*	8	.488	.60	.691	*	8 291.2
9	.734	.735	*	.62	.729	.730	*	.525	.61	.704	*
10	.732	.725	*	.63	.731	.732	*	.566	.62	.718	*
11	.730	.728	*	.64	.732	.728	*	.604	.63	.732	*
12	.726	.728	*	.65	.733	.713	*	.643	.64	.747	*
13	.729	.725	*	.66	.746	.731	*	.740	.65	.764	*
14	.727	.726	*	.67	.766	.760	*	.809	.66	.782	*
15	.727	.726	*	.68	.765	.761	*	.872	.67	.802	*
16	.729	.726	*	.69	.762	.743	*	.907	.68	.824	*
17	.731	.726	*	.70	.755	.718	*	.923	.69	.845	*
18	.732	.723	*	.71	.739	.718	*	.932	.70	.866	*
19	.731	.721	*	.72	.734	.724	*	.932	.71	.886	*
20	.733	.718	*	.73	.736	.735	*	.930	.72	.902	*
21	.736	.715	*	*	*	21	.930	.73	.911	*	I TPG
22	.739	.714	*	PRISES LAT. DROITES	S	22	.935	.74	.918	*	
23	.741	.715	*	*	*	23	.936	.75	.917	*	1 296.1
24	.743	.723	*	.74	.729	.729	*	.938	.76	.913	*
25	.746	.736	*	.75	.730	.729	*	.939	.77	.909	*
26	.750	.743	*	.76	.731	.728	*	.941	.78	.901	*
27	.755	.751	*	.77	.729	.724	*	.944	.79	.889	*
28	.761	.760	*	.78	.731	.727	*	.948	.80	.879	*
29	.765	.765	*	.79	.732	.720	*	.954	.81	.870	*
30	.766	.767	*	.80	.735	.714	*	.959	.82	.864	*
31	.768	.764	*	.81	.742	.717	*	.964	.83	.858	*
32	.767	.768	*	.82	.744	.734	*	.970	.84	.851	*
33	.766	.766	*	.83	.753	.748	*	.977	.85	.846	*
34	.764	.758	*	.84	.765	.761	*	.982	.86	.845	*
35	.762	.754	*	.85	.766	.765	*	.990	.87	.841	*
36	.762	.748	*	.86	.764	.764	*	.998	.88	.836	*
37	.761	.740	*	.87	.762	.755	*	1.003	.89	.835	*
38	.760	.731	*	.88	.761	.743	*	1.001	.90	.825	*
39	.760	.724	*	.89	.759	.727	*	.992	.91	.824	*
40	.757	.720	*	.90	.753	.719	*	.981	.92	.824	*
41	.755	.716	*	.91	.744	.718	*	.972	.93	.813	*
42	.754	.714	*	.92	.740	.719	*	.965	.94	.807	*
43	.749	.713	*	.93	.735	.723	*	.948	.95	.785	*
44	.743	.713	*	.94	.737	.724	*	.840	.96	.815	*
45	.740	.714	*	.95	.733	.730	*	.823	.97	1.020	*
46	.738	.716	*	.96	.736	.730	*	.801	.98	1.031	*
47	.740	.719	*	*	*	47	.775	.99	1.092	*	
48	.739	.721	*	*	*	48	.748	.100	1.057	*	
49	.738	.723	*	*	*	49	.718	.101	.849	*	
50	.736	.724	*	*	*	50	.691	.102	.652	*	
51	.737	.724	*	*	*	51	.663	.103	.514	*	
52	.735	.727	*	PRISES COL	*	52	.624	*	REFERENCE PROFIL		
53	.735	.728	*	*	*						
54	.734	.729	*		.796	1.179	*				
55	.734	.730	*		.839	.943	*				
56	.734	.730	*		.899	.855	*				
57	.734	.728	*		.950	.804	*				
58	.734	.726	*		1.121	.763	*				

***** FICHIER AD220 NO(IT)= 4
 6/ 3/84 18H20 M=.760 PI 1.7 TI=TA I=-2.00 (RM) AD220
 DE AD219 4ITER.

MACH DE REFERENCE= .7667 UINF= 250.406 M/S
 TIV=296.5 K PIV= 1735 MB

I	MACH PAROIS			MACH PROFIL			T(K)				
	HAUT	BAS	I	HAUT	BAS	I	EXT	I	INT	I	TPR
1	.768	.762	*	PRISES DOUBLES	*	*	1	.199	53	.654	*
2	.766	.763	*		*	2	.042	54	.660	*	1
3	.766	.762	*	59	.764	.761	*	3	.144	55	.669
4	.765	.764	*	60	.769	.767	*	4	.253	56	.679
5	.766	.767	*	61	.768	.757	*	5	.340	57	.687
6	.765	.766	*			*	6	.405	58	.699	*
7	.765	.763	*	PRISES LAT. GAUCHE	*	*	7	.456	59	.710	*
8	.767	.761	*			*	8	.497	60	.722	*
9	.768	.768	*	62	.765	.766	*	9	.535	61	.736
10	.766	.759	*	63	.763	.766	*	10	.577	62	.750
11	.765	.764	*	64	.766	.759	*	11	.617	63	.766
12	.761	.766	*	65	.770	.751	*	12	.658	64	.782
13	.763	.762	*	66	.782	.763	*	13	.761	65	.800
14	.760	.762	*	67	.806	.803	*	14	.834	66	.820
15	.761	.763	*	68	.807	.805	*	15	.907	67	.842
16	.763	.761	*	69	.803	.780	*	16	.950	68	.867
17	.765	.757	*	70	.796	.752	*	17	.972	69	.893
18	.768	.751	*	71	.776	.749	*	18	.985	70	.919
19	.767	.751	*	72	.766	.758	*	19	.988	71	.945
20	.769	.754	*	73	.771	.768	*	20	.986	72	.966
21	.772	.752	*			*	21	.988	73	.980	*
22	.773	.748	*	PRISES LAT. DROITES	*	*	22	.997	74	.992	*
23	.776	.745	*			*	23	1.000	75	.992	*
24	.779	.753	*	74	.765	.763	*	24	1.001	76	.985
25	.782	.767	*	75	.766	.764	*	25	1.003	77	.978
26	.788	.777	*	76	.765	.761	*	26	1.004	78	.965
27	.794	.788	*	77	.761	.761	*	27	1.008	79	.950
28	.801	.801	*	78	.765	.758	*	28	1.014	80	.936
29	.805	.809	*	79	.768	.749	*	29	1.022	81	.925
30	.807	.813	*	80	.771	.752	*	30	1.029	82	.916
31	.809	.809	*	81	.777	.748	*	31	1.038	83	.909
32	.807	.814	*	82	.780	.766	*	32	1.047	84	.900
33	.806	.810	*	83	.792	.786	*	33	1.057	85	.894
34	.804	.808	*	84	.805	.804	*	34	1.068	86	.894
35	.802	.794	*	85	.807	.810	*	35	1.080	87	.886
36	.803	.786	*	86	.804	.807	*	36	1.098	88	.882
37	.802	.777	*	87	.803	.796	*	37	1.115	89	.879
38	.802	.766	*	88	.802	.780	*	38	1.131	90	.867
39	.802	.758	*	89	.801	.762	*	39	1.117	91	.864
40	.799	.754	*	90	.793	.753	*	40	1.100	92	.862
41	.795	.749	*	91	.783	.751	*	41	1.098	93	.848
42	.795	.747	*	92	.778	.750	*	42	1.093	94	.836
43	.798	.746	*	93	.769	.757	*	43	.923	95	.842
44	.783	.746	*	94	.768	.758	*	44	.863	96	.837
45	.780	.746	*	95	.767	.759	*	45	.851	97	.834
46	.777	.747	*	96	.771	.759	*	46	.829	98	.1.104
47	.778	.750	*			*	47	.802	99	1.175	*
48	.775	.753	*			*	48	.775	100	1.094	*
49	.772	.757	*			*	49	.744	101	.871	*
50	.768	.759	*			*	50	.716	102	.869	*
51	.769	.758	*			*	51	.687	103	.524	*
52	.767	.758	*			PRISES COL	*	52.	.649		
53	.769	.761	*								
54	.769	.763	*			.835 1.205	*				REFERENCE PROFIL
55	.770	.763	*			.873 .900	*				.766
56	.769	.763	*			.927 .852	*				.766
57	.769	.758	*			.973 .820	*				.766
58	.767	.747	*			1.140 .789	*				.765

***** FICHIER AD221 NO(IT)= 5
7 / 3/85 9H45 M=.725 PI 1.7 TI=TA I=-1.00 (RM) AD221
DE AD207 4ITER.

MACH DE REFERENCE=.7320 UINFL= 238.552 M/S
TIV=292.5 K PIY= 1678 MB

***** FICHIER AD223 NO(IT)= 4
7/ 3/85 15H55 M=.775 PI 1.7 TI=TA I=-1.00 (RM) AD223
DE AD209 4ITER.

MACH DE REFERENCE= .7821 UINF= 254.023 M/S
TIV=294.5 K PIV= 1748 MB

***** FICHIER AD224 NO(IT)= 4
7/3/85 16H55 M=.775 PI 1.7 TI=TA I=-0.00 (RM) AD224
DE AD205 4ITER.

MACH DE REFERENCE= .7823 UINF= 254.288 M/S
TIV=295.0 K PIV= 1749 MB

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***** FICHIER AD225 NO(IT)= 6
 7/3/85 17H45 M=.775 PI=1.7 TI=TA I=-0.50 (RM) AD225
 DE AD225 4ITER.

MACH DE REFERENCE= .7857 UINF= 255.522 M/S
 TIV=295.6 K PIV= 1752 MB

MACH PAROIS						MACH PROFIL						T(K)		
I	HAUT	BAS	I	HAUT	BAS	I	EXT	I	INT	*	I	TPR		
1	.787	.775	*	PRISES DOUBLES		*	1	.074	.53	.677	*	1	299.3	
2	.786	.780	*			*	2	.156	.54	.680	*	2	299.0	
3	.785	.776	*	59	.783	.777	*	3	.270	.55	.687	*	3	299.0
4	.782	.777	*	60	.788	.784	*	4	.384	.56	.694	*	4	299.0
5	.780	.779	*	61	.789	.775	*	5	.473	.57	.703	*	5	299.2
6	.781	.780	*				*	6	.532	.58	.713	*	6	299.2
7	.783	.779	*	PRISES LAT. GAUCHE*		*	7	.576	.59	.724	*	7	299.2	
8	.784	.777	*			*	8	.612	.60	.736	*	8	298.3	
9	.785	.784	*	62	.783	.790	*	9	.646	.61	.749	*	9	291.6
10	.785	.776	*	63	.780	.784	*	10	.686	.62	.764	*	10	291.2
11	.783	.780	*	64	.789	.773	*	11	.725	.63	.780	*	11	290.2
12	.778	.779	*	65	.793	.757	*	12	.767	.64	.795	*	12	290.3
13	.782	.773	*	66	.823	.758	*	13	.875	.65	.814	*	13	290.0
14	.780	.776	*	67	.851	.798	*	14	.955	.66	.833	*	14	291.3
15	.783	.777	*	68	.856	.812	*	15	1.037	.67	.856	*	15	291.4
16	.784	.774	*	69	.847	.793	*	16	1.087	.68	.881	*	16	290.7
17	.788	.771	*	70	.825	.760	*	17	1.113	.69	.906	*	17	299.7
18	.790	.765	*	71	.796	.763	*	18	1.130	.70	.932	*	18	290.1
19	.789	.762	*	72	.790	.776	*	19	1.145	.71	.957	*	19	290.0
20	.789	.762	*	73	.798	.787	*	20	1.148	.72	.977	*		
21	.794	.759	*				*	21	1.153	.73	.987	*	I	TPG
22	.801	.752	*	PRISES LAT. DROITES*		*	22	1.160	.74	.992	*			
23	.809	.747	*				*	23	1.163	.75	.984	*	1	295.3
24	.816	.750	*	74	.783	.779	*	24	1.165	.76	.971	*	2	295.3
25	.822	.760	*	75	.784	.780	*	25	1.167	.77	.959	*	3	295.3
26	.829	.768	*	76	.783	.778	*	26	1.170	.78	.943	*	4	295.3
27	.837	.777	*	77	.780	.774	*	27	1.173	.79	.924	*	5	295.3
28	.845	.791	*	78	.788	.772	*	28	1.171	.80	.907	*		
29	.850	.801	*	79	.790	.761	*	29	1.177	.81	.893	*		
30	.853	.809	*	80	.794	.758	*	30	1.181	.82	.880	*		
31	.858	.809	*	81	.811	.750	*	31	1.184	.83	.869	*		
32	.859	.818	*	82	.819	.760	*	32	1.191	.84	.856	*		
33	.858	.817	*	83	.835	.777	*	33	1.196	.85	.847	*		
34	.856	.810	*	84	.850	.798	*	34	1.202	.86	.841	*		
35	.853	.806	*	85	.855	.809	*	35	1.211	.87	.827	*		
36	.851	.799	*	86	.853	.813	*	36	1.226	.88	.812	*		
37	.846	.799	*	87	.851	.807	*	37	1.239	.89	.798	*		
38	.841	.776	*	88	.847	.792	*	38	1.243	.90	.784	*		
39	.837	.766	*	89	.836	.770	*	39	1.233	.91	.783	*		
40	.830	.761	*	90	.822	.760	*	40	1.230	.92	.773	*		
41	.825	.756	*	91	.808	.759	*	41	1.181	.93	.765	*		
42	.823	.754	*	92	.798	.765	*	42	1.061	.94	.759	*		
43	.815	.752	*	93	.790	.772	*	43	.949	.95	.762	*		
44	.807	.754	*	94	.792	.775	*	44	.889	.96	.767	*		
45	.802	.755	*	95	.789	.782	*	45	.852	.97	.789	*		
46	.799	.759	*	96	.787	.784	*	46	.823	.98	.835	*		
47	.797	.765	*				*	47	.736	.99	.906	*		
48	.795	.769	*				*	48	.771	100	.842	*		
49	.794	.772	*				*	49	.745	101	.678	*		
50	.790	.774	*				*	50	.720	102	.500	*		
51	.795	.776	*				*	51	.697	103	.362	*		
52	.789	.777	*	PRISES COL		*	52	.674						
53	.792	.779	*											
54	.792	.782	*		.855	1.218	*				REFERENCE PROFIL			
55	.792	.781	*		.892	.876	*				.782			
56	.789	.781	*		.942	.845	*				.783			
57	.786	.780	*		.985	.923	*				.783			
58	.780	.776	*		1.151	.796	*				.782			

***** FICHIER AD227 NO(IT)= 4
 8/3/84 10H20 M=.725 PI=2.5 TI=TA I=-0.25 (RM) AD227
 DE AD226 SITER.

MACH DE REFERENCE= .7346 UINF= 240.793 M/S
 TIV=296.1 K PIV= 2509 MB

MACH PAROIS						*	MACH PROFIL			*	T(K)			
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.734	.725	*	PRISES DOUBLES		*	1	.085	53	.652	*	1	292.1	
2	.728	.725	*			*	2	.202	54	.652	*	2	290.3	
3	.730	.724	*	59	.727	.722	*	3	.309	55	.657	*	3	290.5
4	.734	.732	*	60	.736	.732	*	4	.421	56	.663	*	4	290.5
5	.735	.736	*	61	.738	.728	*	5	.505	57	.670	*	5	290.6
6	.729	.729	*			*	6	.558	58	.678	*	6	290.7	
7	.727	.723	*	PRISES LAT. GAUCHE	S*	*	7	.598	59	.686	*	7	290.8	
8	.734	.728	*			*	8	.631	60	.696	*	8	291.6	
9	.738	.739	*	62	.731	.733	*	9	.662	61	.708	*	9	292.7
10	.734	.724	*	63	.736	.732	*	10	.702	62	.721	*	10	292.4
11	.734	.730	*	64	.737	.727	*	11	.738	63	.734	*	11	291.9
12	.733	.734	*	65	.743	.711	*	12	.776	64	.747	*	12	291.8
13	.736	.728	*	66	.764	.713	*	13	.877	65	.763	*	13	292.0
14	.731	.725	*	67	.780	.742	*	14	.952	66	.777	*	14	292.5
15	.731	.727	*	68	.778	.750	*	15	1.020	67	.796	*	15	292.6
16	.734	.728	*	69	.772	.737	*	16	1.065	68	.815	*	16	291.1
17	.737	.725	*	70	.766	.715	*	17	1.071	69	.835	*	17	291.0
18	.740	.719	*	71	.742	.718	*	18	1.077	70	.852	*	18	290.9
19	.740	.718	*	72	.736	.723	*	19	1.072	71	.869	*	19	291.5
20	.742	.717	*	73	.745	.735	*	20	1.042	72	.879	*		
21	.746	.714	*			*	21	1.027	73	.883	*	I	TPG	
22	.750	.707	*	PRISES LAT. DROITES	S*	22		1.022	74	.896	*			
23	.755	.703	*			*	23	1.018	75	.881	*	1	296.1	
24	.759	.706	*	74	.731	.731	*	24	1.010	76	.873	*	2	296.1
25	.763	.714	*	75	.728	.724	*	25	.997	77	.866	*	3	296.9
26	.767	.721	*	76	.732	.727	*	26	.978	78	.855	*	4	296.0
27	.771	.727	*	77	.731	.725	*	27	.986	79	.842	*	5	296.0
28	.776	.738	*	78	.737	.726	*	28	.991	80	.829	*		
29	.779	.745	*	79	.740	.716	*	29	.995	81	.818	*		
30	.779	.750	*	80	.745	.712	*	30	.997	82	.808	*		
31	.781	.749	*	81	.756	.705	*	31	.999	83	.798	*		
32	.780	.754	*	82	.763	.715	*	32	1.004	84	.798	*		
33	.778	.754	*	83	.770	.727	*	33	1.005	85	.781	*		
34	.776	.748	*	84	.778	.743	*	34	1.008	86	.775	*		
35	.773	.746	*	85	.780	.750	*	35	1.011	87	.763	*		
36	.773	.741	*	86	.776	.751	*	36	1.016	88	.748	*		
37	.771	.734	*	87	.774	.747	*	37	1.013	89	.734	*		
38	.770	.727	*	88	.772	.736	*	38	1.004	90	.719	*		
39	.770	.720	*	89	.769	.722	*	39	.985	91	.729	*		
40	.767	.718	*	90	.763	.716	*	40	.961	92	.714	*		
41	.764	.713	*	91	.755	.716	*	41	.936	93	.707	*		
42	.764	.712	*	92	.743	.718	*	42	.907	94	.704	*		
43	.760	.711	*	93	.738	.723	*	43	.880	95	.701	*		
44	.754	.712	*	94	.738	.723	*	44	.849	96	.705	*		
45	.750	.713	*	95	.733	.733	*	45	.819	97	.707	*		
46	.746	.715	*	96	.744	.733	*	46	.787	98	.748	*		
47	.743	.719	*			*	47	.758	99	.803	*			
48	.741	.721	*			*	48	.731	100	.746	*			
49	.741	.723	*			*	49	.706	101	.695	*			
50	.740	.726	*			*	50	.685	102	.442	*			
51	.739	.724	*			*	51	.665	103	.314	*			
52	.739	.731	*	PRISES COL		*	52	.650						
53	.737	.730	*											
54	.734	.729	*		.796	1.179	*							
55	.736	.731	*		.825	1.244	*							
56	.739	.734	*		.898	1.349	*							
57	.742	.731	*		.950	.912	*							
58	.744	.728	*		1.122	.842	*							
								REFERENCE PROFIL						

***** FICHIER AD229 NO(IT)= 4
8/ 3/85 11H55 M=.723 PI=3.3 TI=TA I=-0.25 (RMP) AD229
DE AD228 4 IEME ITE

MACH DE REFERENCE= .7299 UINF= 239.878 M/S
TIV=297.3 K PIV= 3301 MB

MACH PAROIS						MACH PROFIL						T(K)		
I	HAUT	BAS	I	HAUT	BAS	I	EXT	I	INT	I	TPR			
1	.731	.722	*	PRISES DOUBLES	*	*	1	.085	53	.649	*	1	293.7	
2	.724	.722	*		*	*	2	.201	54	.649	*	2	292.1	
3	.727	.721	*	59	.724	.718	*	3	.308	55	.653	*	3	292.3
4	.731	.729	*	60	.733	.730	*	4	.421	56	.659	*	4	292.0
5	.731	.733	*	61	.735	.724	*	5	.505	57	.665	*	5	292.1
6	.726	.726	*			*	6	.556	58	.674	*	6	292.1	
7	.724	.720	*	PRISES LAT. GAUCHE	S*	*	7	.597	59	.682	*	7	292.1	
8	.731	.724	*			*	8	.630	60	.691	*	8	292.3	
9	.734	.736	*	62	.727	.730	*	9	.660	61	.703	*	9	294.1
10	.730	.721	*	63	.735	.729	*	10	.702	62	.716	*	10	293.8
11	.730	.727	*	64	.733	.724	*	11	.736	63	.729	*	11	293.3
12	.728	.731	*	65	.741	.707	*	12	.775	64	.742	*	12	293.1
13	.733	.724	*	66	.759	.711	*	13	.874	65	.757	*	13	293.4
14	.729	.722	*	67	.774	.739	*	14	.946	66	.769	*	14	293.9
15	.729	.723	*	68	.772	.746	*	15	1.014	67	.787	*	15	294.1
16	.732	.724	*	69	.766	.732	*	16	1.036	68	.807	*	16	292.8
17	.732	.721	*	70	.760	.711	*	17	1.059	69	.826	*	17	292.9
18	.733	.715	*	71	.739	.714	*	18	1.060	70	.843	*	18	292.5
19	.733	.713	*	72	.733	.720	*	19	1.030	71	.860	*	19	293.3
20	.738	.712	*	73	.737	.732	*	20	1.022	72	.870	*		
21	.745	.710	*			*	21	1.010	73	.874	*	I	TPG	
22	.747	.706	*	PRISES LAT. DROITES	S*	*	22	1.011	74	.876	*			
23	.751	.702	*			*	23	.992	75	.872	*	1	297.2	
24	.753	.703	*	74	.728	.729	*	24	.988	76	.863	*	2	297.2
25	.758	.710	*	75	.726	.720	*	25	.985	77	.857	*	3	297.2
26	.762	.716	*	76	.729	.723	*	26	.981	78	.846	*	4	297.1
27	.766	.722	*	77	.728	.722	*	27	.982	79	.834	*	5	297.1
28	.770	.733	*	78	.733	.722	*	28	.983	80	.820	*		
29	.772	.740	*	79	.733	.712	*	29	.986	81	.810	*		
30	.772	.745	*	80	.743	.709	*	30	.987	82	.800	*		
31	.774	.743	*	81	.752	.705	*	31	.987	83	.791	*		
32	.772	.749	*	82	.758	.710	*	32	.991	84	.791	*		
33	.771	.748	*	83	.765	.722	*	33	.992	85	.777	*		
34	.769	.742	*	84	.772	.739	*	34	.993	86	.770	*		
35	.766	.740	*	85	.774	.745	*	35	.996	87	.757	*		
36	.767	.736	*	86	.770	.746	*	36	.999	88	.743	*		
37	.765	.729	*	87	.768	.742	*	37	.997	89	.735	*		
38	.764	.722	*	88	.766	.731	*	38	.990	90	.717	*		
39	.764	.716	*	89	.763	.718	*	39	.973	91	.730	*		
40	.761	.714	*	90	.756	.711	*	40	.951	92	.710	*		
41	.758	.710	*	91	.749	.712	*	41	.926	93	.700	*		
42	.758	.708	*	92	.741	.714	*	42	.899	94	.700	*		
43	.753	.707	*	93	.735	.720	*	43	.873	95	.698	*		
44	.748	.708	*	94	.735	.719	*	44	.842	96	.702	*		
45	.743	.709	*	95	.730	.725	*	45	.813	97	.705	*		
46	.741	.711	*	96	.736	.725	*	46	.781	98	.746	*		
47	.740	.716	*			*	47	.752	99	.802	*			
48	.738	.717	*			*	48	.726	100	.745	*			
49	.738	.720	*			*	49	.701	101	.606	*			
50	.736	.723	*			*	50	.682	102	.443	*			
51	.734	.720	*			*	51	.664	103	.315	*			
52	.736	.727	*	PRISES COL	*	*	52	.651						
53	.734	.726	*											
54	.731	.726	*		.789	1.177	*							
55	.732	.729	*		.835	1.245	*							
56	.734	.731	*		.896	.909	*							
57	.735	.725	*		.948	.828	*							
58	.735	.717	*		1.122	.781	*							
								REFERENCE PROFIL						

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***** FICHIER AD230 NO(IT)= 4
8/ 3/85 16H15 M=.723 PI=2.9 TI=240 I=-0.25 (RMPT) AD230
DE AD229 4 IEUME ITE

MACH DE REFERENCE= .7299 UINF= 215.723 M/S
TIY=240.4 K PIV= 2903 MB

MACH PAROIS						*	MACH PROFIL				*	T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPP	
1	.731	.721	*	PRISES DOUBLES		*	1	.073	.53	.649	*	1	236.3	
2	.726	.724	*			*	2	.188	.54	.649	*	2	234.3	
3	.727	.722	*	59	.726	.721	*	3	.299	.55	.653	*	3	234.3
4	.729	.728	*	60	.735	.732	*	4	.412	.56	.659	*	4	235.2
5	.728	.732	*	61	.734	.724	*	5	.497	.57	.666	*	5	235.1
6	.726	.727	*			*	6	.548	.58	.674	*	6	235.0	
7	.726	.723	*	PRISES LAT. GAUCHE	S	*	7	.589	.59	.682	*	7	235.9	
8	.732	.724	*			*	8	.623	.60	.692	*	8	235.7	
9	.734	.735	*	62	.727	.731	*	9	.653	.61	.704	*	9	237.3
10	.733	.723	*	63	.735	.732	*	10	.696	.62	.717	*	10	236.3
11	.731	.730	*	64	.734	.723	*	11	.730	.63	.731	*	11	235.9
12	.728	.732	*	65	.737	.706	*	12	.768	.64	.743	*	12	235.9
13	.733	.726	*	66	.759	.711	*	13	.867	.65	.759	*	13	236.2
14	.730	.722	*	67	.773	.740	*	14	.942	.66	.773	*	14	236.3
15	.729	.722	*	68	.771	.747	*	15	1.005	.67	.791	*	15	236.3
16	.732	.721	*	69	.766	.733	*	16	1.063	.68	.810	*	16	236.3
17	.733	.720	*	70	.760	.712	*	17	1.054	.69	.829	*	17	235.0
18	.735	.718	*	71	.736	.712	*	18	1.051	.70	.847	*	18	235.3
19	.733	.715	*	72	.733	.722	*	19	1.038	.71	.863	*	19	237.0
20	.735	.711	*	73	.736	.732	*	20	.999	.72	.873	*		
21	.739	.708	*			*	21	1.000	.73	.877	*	I	TPG	
22	.742	.706	*	PRISES LAT. DROITES	S	*	22	1.014	.74	.880	*			
23	.747	.703	*			*	23	.995	.75	.875	*	1	240.8	
24	.752	.704	*	74	.727	.729	*	24	.989	.76	.866	*	2	240.9
25	.758	.711	*	75	.729	.723	*	25	.984	.77	.860	*	3	240.6
26	.762	.717	*	76	.731	.725	*	26	.979	.78	.849	*	4	240.2
27	.766	.723	*	77	.729	.723	*	27	.980	.79	.836	*	5	240.4
28	.769	.734	*	78	.733	.721	*	28	.981	.80	.823	*		
29	.771	.741	*	79	.733	.714	*	29	.982	.81	.813	*		
30	.771	.746	*	80	.738	.707	*	30	.983	.82	.803	*		
31	.773	.745	*	81	.748	.705	*	31	.983	.83	.793	*		
32	.772	.751	*	82	.758	.710	*	32	.987	.84	.783	*		
33	.770	.750	*	83	.765	.723	*	33	.987	.85	.773	*		
34	.768	.744	*	84	.771	.740	*	34	.989	.86	.774	*		
35	.765	.742	*	85	.772	.746	*	35	.992	.87	.760	*		
36	.765	.737	*	86	.769	.747	*	36	.996	.88	.748	*		
37	.764	.730	*	87	.767	.743	*	37	.992	.89	.739	*		
38	.763	.723	*	88	.765	.733	*	38	.984	.90	.721	*		
39	.764	.717	*	89	.763	.719	*	39	.968	.91	.727	*		
40	.760	.715	*	90	.757	.712	*	40	.947	.92	.715	*		
41	.758	.710	*	91	.750	.712	*	41	.923	.93	.704	*		
42	.758	.709	*	92	.739	.713	*	42	.895	.94	.699	*		
43	.755	.707	*	93	.734	.720	*	43	.869	.95	.696	*		
44	.749	.708	*	94	.736	.721	*	44	.840	.96	.705	*		
45	.745	.709	*	95	.731	.727	*	45	.809	.97	.710	*		
46	.741	.710	*	96	.735	.726	*	46	.779	.98	.752	*		
47	.738	.714	*			*	47	.751	.99	.811	*			
48	.736	.716	*			*	48	.725	100	.754	*			
49	.736	.720	*			*	49	.701	101	.613	*			
50	.735	.723	*			*	50	.682	102	.449	*			
51	.734	.722	*			*	51	.664	103	.321	*			
52	.735	.728	*		PRISES COL	*	52	.651						
53	.734	.726	*											
54	.731	.726	*		.792	1.177	*							
55	.732	.728	*		.827	1.244	*							
56	.733	.730	*		.896	.911	*							
57	.733	.725	*		.948	.831	*							
58	.735	.721	*		1.124	.782	*							

REFERENCE PROFIL

.728

.731

.728

.729

.725

FICHIER RD233 N°(IT)= 4
 11/ 3/85 15H10 M=.727 PI=1.7 TI=296 I=-0.25 (RM) AD233
 DE AD226 5 IEUME ITE

MACH DE REFERENCE= .7280 UINF= 237.665 M/S
 TIV=293.2 K PIV= 1688 MB

I	MACH PAROIS				*	MACH PROFIL				*	T(K)			
	HAUT	BAS	I	HAUT	BAS	I	EXT	I	INT	I	TPR			
1	.730	.720	*	PRISES DOUBLES	*	*	1	.070	53	.651	*	1	299.4	
2	.728	.723	*		*	*	2	.193	54	.651	*	2	299.3	
3	.728	.722	*	59	.727	.722	*	3	.301	55	.653	*	3	291.4
4	.728	.725	*	60	.733	.728	*	4	.413	56	.660	*	4	291.3
5	.727	.728	*	61	.731	.721	*	5	.499	57	.666	*	5	290.1
6	.726	.726	*			*	6	.553	58	.674	*	6	299.3	
7	.727	.723	*	PRISES LAT. GAUCHE	*	*	7	.594	59	.682	*	7	299.3	
8	.730	.723	*			*	8	.627	60	.692	*	8	290.0	
9	.731	.730	*	62	.727	.727	*	9	.658	61	.704	*	9	291.0
10	.730	.721	*	63	.728	.728	*	10	.695	62	.717	*	10	290.7
11	.730	.726	*	64	.733	.721	*	11	.732	63	.730	*	11	290.4
12	.727	.726	*	65	.739	.704	*	12	.770	64	.742	*	12	290.1
13	.731	.723	*	66	.756	.706	*	13	.871	65	.758	*	13	290.4
14	.728	.722	*	67	.771	.735	*	14	.942	66	.774	*	14	290.0
15	.730	.723	*	68	.770	.744	*	15	1.012	67	.791	*	15	291.2
16	.731	.721	*	69	.765	.731	*	16	1.043	68	.811	*	16	299.5
17	.732	.719	*	70	.758	.710	*	17	1.058	69	.830	*	17	293.2
18	.732	.715	*	71	.740	.712	*	18	1.060	70	.848	*	18	292.2
19	.733	.712	*	72	.731	.720	*	19	1.048	71	.863	*	19	288.4
20	.737	.709	*	73	.731	.729	*	20	1.027	72	.874	*		TPG
21	.741	.706	*			*	21	1.014	73	.877	*	I		
22	.743	.704	*	PRISES LAT. DROITES	*	*	22	1.010	74	.880	*			
23	.746	.700	*			*	23	1.004	75	.876	*	1	293.3	
24	.750	.701	*	74	.728	.726	*	24	.998	76	.870	*	2	293.3
25	.755	.708	*	75	.728	.723	*	25	.994	77	.861	*	3	293.2
26	.759	.713	*	76	.729	.723	*	26	.986	78	.850	*	4	293.2
27	.763	.719	*	77	.728	.721	*	27	.982	79	.837	*	5	293.1
28	.768	.730	*	78	.732	.721	*	28	.982	80	.824	*		
29	.770	.740	*	79	.733	.711	*	29	.983	81	.813	*		
30	.770	.742	*	80	.741	.706	*	30	.984	82	.803	*		
31	.773	.742	*	81	.747	.702	*	31	.985	83	.794	*		
32	.771	.748	*	82	.753	.707	*	32	.988	84	.783	*		
33	.770	.747	*	83	.763	.719	*	33	.991	85	.775	*		
34	.768	.742	*	84	.771	.735	*	34	.995	86	.769	*		
35	.766	.739	*	85	.772	.742	*	35	.998	87	.757	*		
36	.766	.734	*	86	.768	.744	*	36	1.003	88	.744	*		
37	.764	.727	*	87	.766	.739	*	37	1.001	89	.731	*		
38	.763	.721	*	88	.765	.730	*	38	.993	90	.720	*		
39	.764	.714	*	89	.762	.716	*	39	.976	91	.718	*		
40	.760	.711	*	90	.756	.710	*	40	.956	92	.710	*		
41	.757	.708	*	91	.748	.710	*	41	.930	93	.703	*		
42	.757	.706	*	92	.742	.713	*	42	.903	94	.699	*		
43	.752	.705	*	93	.734	.717	*	43	.873	95	.697	*		
44	.746	.706	*	94	.734	.719	*	44	.843	96	.700	*		
45	.743	.706	*	95	.731	.729	*	45	.813	97	.704	*		
46	.741	.709	*	96	.731	.728	*	46	.782	98	.744	*		
47	.743	.713	*			*	47	.753	99	.796	*			
48	.738	.715	*			*	48	.727	100	.739	*			
49	.736	.717	*			*	49	.702	101	.599	*			
50	.732	.719	*			*	50	.680	102	.439	*			
51	.732	.719	*			*	51	.662	103	.309	*			
52	.732	.723	*	PRISES COL	*	*	52	.645						
53	.733	.724	*											
54	.732	.725	*		.793	1.177	*							
55	.733	.725	*		.836	.989	*							
56	.731	.735	*		.897	.864	*							
57	.730	.726	*		.947	.809	*							
58	.727	.728	*		1.120	.766	*							

REFERENCE PROFIL

.730

.730

.728

.727

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD234 NO(IT)= 4
11/ 3/84 16H 5 M=.727 PI=1.7 TI=120 I=-0.25 (RM) AD234
DE AD230 4 IEME ITE

MACH DE REFERENCE= .7309 UINF= 152.129 M/S
TIV=119.3 K PIV= 1627 MB

***** FICHIER AD235 NO(IT)= 4
 11/3/85 17H15 M=.760 PI=1.7 TI=300 I=+0.25 (RM) AD235
 DE AD65 4 IEME ITE

MACH DE REFERENCE= .7634 UINF= 247.931 M/S
 TIV=293.0 K PIV= 1723 MB

MACH PAROIS						*	MACH PROFIL			*	T(K)			
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.767	.754	*	PRISES DOUBLES		*	1	.069	.53	.651	*	1	289.0	
2	.767	.753	*			*	2	.245	.54	.656	*	2	287.7	
3	.767	.756	*	59	.763	.755	*	3	.357	.55	.662	*	3	288.9
4	.764	.756	*	60	.769	.763	*	4	.473	.56	.671	*	4	289.2
5	.762	.759	*	61	.768	.755	*	5	.561	.57	.678	*	5	289.4
6	.762	.758	*				*	.613	.58	.688	*	6	289.2	
7	.763	.757	*	PRISES LAT. GAUCHE	S	*	7	.651	.59	.699	*	7	287.9	
8	.764	.756	*			*	8	.682	.60	.711	*	8	287.3	
9	.765	.762	*	62	.765	.760	*	9	.712	.61	.723	*	9	289.8
10	.766	.754	*	63	.762	.762	*	10	.750	.62	.737	*	10	289.5
11	.766	.760	*	64	.770	.752	*	11	.786	.63	.751	*	11	289.2
12	.761	.759	*	65	.777	.732	*	12	.826	.64	.765	*	12	289.0
13	.765	.755	*	66	.810	.726	*	13	.933	.65	.781	*	13	289.3
14	.763	.756	*	67	.832	.758	*	14	1.008	.66	.798	*	14	289.7
15	.764	.757	*	68	.833	.774	*	15	1.086	.67	.818	*	15	290.0
16	.765	.755	*	69	.824	.761	*	16	1.130	.68	.839	*	16	287.2
17	.769	.751	*	70	.809	.736	*	17	1.162	.69	.859	*	17	292.4
18	.773	.743	*	71	.778	.741	*	18	1.178	.70	.879	*	18	289.8
19	.773	.741	*	72	.770	.755	*	19	1.191	.71	.896	*	19	283.4
20	.773	.739	*	73	.763	.765	*	20	1.195	.72	.908	*		
21	.778	.735	*				*	21	1.197	.73	.912	*	I	TPG
22	.785	.726	*	PRISES LAT. DROITES	S	*	22	1.202	.74	.913	*			
23	.794	.718	*			*	23	1.203	.75	.908	*	1	292.9	
24	.802	.719	*	74	.765	.759	*	24	1.203	.76	.900	*	2	293.0
25	.809	.727	*	75	.764	.756	*	25	1.205	.77	.888	*	3	292.9
26	.816	.733	*	76	.764	.758	*	26	1.207	.78	.874	*	4	292.8
27	.822	.739	*	77	.763	.754	*	27	1.208	.79	.858	*	5	292.8
28	.829	.751	*	78	.769	.752	*	28	1.210	.80	.843	*		
29	.831	.762	*	79	.773	.739	*	29	1.213	.81	.830	*		
30	.832	.766	*	80	.778	.734	*	30	1.217	.82	.818	*		
31	.836	.767	*	81	.796	.721	*	31	1.220	.83	.807	*		
32	.834	.775	*	82	.807	.729	*	32	1.225	.84	.794	*		
33	.833	.775	*	83	.821	.739	*	33	1.225	.85	.784	*		
34	.830	.769	*	84	.831	.758	*	34	1.214	.86	.776	*		
35	.826	.767	*	85	.834	.769	*	35	1.200	.87	.760	*		
36	.826	.762	*	86	.831	.773	*	36	1.193	.88	.744	*		
37	.822	.754	*	87	.828	.770	*	37	1.192	.89	.726	*		
38	.820	.745	*	88	.824	.759	*	38	1.189	.90	.714	*		
39	.820	.737	*	89	.819	.743	*	39	1.005	.91	.707	*		
40	.814	.733	*	90	.807	.736	*	40	.918	.92	.697	*		
41	.809	.730	*	91	.789	.739	*	41	.932	.93	.687	*		
42	.807	.728	*	92	.781	.742	*	42	.924	.94	.681	*		
43	.796	.730	*	93	.771	.749	*	43	.909	.95	.675	*		
44	.787	.733	*	94	.773	.753	*	44	.882	.96	.678	*		
45	.782	.734	*	95	.768	.762	*	45	.853	.97	.673	*		
46	.779	.737	*	96	.765	.762	*	46	.823	.98	.699	*		
47	.779	.741	*				*	47	.794	.99	.735	*		
48	.777	.745	*				*	48	.764	100	.675	*		
49	.775	.749	*				*	49	.734	101	.541	*		
50	.771	.753	*				*	50	.706	102	.384	*		
51	.770	.754	*				*	51	.678	103	.256	*		
52	.769	.757	*	PRISES COL		*	52	.653						
53	.771	.759	*											
54	.770	.759	*		.830	1.204	*				REFERENCE PROFIL			
55	.771	.759	*		.870	.896	*				.763			
56	.767	.759	*		.924	.843	*				.762			
57	.764	.759	*		.970	.815	*				.763			
58	.756	.760	*		1.139	.785	*				.761			

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD236 NO(IT)= 4
12/ 3/85 9H10 M=.757 PI=1.7 TI=300 I=+0.25 (RM) AD236
DE AD235 4 IEME ITE

MACH DE REFERENCE= .7607 UINF= 246.588 M/S
TIV=291.6 K PIV= 1718 MB

MACH PAROIS

***** FICHIER RD238 NO(IT)= 4
12/ 3/84 12H 5 M=.754 PI=3.3 TI=300 I=+0.25 (RMP) RD238
DE RD237 4IEME ITE

MACH DE REFERENCE= .7600 UINF= 248.202 M/S
TIV=295.0 K PIV= 3292 MB

MACH PAROIS						MACH PROFIL						TICK		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.762	.751	*	PRISES DOUBLES		*	1	.971	53	.665	*	1	291.8	
2	.757	.752	*			*	2	.241	54	.665	*	2	289.5	
3	.758	.749	*	59	.755	.747	*	3	.354	55	.669	*	3	289.2
4	.760	.755	*	60	.766	.757	*	4	.471	56	.675	*	4	289.0
5	.759	.758	*	61	.766	.748	*	5	.558	57	.682	*	5	289.2
6	.756	.753	*			*	6	.608	58	.691	*	6	289.7	
7	.755	.749	*	PRISES LAT. GRUCHES		*	7	.647	59	.701	*	7	289.5	
8	.761	.753	*			*	8	.679	60	.710	*	8	290.6	
9	.765	.765	*	62	.758	.758	*	9	.709	61	.723	*	9	292.3
10	.761	.751	*	63	.763	.761	*	10	.749	62	.737	*	10	292.0
11	.760	.757	*	64	.766	.758	*	11	.783	63	.750	*	11	291.5
12	.756	.759	*	65	.774	.730	*	12	.827	64	.763	*	12	291.3
13	.761	.752	*	66	.803	.739	*	13	.930	65	.779	*	13	291.7
14	.758	.749	*	67	.824	.756	*	14	1.009	66	.793	*	14	292.2
15	.753	.750	*	68	.824	.769	*	15	1.084	67	.812	*	15	292.5
16	.762	.749	*	69	.814	.756	*	16	1.135	68	.834	*	16	289.9
17	.764	.747	*	70	.799	.734	*	17	1.159	69	.854	*	17	289.6
18	.766	.742	*	71	.772	.737	*	18	1.174	70	.873	*	18	289.5
19	.767	.739	*	72	.764	.749	*	19	1.187	71	.889	*	19	290.2
20	.769	.736	*	73	.764	.761	*	20	1.190	72	.901	*		
21	.779	.732	*			*	21	1.191	73	.905	*	I	TPG	
22	.784	.727	*	PRISES LAT. DROITES		*	22	1.195	74	.906	*			
23	.791	.721	*			*	23	1.195	75	.900	*	1	295.8	
24	.796	.722	*	74	.758	.755	*	24	1.195	76	.892	*	2	295.8
25	.801	.729	*	75	.757	.750	*	25	1.194	77	.881	*	3	295.8
26	.808	.735	*	76	.760	.753	*	26	1.194	78	.868	*	4	295.8
27	.814	.740	*	77	.757	.749	*	27	1.193	79	.852	*	5	295.7
28	.820	.750	*	78	.765	.748	*	28	1.191	80	.837	*		
29	.822	.753	*	79	.768	.738	*	29	1.185	81	.825	*		
30	.823	.763	*	80	.776	.732	*	30	1.187	82	.813	*		
31	.826	.764	*	81	.793	.725	*	31	1.185	83	.802	*		
32	.824	.771	*	82	.801	.729	*	32	1.184	84	.790	*		
33	.822	.770	*	83	.812	.739	*	33	1.085	85	.783	*		
34	.819	.766	*	84	.821	.756	*	34	.986	86	.775	*		
35	.816	.764	*	85	.824	.763	*	35	.993	87	.768	*		
36	.815	.760	*	86	.822	.769	*	36	1.019	88	.743	*		
37	.811	.753	*	87	.818	.757	*	37	1.047	89	.725	*		
38	.809	.744	*	88	.813	.755	*	38	1.071	90	.708	*		
39	.806	.737	*	89	.805	.740	*	39	1.041	91	.713	*		
40	.801	.735	*	90	.786	.735	*	40	.996	92	.700	*		
41	.797	.731	*	91	.786	.737	*	41	.968	93	.692	*		
42	.796	.729	*	92	.774	.737	*	42	.937	94	.686	*		
43	.791	.730	*	93	.765	.749	*	43	.907	95	.681	*		
44	.785	.732	*	94	.766	.748	*	44	.875	96	.682	*		
45	.780	.734	*	95	.763	.745	*	45	.843	97	.679	*		
46	.777	.735	*	96	.763	.746	*	46	.810	98	.707	*		
47	.773	.738	*			*	47	.789	99	.749	*			
48	.770	.742	*			*	48	.751	100	.688	*			
49	.768	.749	*			*	49	.735	101	.551	*			
50	.765	.754	*			*	50	.702	102	.394	*			
51	.764	.749	*			*	51	.681	103	.267	*			
52	.766	.752	*	PRISES COL		*	52	.661						
53	.766	.753	*											
54	.765	.757	*		.822	1.193	*							
55	.765	.759	*		.864	1.234	*							
56	.764	.761	*		.819	.937	*							
57	.763	.749	*		.966	.355	*							
58	.757	.729	*		1.138	.815	*							
									REFERENCE PROFIL					

***** FICHIER AD244 NO(IT)= 4
13/ 3/85 16H50 M=.755 PI=1.7 TI=120 I=+0.25 (RMP) AD244
DE AD239 4' ITER.

MACH DE REFERENCE= .7622 UINF= 157.673 M/S
TIY=119.1 K PIV= 1639 MB

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD246 NO(ITER)= 4
14/ 3/85 11H25 M=.759 PI=1.7 TI=300 I=+1.00 (RM) AD246
DE AD245 4' ITER.

MACH DE REFERENCE= .7646 UINF= 247.322 M/S
TIV=291.9 K PIV= 1690 MB

***** FICHIER AD247 NO(IT)= 4
14/ 3/85 14H35 M=.726 PI=1.7 TI=300 I=+1.00 (RM) AD247
DE AD246 4' ITER.

MACH DE REFERENCE= .7320 UINF= 238.690 M/S
TIV=292.8 K PIY= 1677 MB

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD248 NO(IT)= 4
15/ 3/85 9H30 M=.695 PI=1.7 TI=300 I=+1.00 (RM) AD248
DE AD247 4' ITER.

MACH DE REFERENCE= .6988 UINF= 228.316 M/S
TIV=291.5 K PIV= 1599 MB

MACH PAROIS						MACH PROFIL						T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.703	.692	*	PRISES DOUBLES		*	1	0.000	53	.644	*	1	298.4	
2	.702	.695	*			*	2	.309	54	.639	*	2	287.9	
3	.702	.694	*	59	.699	.692	*	3	.422	55	.640	*	3	287.5
4	.701	.694	*	60	.704	.697	*	4	.531	56	.644	*	4	287.5
5	.699	.696	*	61	.704	.690	*	5	.620	57	.648	*	5	287.5
6	.699	.695	*				*	6	.696	58	.654	*	6	287.7
7	.699	.694	*	PRISES LAT. GAUCHE	S	*	7	.697	59	.661	*	7	287.9	
8	.701	.694	*			*	8	.721	60	.669	*	8	298.4	
9	.701	.699	*	62	.700	.696	*	9	.747	61	.677	*	9	299.3
10	.701	.693	*	63	.700	.698	*	10	.778	62	.689	*	10	289.0
11	.699	.696	*	64	.704	.688	*	11	.811	63	.700	*	11	288.7
12	.696	.696	*	65	.715	.675	*	12	.848	64	.710	*	12	288.6
13	.700	.692	*	66	.732	.669	*	13	.936	65	.723	*	13	288.9
14	.699	.691	*	67	.743	.692	*	14	.991	66	.737	*	14	289.2
15	.701	.691	*	68	.742	.701	*	15	1.066	67	.751	*	15	289.3
16	.703	.689	*	69	.738	.693	*	16	1.104	68	.767	*	16	288.6
17	.705	.687	*	70	.729	.679	*	17	1.123	69	.782	*	17	288.5
18	.709	.683	*	71	.712	.681	*	18	1.112	70	.795	*	18	288.7
19	.707	.683	*	72	.704	.693	*	19	1.017	71	.807	*	19	288.8
20	.711	.681	*	73	.700	.697	*	20	1.001	72	.813	*		
21	.713	.676	*				*	21	.993	73	.814	*	I	TPG
22	.719	.668	*	PRISES LAT. DROITES	S	*	22	.991	74	.814	*			
23	.723	.662	*			*	23	.976	75	.809	*	1	291.5	
24	.727	.664	*	74	.701	.696	*	24	.968	76	.803	*	2	291.4
25	.732	.671	*	75	.700	.694	*	25	.960	77	.793	*	3	291.4
26	.735	.674	*	76	.699	.694	*	26	.954	78	.782	*	4	291.4
27	.737	.680	*	77	.699	.691	*	27	.951	79	.770	*	5	291.4
28	.741	.688	*	78	.703	.688	*	28	.948	80	.757	*		
29	.741	.694	*	79	.711	.680	*	29	.946	81	.746	*		
30	.742	.698	*	80	.714	.676	*	30	.945	82	.735	*		
31	.743	.698	*	81	.724	.664	*	31	.942	83	.725	*		
32	.742	.704	*	82	.730	.670	*	32	.940	84	.713	*		
33	.741	.703	*	83	.737	.679	*	33	.939	85	.704	*		
34	.739	.699	*	84	.741	.691	*	34	.937	86	.695	*		
35	.738	.698	*	85	.742	.698	*	35	.936	87	.681	*		
36	.738	.695	*	86	.740	.701	*	36	.934	88	.665	*		
37	.736	.691	*	87	.739	.698	*	37	.929	89	.647	*		
38	.736	.686	*	88	.737	.691	*	38	.919	90	.633	*		
39	.735	.682	*	89	.734	.683	*	39	.906	91	.624	*		
40	.732	.680	*	90	.728	.680	*	40	.887	92	.614	*		
41	.729	.678	*	91	.717	.682	*	41	.865	93	.604	*		
42	.728	.677	*	92	.714	.682	*	42	.840	94	.596	*		
43	.722	.678	*	93	.705	.688	*	43	.816	95	.587	*		
44	.717	.679	*	94	.705	.691	*	44	.783	96	.587	*		
45	.713	.680	*	95	.704	.699	*	45	.760	97	.577	*		
46	.713	.681	*	96	.700	.697	*	46	.735	98	.593	*		
47	.714	.682	*				*	47	.712	99	.596	*		
48	.711	.684	*				*	48	.693	100	.538	*		
49	.708	.688	*				*	49	.678	101	.421	*		
50	.704	.692	*				*	50	.667	102	.282	*		
51	.704	.692	*				*	51	.659	103	.161	*		
52	.705	.692	*				*	52	.651					
53	.706	.692	*											
54	.705	.693	*											
55	.704	.695	*											
56	.702	.696	*											
57	.700	.696	*											
58	.695	.696	*											

REFERENCE PROFIL

.766 1.158 * .700
.813 .934 * .791
.878 .843 * .699
.934 .781 * .699
1.104 .735 *

***** FICHIER AD249 NO(IT)= 4
15/ 3/85 10H50 M=.696 PI=1.7 TI=300 I=+0.00 (RM) AD249
DE AD248 4' ITER.

MACH DE REFERENCE= .6997 UINF= 228.890 M/S
TIV=292.3 K PIV= 1597 MB

***** FICHIER AD250 NO(IT)= 4
 15/ 3/84 11H50 M=.726 PI=1.7 TI=300 I=+0.00 (RM) AD250
 DE AD249 4' ITER.

MACH DE REFERENCE= .7300 UINF= 238.255 M/S
 TIV=293.2 K PIV= 1644 MB

	MACH PAROIS						*	MACH PROFIL			*	T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.733	.725	*	PRISES DOUBLES	*	*	1	.061	53	.670	*	1	289.5	
2	.731	.728	*		*	*	2	.192	54	.667	*	2	288.4	
3	.731	.725	*	59	.729	.724	*	3	.304	55	.669	*	3	288.6
4	.730	.726	*	60	.736	.729	*	4	.412	56	.674	*	4	288.6
5	.730	.729	*	61	.733	.725	*	5	.501	57	.679	*	5	288.5
6	.729	.728	*		*	*	6	.557	58	.686	*	6	288.5	
7	.729	.725	*	PRISES LAT. GAUCHE*	*	*	7	.596	59	.694	*	7	288.7	
8	.731	.725	*		*	*	8	.628	60	.703	*	8	289.2	
9	.733	.730	*	62	.730	.729	*	9	.660	61	.715	*	9	290.2
10	.732	.724	*	63	.730	.731	*	10	.695	62	.728	*	10	289.8
11	.732	.729	*	64	.734	.722	*	11	.732	63	.739	*	11	289.3
12	.729	.730	*	65	.738	.709	*	12	.771	64	.752	*	12	289.4
13	.732	.725	*	66	.758	.708	*	13	.866	65	.768	*	13	289.4
14	.730	.725	*	67	.773	.742	*	14	.961	66	.784	*	14	290.0
15	.732	.724	*	68	.771	.750	*	15	1.011	67	.802	*	15	290.1
16	.733	.722	*	69	.766	.735	*	16	1.051	68	.821	*	16	289.1
17	.737	.720	*	70	.760	.715	*	17	1.058	69	.840	*	17	289.8
18	.739	.717	*	71	.740	.715	*	18	1.060	70	.858	*	18	289.0
19	.739	.716	*	72	.734	.723	*	19	1.048	71	.874	*	19	289.2
20	.733	.714	*	73	.735	.733	*	20	1.014	72	.884	*		
21	.736	.711	*		*	*	21	1.009	73	.888	*	I	TPG	
22	.746	.704	*	PRISES LAT. DROITES*	*	*	22	1.012	74	.889	*			
23	.751	.700	*		*	*	23	1.000	75	.885	*	1	293.2	
24	.754	.702	*	74	.730	.728	*	24	.992	76	.879	*	2	293.2
25	.757	.710	*	75	.730	.726	*	25	.987	77	.869	*	3	293.2
26	.761	.716	*	76	.731	.726	*	26	.983	78	.857	*	4	293.1
27	.764	.724	*	77	.730	.724	*	27	.981	79	.843	*	5	293.1
28	.769	.736	*	78	.735	.722	*	28	.981	80	.830	*		
29	.771	.745	*	79	.738	.715	*	29	.983	81	.818	*		
30	.771	.749	*	80	.738	.711	*	30	.983	82	.808	*		
31	.773	.748	*	81	.753	.702	*	31	.982	83	.798	*		
32	.771	.754	*	82	.756	.710	*	32	.984	84	.788	*		
33	.769	.752	*	83	.764	.724	*	33	.984	85	.779	*		
34	.767	.747	*	84	.771	.741	*	34	.985	86	.772	*		
35	.766	.744	*	85	.772	.749	*	35	.985	87	.760	*		
36	.766	.739	*	86	.768	.750	*	36	.985	88	.747	*		
37	.764	.733	*	87	.767	.744	*	37	.978	89	.732	*		
38	.764	.726	*	88	.766	.734	*	38	.969	90	.723	*		
39	.765	.719	*	89	.764	.721	*	39	.952	91	.723	*		
40	.762	.716	*	90	.758	.715	*	40	.930	92	.709	*		
41	.760	.713	*	91	.746	.715	*	41	.907	93	.702	*		
42	.758	.712	*	92	.742	.716	*	42	.879	94	.698	*		
43	.752	.711	*	93	.735	.720	*	43	.852	95	.696	*		
44	.745	.712	*	94	.736	.723	*	44	.822	96	.697	*		
45	.741	.712	*	95	.732	.720	*	45	.792	97	.701	*		
46	.740	.713	*	96	.734	.720	*	46	.765	98	.740	*		
47	.742	.715	*		*	*	47	.741	99	.791	*			
48	.740	.718	*		*	*	48	.721	100	.733	*			
49	.739	.719	*		*	*	49	.705	101	.593	*			
50	.735	.722	*		*	*	50	.693	102	.434	*			
51	.735	.723	*		*	*	51	.683	103	.306	*			
52	.734	.726	*		PRISES COL	*	52	.675						
53	.735	.728	*											
54	.734	.729	*		.800	1.182	*				REFERENCE PROFIL			
55	.734	.727	*		.843	.904	*				.730			
56	.734	.726	*		.902	.843	*				.729			
57	.733	.721	*		.953	.795	*				.730			
58	.731	.708	*		1.123	.757	*				.730			

***** FICHIER AD251 NO(IT)= 4
15/ 3/95 14H20 M=.756 PI=1.7 TI=300 I=+0.00 (RM) AD251
DE AD250 4' ITER.

MACH DE REFERENCE= .7615 UINF= 247.741 M/S
TIV=293.8 K PIV= 1680 MB

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD253 NO(IT)= 4
15/ 3/85 15H45 M=.754 PI=1.7 TI=300 I=-2.00 <RM > AD253
DE AD252 4' ITER.

MACH DE REFERENCE= .7608 UINF= 248.260 M/S
TIV=295.5 K PIV= 1685 MB

***** FICHIER AD254 NO(IT)= 4
15/ 3/85 15H55 M=.726 PI=1.7 TI=300 I=-2.00 (RM) AD254
DE AD253 4' ITER.

MACH DE REFERENCE= .7318 UINF= 240.053 M/S
TIV=296.3 K PIY= 1647 MB

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD255 NO(IT)= 4
15/ 3/84 16H15 M=.694 PI=1.7 TI=300 I=-2.00 (RM) AD255
DE AD254 4' ITER.

MACH DE REFERENCE= .6995 UINF= 230.360 M/S
TIV=296.2 K PIV= 1562 MB

MACH PAROIS						MACH PROFIL						T(K)		
I	HAUT	SAS	I	HAUT	BAS	I	EXT	I	INT	I	TPR			
1	.699	.696	*	PRISES DOUBLES	*	1	.225	.53	.632	*	1	291.2		
2	.697	.699	*		*	2	.050	.54	.635	*	2	292.1		
3	.698	.697	*	59	.697	.696	*	3	.105	.55	.639	*	3	292.2
4	.698	.697	*	60	.702	.700	*	4	.204	.56	.646	*	4	292.0
5	.698	.700	*	61	.702	.695	*	5	.288	.57	.653	*	5	291.9
6	.697	.699	*			*	6	.357	.58	.661	*	6	291.7	
7	.697	.697	*	PRISES LAT. GAUCHE	S*	7	.404	.59	.670	*	7	291.7		
8	.698	.697	*			*	8	.444	.60	.680	*	8	292.0	
9	.699	.702	*	62	.698	.699	*	9	.481	.61	.691	*	9	292.9
10	.699	.695	*	63	.698	.702	*	10	.520	.62	.704	*	10	292.6
11	.698	.698	*	64	.699	.696	*	11	.557	.63	.717	*	11	292.2
12	.695	.698	*	65	.698	.688	*	12	.595	.64	.730	*	12	292.0
13	.698	.695	*	66	.707	.703	*	13	.682	.65	.745	*	13	292.2
14	.696	.696	*	67	.719	.736	*	14	.757	.66	.762	*	14	292.4
15	.697	.697	*	68	.721	.734	*	15	.802	.67	.781	*	15	292.2
16	.697	.695	*	69	.719	.716	*	16	.835	.68	.799	*	16	291.6
17	.700	.694	*	70	.714	.696	*	17	.846	.69	.819	*	17	292.0
18	.703	.690	*	71	.703	.689	*	18	.852	.70	.838	*	18	291.7
19	.698	.690	*	72	.700	.696	*	19	.850	.71	.855	*	19	291.8
20	.699	.691	*	73	.704	.703	*	20	.949	.72	.868	*		
21	.701	.691	*			*	21	.852	.73	.876	*	I	TPG	
22	.701	.689	*	PRISES LAT. DROITES	S*	22	.858	.74	.881	*				
23	.703	.689	*			*	23	.857	.75	.881	*	1	296.2	
24	.705	.696	*	74	.698	.700	*	24	.858	.76	.879	*	2	296.2
25	.707	.706	*	75	.698	.697	*	25	.860	.77	.874	*	3	296.1
26	.709	.714	*	76	.698	.698	*	26	.861	.78	.867	*	4	296.1
27	.712	.724	*	77	.697	.695	*	27	.864	.79	.857	*	5	296.1
28	.716	.734	*	78	.699	.695	*	28	.867	.80	.848	*		
29	.718	.740	*	79	.708	.689	*	29	.871	.81	.841	*		
30	.718	.742	*	80	.699	.690	*	30	.874	.82	.835	*		
31	.721	.739	*	81	.704	.691	*	31	.877	.83	.830	*		
32	.721	.742	*	82	.705	.705	*	32	.881	.84	.825	*		
33	.721	.738	*	83	.711	.722	*	33	.884	.85	.820	*		
34	.720	.731	*	84	.718	.736	*	34	.889	.86	.822	*		
35	.720	.727	*	85	.720	.740	*	35	.892	.87	.818	*		
36	.720	.721	*	86	.719	.735	*	36	.897	.88	.815	*		
37	.718	.715	*	87	.720	.726	*	37	.998	.89	.814	*		
38	.718	.708	*	88	.719	.716	*	38	.997	.90	.809	*		
39	.717	.702	*	89	.716	.703	*	39	.889	.91	.820	*		
40	.714	.699	*	90	.712	.696	*	40	.878	.92	.810	*		
41	.713	.696	*	91	.710	.692	*	41	.862	.93	.801	*		
42	.714	.694	*	92	.704	.690	*	42	.843	.94	.791	*		
43	.711	.691	*	93	.698	.693	*	43	.822	.95	.804	*		
44	.709	.690	*	94	.701	.694	*	44	.797	.96	.797	*		
45	.706	.689	*	95	.702	.693	*	45	.772	.97	1.038	*		
46	.706	.689	*	96	.703	.694	*	46	.745	.98	1.047	*		
47	.705	.690	*			*	47	.721	.99	1.094	*			
48	.702	.691	*			*	48	.697	100	1.089	*			
49	.701	.692	*			*	49	.676	101	.878	*			
50	.698	.693	*			*	50	.659	102	.684	*			
51	.700	.694	*			*	51	.643	103	.546	*			
52	.702	.696	*	PRISES COL	*	52	.630							
53	.705	.697	*											
54	.704	.697	*		.768	1.157	*							
55	.704	.696	*		.813	.891	*							
56	.702	.696	*		.878	.827	*							
57	.702	.693	*		.934	.771	*							
58	.701	.685	*		1.104	.725	*							
								REFERENCE PROFIL						

***** FICHIER AD257 NO(IT)= 4
18/ 3/85 14H45 M=.700 PI=1.7 TI=300 I=+2.00 (RM) AD257
DE AD216 5' ITER.

MACH DE REFERENCE= .7017 UINF= 229.100 M/S
TIY=291.3 K PIV= 1602 MB

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD258 NO(IT)= 4
18/ 3/85 15H15 M=.723 PI=1.7 TI=300 I=+2.00 (RM) AD258
DE AD257 4' ITER.

MACH DE REFERENCE= .7306 UINF= 238.522 M/S
TIV=293.4 K PIY= 1644 MB

***** FICHIER AD260 NO(IT)= 4
13/ 3/85 17H 0 M=.762 PI=1.7 TI=300 I=+2.00 (RM) AD260
DE AD259 4' ITER.

MACH DE REFERENCE= .7656 UINF= 249.028 M/S
TIV=294.0 K PIV= 1685 MB

***** FICHIER AD261 NO(IT)= 4
 18/ 3/85 17H30 M=.747 PI=1.7 TI=300 I=+2.00 (RM) AD261
 DE AD260 4' ITER.

MACH DE REFERENCE= .7522 UINF= 245.374 M/S
 TIV=294.7 K PIV= 1667 MB

I	MACH PAROIS			*	MACH PROFIL			*	T(K)			
	HAUT	BAS	I		HAUT	BAS	I	EXT	I	INT		
* PRISES DOUBLES												
1	.758	.741	*	PRISES DOUBLES	*	*	1	.162	53	.687	*	
2	.758	.746	*		*	*	2	.371	54	.682	*	
3	.756	.744	*	59	.753	.744	*	3	.488	55	.683	*
4	.751	.743	*	60	.759	.747	*	4	.603	56	.686	*
5	.748	.746	*	61	.756	.742	*	5	.697	57	.691	*
6	.750	.747	*				*	6	.744	58	.697	*
7	.753	.746	*	PRISES LAT. GAUCHE	*	*	7	.771	59	.704	*	
8	.753	.742	*		*	*	8	.793	60	.713	*	
9	.754	.746	*	62	.753	.746	*	9	.817	61	.723	*
10	.756	.741	*	63	.752	.748	*	10	.845	62	.736	*
11	.754	.746	*	64	.758	.737	*	11	.878	63	.746	*
12	.748	.745	*	65	.773	.714	*	12	.917	64	.758	*
13	.752	.741	*	66	.805	.702	*	13	1.001	65	.772	*
14	.752	.742	*	67	.829	.732	*	14	1.116	66	.788	*
15	.754	.743	*	68	.830	.750	*	15	1.217	67	.805	*
16	.754	.739	*	69	.818	.745	*	16	1.225	68	.823	*
17	.761	.736	*	70	.795	.728	*	17	1.257	69	.840	*
18	.767	.730	*	71	.770	.730	*	18	1.273	70	.854	*
19	.765	.727	*	72	.759	.742	*	19	1.277	71	.866	*
20	.765	.723	*	73	.746	.753	*	20	1.277	72	.873	*
21	.778	.716	*				*	21	1.278	73	.873	*
22	.784	.705	*	PRISES LAT. DROITES	*	*	22	1.288	74	.871	*	
23	.793	.697	*		*	*	23	1.298	75	.863	*	
24	.800	.697	*	74	.753	.747	*	24	1.290	76	.853	*
25	.806	.704	*	75	.754	.745	*	25	1.291	77	.840	*
26	.813	.707	*	76	.754	.744	*	26	1.294	78	.825	*
27	.820	.714	*	77	.751	.740	*	27	1.297	79	.809	*
28	.827	.725	*	78	.759	.737	*	28	1.299	80	.793	*
29	.830	.734	*	79	.773	.724	*	29	1.305	81	.779	*
30	.831	.741	*	80	.773	.716	*	30	1.309	82	.766	*
31	.835	.742	*	81	.794	.699	*	31	1.310	83	.753	*
32	.833	.750	*	82	.803	.783	*	32	1.315	84	.738	*
33	.832	.751	*	83	.818	.714	*	33	1.305	85	.726	*
34	.827	.749	*	84	.828	.731	*	34	1.100	86	.714	*
35	.823	.747	*	85	.832	.742	*	35	1.021	87	.697	*
36	.821	.745	*	86	.828	.748	*	36	.987	88	.676	*
37	.815	.748	*	87	.823	.748	*	37	.963	89	.652	*
38	.811	.735	*	88	.817	.741	*	38	.943	90	.636	*
39	.807	.730	*	89	.806	.732	*	39	.925	91	.620	*
40	.800	.727	*	90	.793	.726	*	40	.909	92	.609	*
41	.795	.724	*	91	.781	.724	*	41	.890	93	.594	*
42	.794	.723	*	92	.772	.732	*	42	.869	94	.585	*
43	.787	.721	*	93	.761	.738	*	43	.848	95	.572	*
44	.779	.722	*	94	.760	.741	*	44	.827	96	.573	*
45	.775	.722	*	95	.757	.736	*	45	.805	97	.555	*
46	.772	.726	*	96	.745	.736	*	46	.783	98	.553	*
47	.771	.732	*				*	47	.764	99	.550	*
48	.769	.736	*				*	48	.748	100	.486	*
49	.766	.739	*				*	49	.732	101	.369	*
50	.760	.740	*				*	50	.720	102	.229	*
51	.760	.742	*				*	51	.707	103	.107	*
52	.757	.743	*		PRISES COL	*	*	52	.698			
53	.761	.746	*								REFERENCE PROFIL	
54	.761	.749	*		.826	1.204	*				.750	
55	.760	.747	*		.865	.883	*				.749	
56	.755	.744	*		.922	.843	*				.749	
57	.748	.738	*		.969	.912	*				.749	
58	.731	.721	*		1.137	.775	*				.750	

***** FICHIER AD262 NO(IT)= 5
 13/ 3/85 9H48 M=.696 PI=1.7 TI=300 I=+3.00 (RM) AD262
 DE AD137 4' ITER.

MACH DE REFERENCE= .7009 UINF= 229.012 M/S
 TIV=291.7 K PIV= 1656 MB

MACH PAROIS						*	MACH PROFIL			*	T(K)			
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.708	.689	*	PRISES DOUBLES		*	1	.304	53	.532	*	1	287.2	
2	.707	.692	*			*	2	.513	54	.628	*	2	285.0	
3	.705	.692	*	59	.702	.693	*	3	.632	55	.629	*	3	284.6
4	.702	.694	*	60	.710	.696	*	4	.756	56	.532	*	4	285.5
5	.700	.697	*	61	.709	.693	*	5	.858	57	.536	*	5	286.1
6	.700	.696	*			*	6	.899	58	.541	*	6	285.8	
7	.702	.694	*	PRISES LAT. GAUCHE	S	*	7	.909	59	.546	*	7	285.9	
8	.704	.693	*			*	8	.916	60	.654	*	8	286.6	
9	.706	.698	*	62	.703	.696	*	9	.929	61	.663	*	9	288.6
10	.707	.691	*	63	.707	.697	*	10	.949	62	.674	*	10	288.5
11	.706	.695	*	64	.712	.687	*	11	.975	63	.682	*	11	288.2
12	.703	.695	*	65	.726	.665	*	12	1.009	64	.691	*	12	288.3
13	.707	.691	*	66	.756	.645	*	13	1.095	65	.701	*	13	288.5
14	.706	.691	*	67	.773	.663	*	14	1.143	66	.714	*	14	288.8
15	.707	.691	*	68	.770	.679	*	15	1.278	67	.726	*	15	288.4
16	.708	.689	*	69	.759	.679	*	16	1.323	68	.738	*	16	287.0
17	.712	.685	*	70	.743	.674	*	17	1.333	69	.749	*	17	286.2
18	.713	.677	*	71	.720	.682	*	18	1.333	70	.759	*	18	286.8
19	.716	.674	*	72	.712	.693	*	19	1.337	71	.766	*	19	287.1
20	.719	.672	*	73	.701	.701	*	20	1.339	72	.770	*		
21	.729	.666	*			*	21	1.333	73	.768	*	I	TPG	
22	.737	.655	*	PRISES LAT. DROITES	S	*	22	1.333	74	.766	*			
23	.745	.645	*			*	23	1.325	75	.758	*	1	291.6	
24	.750	.641	*	74	.704	.696	*	24	1.323	76	.751	*	2	291.6
25	.755	.644	*	75	.703	.693	*	25	1.317	77	.739	*	3	291.6
26	.760	.645	*	76	.706	.693	*	26	1.308	78	.728	*	4	291.5
27	.765	.648	*	77	.706	.690	*	27	1.101	79	.714	*	5	291.6
28	.770	.656	*	78	.713	.686	*	28	1.002	80	.701	*		
29	.771	.663	*	79	.726	.673	*	29	.964	81	.688	*		
30	.772	.669	*	80	.727	.666	*	30	.939	82	.675	*		
31	.775	.670	*	81	.746	.648	*	31	.924	83	.663	*		
32	.773	.678	*	82	.754	.644	*	32	.919	84	.649	*		
33	.770	.680	*	83	.764	.650	*	33	.918	85	.637	*		
34	.766	.679	*	84	.772	.663	*	34	.920	86	.624	*		
35	.763	.679	*	85	.773	.673	*	35	.921	87	.606	*		
36	.761	.678	*	86	.768	.679	*	36	.923	88	.584	*		
37	.756	.675	*	87	.763	.680	*	37	.920	89	.558	*		
38	.752	.673	*	88	.758	.677	*	38	.914	90	.539	*		
39	.749	.671	*	89	.749	.673	*	39	.903	91	.522	*		
40	.744	.670	*	90	.741	.673	*	40	.888	92	.508	*		
41	.741	.669	*	91	.733	.677	*	41	.868	93	.492	*		
42	.741	.669	*	92	.722	.683	*	42	.846	94	.478	*		
43	.736	.671	*	93	.713	.688	*	43	.824	95	.460	*		
44	.731	.673	*	94	.713	.691	*	44	.798	96	.461	*		
45	.727	.675	*	95	.709	.695	*	45	.772	97	.432	*		
46	.724	.678	*	96	.701	.695	*	46	.746	98	.406	*		
47	.719	.682	*			*	47	.723	99	.376	*			
48	.718	.684	*			*	48	.701	100	.308	*			
49	.716	.687	*			*	49	.682	101	.199	*			
50	.713	.689	*			*	50	.663	102	.084	*			
51	.713	.691	*			*	51	.650	103	.076	*			
52	.710	.694	*	PRISES COL		*	52	.640						
53	.712	.696	*											
54	.712	.697	*											
55	.711	.697	*											
56	.707	.697	*											
57	.702	.695	*											
58	.692	.691	*											

REFERENCE PROFIL

.702.

.701

.701

.702

***** FICHIER AD263 NO(IT)= 4
 19/ 3/85 10H 0 M=.725 PI=1.7 TI=300 I=+3.00 (RM) AD263
 DE AD262 5' ITER.

MACH DE REFERENCE= .7296 UINF= 238.227 M/S
 TIV=293.4 K PIV= 1699 MB

MACH PAROIS						*	MACH PROFIL				*	T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.738	.719	*	PRISES DOUBLES		*	1	.269	.53	.663	*	1	289.8	
2	.739	.723	*			*	2	.479	.54	.658	*	2	286.8	
3	.736	.721	*	59	.732	.722	*	3	.598	.55	.658	*	3	286.1
4	.731	.721	*	60	.738	.725	*	4	.721	.56	.660	*	4	285.8
5	.729	.724	*	61	.735	.721	*	5	.821	.57	.664	*	5	286.4
6	.731	.725	*			*	6	.864	.58	.671	*	6	287.9	
7	.732	.725	*	PRISES LAT. GAUCHE*		*	7	.879	.59	.676	*	7	287.9	
8	.732	.722	*			*	8	.890	.60	.695	*	8	287.9	
9	.732	.725	*	62	.734	.724	*	9	.907	.61	.693	*	9	290.0
10	.734	.720	*	63	.733	.726	*	10	.930	.62	.705	*	10	289.8
11	.733	.723	*	64	.740	.715	*	11	.958	.63	.714	*	11	289.3
12	.729	.721	*	65	.757	.690	*	12	.994	.64	.724	*	12	289.6
13	.734	.718	*	66	.786	.670	*	13	1.082	.65	.735	*	13	289.9
14	.734	.719	*	67	.814	.698	*	14	1.139	.66	.750	*	14	290.2
15	.737	.720	*	68	.811	.714	*	15	1.276	.67	.763	*	15	289.9
16	.737	.718	*	69	.798	.711	*	16	1.318	.68	.778	*	16	287.1
17	.742	.713	*	70	.779	.704	*	17	1.334	.69	.792	*	17	286.6
18	.748	.705	*	71	.750	.708	*	18	1.339	.70	.803	*	18	296.8
19	.746	.701	*	72	.740	.721	*	19	1.345	.71	.812	*	19	287.3
20	.749	.698	*	73	.721	.732	*	20	1.353	.72	.816	*		
21	.760	.691	*			*	21	1.349	.73	.815	*	I	TPG	
22	.768	.680	*	PRISES LAT. DROITES*		*	22	1.351	.74	.812	*			
23	.775	.669	*			*	23	1.350	.75	.803	*	1	293.4	
24	.781	.666	*	74	.734	.724	*	24	1.349	.76	.794	*	2	293.5
25	.787	.669	*	75	.734	.724	*	25	1.349	.77	.782	*	3	293.4
26	.794	.672	*	76	.733	.723	*	26	1.348	.78	.769	*	4	293.4
27	.802	.678	*	77	.733	.717	*	27	1.348	.79	.754	*	5	293.4
28	.811	.689	*	78	.742	.715	*	28	1.353	.80	.739	*		
29	.815	.698	*	79	.754	.699	*	29	1.353	.81	.725	*		
30	.815	.704	*	80	.758	.691	*	30	1.357	.82	.711	*		
31	.818	.705	*	81	.777	.672	*	31	1.303	.83	.698	*		
32	.816	.713	*	82	.785	.669	*	32	1.089	.84	.683	*		
33	.813	.714	*	83	.800	.679	*	33	1.036	.85	.670	*		
34	.807	.711	*	84	.813	.696	*	34	1.007	.86	.657	*		
35	.803	.711	*	85	.816	.707	*	35	.981	.87	.638	*		
36	.800	.709	*	86	.810	.712	*	36	.956	.88	.615	*		
37	.796	.705	*	87	.803	.712	*	37	.936	.89	.588	*		
38	.792	.702	*	88	.798	.707	*	38	.918	.90	.570	*		
39	.789	.699	*	89	.789	.702	*	39	.902	.91	.554	*		
40	.784	.698	*	90	.776	.701	*	40	.886	.92	.539	*		
41	.779	.697	*	91	.760	.705	*	41	.869	.93	.525	*		
42	.777	.697	*	92	.751	.708	*	42	.850	.94	.510	*		
43	.767	.698	*	93	.743	.715	*	43	.831	.95	.494	*		
44	.759	.701	*	94	.742	.721	*	44	.809	.96	.495	*		
45	.754	.702	*	95	.736	.717	*	45	.788	.97	.468	*		
46	.752	.705	*	96	.721	.716	*	46	.766	.98	.448	*		
47	.750	.709	*			*	47	.746	.99	.424	*			
48	.749	.713	*			*	48	.728	100	.355	*			
49	.748	.716	*			*	49	.711	101	.244	*			
50	.743	.719	*			*	50	.696	102	.118	*			
51	.742	.722	*			*	51	.683	103	.066	*			
52	.736	.722	*	PRISES COL		*	52	.673						
53	.740	.725	*											
54	.740	.727	*		.805	1.191	*				REFERENCE PROFIL			
55	.739	.726	*		.848	1.134	*				.730			
56	.732	.724	*		.907	.884	*				.731			
57	.725	.718	*		.956	.834	*				.729			
58	.703	.703	*		1.127	.789	*				.730			

***** FICHIER AD264 NO(IT)= 4
19/ 3/85 10H60 M=.759 PI=1.7 TI=300 I=+3.00 (RM) AD264
DE AD263 4' ITER.

MACH DE REFERENCE= .7665 UINF= 249.154 M/S
TIV=293.7 K PIV= 1741 MB

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD265 NO(IT)= 4
19/3/85 11H15 M=.745 PI=1.7 TI=300 I=+3.00 (RM) AD265
DE AD264 4' ITER.

MACH DE REFERENCE= .7517 UINF= 245.386 M/S
TIV=295.0 K PIV= 1726 MB

***** FICHIER AD267 NO(IT)= 4
19/ 3/85 14H20 M=.725 PI=1.7 TI=300 I=+4.00 (RM) AD267
DE AD266 4' ITER.

MACH DE REFERENCE= .7316 UINF= 239.020 M/S
TIV=293.9 K PIY= 1697 MB

***** FICHIER AD268 NO(IT)= 4
 19/ 3/85 14H55 M=.695 PI=1.7 TI=300 I=-1.00 (RM) AD268
 DE AD249 4' ITER.

MACH DE REFERENCE= .6994 UINF= 229.676 M/S
 TIV=294.5 K PIV= 1588 MB

R	MACH PAROIS						MACH PROFIL				T(K)				
	I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
.8	1	.701	.696	*	PRISES DOUBLES	*	*	1	.125	53	.636	*	1	290.9	
.5	2	.700	.698	*			*	2	.100	54	.636	*	2	290.4	
.9	3	.701	.696	*	59	.698	.696	*	3	.203	55	.640	*	3	290.3
.2	4	.701	.697	*	60	.703	.698	*	4	.307	56	.644	*	4	290.2
.8	5	.700	.699	*	61	.702	.693	*	5	.390	57	.651	*	5	290.1
.0	6	.698	.699	*				*	6	.451	58	.659	*	6	290.0
.2	7	.697	.697	*	PRISES LAT. GAUCHE	S*	*	7	.493	59	.666	*	7	290.0	
.7	8	.698	.696	*			*	8	.530	60	.676	*	8	290.4	
.5	9	.699	.700	*	62	.701	.699	*	9	.564	61	.687	*	9	291.2
.3	10	.699	.693	*	63	.700	.701	*	10	.600	62	.700	*	10	291.0
.4	11	.700	.697	*	64	.700	.696	*	11	.635	63	.711	*	11	290.6
.7	12	.698	.698	*	65	.705	.684	*	12	.673	64	.724	*	12	290.5
.1	13	.701	.695	*	66	.718	.693	*	13	.759	65	.738	*	13	290.7
.9	14	.698	.695	*	67	.726	.717	*	14	.838	66	.754	*	14	291.1
.4	15	.699	.696	*	68	.726	.722	*	15	.877	67	.771	*	15	291.3
.1	16	.698	.694	*	69	.725	.711	*	16	.906	68	.789	*	16	289.9
.3	17	.700	.693	*	70	.722	.691	*	17	.910	69	.807	*	17	290.1
.5	18	.703	.690	*	71	.705	.687	*	18	.911	70	.824	*	18	289.8
G	19	.701	.689	*	72	.704	.695	*	19	.904	71	.838	*	19	289.9
	20	.702	.687	*	73	.703	.702	*	20	.998	72	.849	*		
	21	.714	.685	*				*	21	.897	73	.854	*	I	TPG
	22	.706	.682	*	PRISES LAT. DROITES	S*	22	.898	74	.858	*				
	23	.711	.682	*			*	23	.895	75	.856	*	1	294.5	
	24	.714	.687	*	74	.700	.698	*	24	.894	76	.852	*	2	294.6
	25	.717	.696	*	75	.699	.698	*	25	.892	77	.845	*	3	294.5
	26	.720	.701	*	76	.699	.696	*	26	.892	78	.837	*	4	294.4
	27	.722	.707	*	77	.700	.695	*	27	.892	79	.826	*	5	294.4
	28	.724	.715	*	78	.700	.695	*	28	.895	80	.816	*		
	29	.724	.719	*	79	.709	.688	*	29	.897	81	.808	*		
	30	.724	.722	*	80	.707	.685	*	30	.898	82	.800	*		
	31	.726	.720	*	81	.712	.684	*	31	.899	83	.793	*		
	32	.725	.725	*	82	.717	.696	*	32	.903	84	.786	*		
	33	.724	.724	*	83	.721	.707	*	33	.904	85	.780	*		
	34	.723	.719	*	84	.725	.717	*	34	.906	86	.778	*		
	35	.723	.718	*	85	.726	.722	*	35	.909	87	.771	*		
	36	.724	.714	*	86	.725	.723	*	36	.911	88	.762	*		
	37	.723	.708	*	87	.724	.718	*	37	.911	89	.755	*		
	38	.724	.702	*	88	.724	.709	*	38	.908	90	.747	*		
	39	.725	.697	*	89	.725	.698	*	39	.899	91	.750	*		
	40	.723	.694	*	90	.721	.692	*	40	.882	92	.741	*		
	41	.721	.690	*	91	.713	.689	*	41	.864	93	.734	*		
	42	.721	.688	*	92	.708	.688	*	42	.843	94	.729	*		
	43	.716	.686	*	93	.702	.692	*	43	.821	95	.707	*		
	44	.712	.686	*	94	.704	.694	*	44	.795	96	.736	*		
	45	.707	.685	*	95	.702	.694	*	45	.769	97	.812	*		
	46	.706	.686	*	96	.702	.693	*	46	.742	98	.840	*		
	47	.704	.687	*				*	47	.718	99	.813	*		
	48	.704	.689	*				*	48	.695	100	.874	*		
	49	.704	.691	*				*	49	.676	101	.718	*		
	50	.703	.694	*				*	50	.659	102	.547	*		
	51	.703	.694	*				*	51	.646	103	.417	*		
	52	.703	.695	*	PRISES COL		*	52	.636						
	53	.704	.696	*											
	54	.703	.697	*		.767	1.156	*				REFERENCE PROFIL			
	55	.703	.697	*		.813	.958	*				.700			
	56	.700	.596	*		.878	.348	*				.701			
	57	.700	.693	*		.933	.786	*				.699			
	58	.698	.685	*		1.105	.738	*				.700			

ORIGINAL PAGE IS
OF POOR QUALITY

52

***** FICHIER AD269 NO(IT)= 4
19/ 3/85 15H20 M=.725 PI=1.7 TI=300 I=-1.00 (RM) AD269
DE AD268 4' ITER.

MACH DE REFERENCE= .7312 UINF= 239.567 M/S
TIV=295.6 K PIV= 1630 MB

	MACH PAROIS						*	MACH PROFIL			*	T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.731	.725	*	PRISES DOUBLES	*	*	1	.127	.53	.663	*	1	291.7	
2	.729	.728	*			*	2	.082	.54	.663	*	2	291.2	
3	.730	.727	*	59	.728	.726	*	3	.193	.55	.666	*	3	291.1
4	.730	.729	*	60	.735	.729	*	4	.301	.56	.672	*	4	290.9
5	.730	.733	*	61	.734	.726	*	5	.388	.57	.678	*	5	290.8
6	.729	.731	*			*	6	.453	.58	.686	*	6	290.7	
7	.728	.727	*	PRISES LAT. GAUCHE	S	*	7	.497	.59	.695	*	7	290.7	
8	.731	.726	*			*	8	.534	.60	.705	*	8	291.2	
9	.733	.731	*	62	.729	.730	*	9	.570	.61	.717	*	9	292.1
10	.731	.723	*	63	.729	.729	*	10	.608	.62	.731	*	10	291.8
11	.730	.728	*	64	.732	.725	*	11	.645	.63	.743	*	11	291.4
12	.726	.729	*	65	.733	.713	*	12	.685	.64	.757	*	12	291.2
13	.730	.726	*	66	.748	.722	*	13	.779	.65	.773	*	13	291.5
14	.727	.726	*	67	.764	.759	*	14	.864	.66	.791	*	14	291.9
15	.729	.726	*	68	.766	.763	*	15	.913	.67	.810	*	15	292.1
16	.731	.725	*	69	.762	.744	*	16	.951	.68	.831	*	16	290.6
17	.734	.724	*	70	.752	.720	*	17	.960	.69	.852	*	17	291.0
18	.738	.721	*	71	.740	.717	*	18	.963	.70	.872	*	18	290.7
19	.734	.719	*	72	.732	.726	*	19	.956	.71	.891	*	19	290.7
20	.732	.717	*	73	.739	.733	*	20	.949	.72	.905	*		
21	.743	.715	*			*	21	.949	.73	.912	*	I	TPG	
22	.738	.714	*	PRISES LAT. DROITES	S	*	22	.955	.74	.916	*			
23	.743	.712	*			*	23	.948	.75	.914	*	1	295.6	
24	.744	.715	*	74	.730	.730	*	24	.947	.76	.910	*	2	295.6
25	.747	.725	*	75	.729	.727	*	25	.946	.77	.901	*	3	295.6
26	.751	.732	*	76	.729	.725	*	26	.945	.78	.890	*	4	295.5
27	.755	.742	*	77	.727	.724	*	27	.947	.79	.877	*	5	295.5
28	.760	.754	*	78	.732	.725	*	28	.950	.80	.864	*		
29	.762	.763	*	79	.739	.717	*	29	.951	.81	.854	*		
30	.763	.767	*	80	.735	.714	*	30	.953	.82	.845	*		
31	.765	.765	*	81	.743	.714	*	31	.955	.83	.837	*		
32	.765	.769	*	82	.745	.724	*	32	.961	.84	.828	*		
33	.764	.767	*	83	.754	.741	*	33	.963	.85	.821	*		
34	.763	.759	*	84	.763	.759	*	34	.965	.86	.818	*		
35	.762	.754	*	85	.765	.766	*	35	.969	.87	.810	*		
36	.762	.749	*	86	.764	.764	*	36	.971	.88	.801	*		
37	.759	.741	*	87	.763	.755	*	37	.970	.89	.792	*		
38	.758	.733	*	88	.761	.743	*	38	.964	.90	.783	*		
39	.757	.726	*	89	.756	.727	*	39	.950	.91	.785	*		
40	.754	.723	*	90	.750	.720	*	40	.929	.92	.776	*		
41	.751	.719	*	91	.744	.718	*	41	.905	.93	.768	*		
42	.751	.717	*	92	.742	.718	*	42	.880	.94	.762	*		
43	.747	.715	*	93	.734	.723	*	43	.854	.95	.738	*		
44	.744	.716	*	94	.733	.725	*	44	.825	.96	.752	*		
45	.741	.716	*	95	.733	.726	*	45	.796	.97	.867	*		
46	.741	.717	*	96	.738	.725	*	46	.768	.98	.894	*		
47	.741	.719	*				*	47	.742	.99	.970	*		
48	.740	.721	*				*	48	.719	100	.924	*		
49	.738	.724	*				*	49	.701	101	.751	*		
50	.734	.726	*				*	50	.686	102	.571	*		
51	.734	.726	*				*	51	.674	103	.434	*		
52	.735	.727	*				PRISES COL	*	52	.665				
53	.736	.728	*											
54	.735	.729	*											
55	.736	.729	*											
56	.735	.729	*											
57	.736	.726	*											
58	.736	.717	*											

REFERENCE PROFIL

***** FICHIER RD270 NO(IT)= 4
 19/ 3/85 15H35 M=.758 PI=1.7 TI=300 I=-1.00 CRM) RD270
 DE AD269 4' ITER.

MACH DE REFERENCE= .7652 UINF= 249.959 M/S
 TIV=296.5 K PIV= 1683 MB

MACH PAROIS

MACH PROFIL

T(K)

PR	I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR
1.7	1	.765	.759	*	PRISES DOUBLES	*	*	1	.152	.53	.699	*	1	292.1
1.2	2	.763	.762	*		*	*	2	.088	.54	.698	*	2	291.7
1.1	3	.764	.759	*	59	.761	.759	*	.192	.55	.701	*	3	291.5
0.9	4	.763	.760	*	60	.769	.763	*	.299	.56	.706	*	4	291.3
0.8	5	.763	.764	*	61	.766	.757	*	.388	.57	.714	*	5	291.1
0.7	6	.761	.763	*		*	*	6	.453	.58	.722	*	6	290.9
0.7	7	.760	.761	*	PRISES LAT. GAUCHE	*	*	7	.500	.59	.731	*	7	291.1
1.2	8	.763	.761	*		*	*	8	.539	.60	.742	*	8	291.8
2.1	9	.765	.767	*	62	.763	.762	*	.576	.61	.754	*	9	292.8
1.8	10	.765	.758	*	63	.761	.765	*	.616	.62	.770	*	10	292.4
1.4	11	.765	.760	*	64	.764	.759	*	.655	.63	.784	*	11	291.9
1.2	12	.762	.761	*	65	.766	.746	*	.696	.64	.799	*	12	291.6
1.5	13	.765	.757	*	66	.785	.759	*	.794	.65	.816	*	13	291.9
1.9	14	.761	.758	*	67	.805	.799	*	.888	.66	.836	*	14	292.4
2.1	15	.762	.759	*	68	.803	.809	*	.946	.67	.858	*	15	292.6
3.6	16	.762	.758	*	69	.797	.786	*	.996	.68	.882	*	16	291.1
1.0	17	.765	.757	*	70	.790	.752	*	1.013	.69	.908	*	17	291.5
1.7	18	.769	.753	*	71	.773	.751	*	1.026	.70	.934	*	18	291.2
1.7	19	.765	.752	*	72	.765	.758	*	1.020	.71	.960	*	19	291.3
20	20	.764	.751	*	73	.773	.768	*	1.011	.72	.980	*		
G	21	.774	.748	*		*	*	21	1.013	.73	.992	*	I	TPG
22	22	.771	.743	*	PRISES LAT. DROITES	*	*	22	1.026	.74	.999	*		
1.6	23	.777	.741	*		*	*	23	1.018	.75	.994	*	1	296.5
1.6	24	.780	.748	*	74	.763	.762	*	1.015	.76	.986	*	2	296.5
1.5	25	.785	.762	*	75	.762	.762	*	1.013	.77	.972	*	3	296.5
1.5	26	.791	.772	*	76	.763	.760	*	1.012	.78	.956	*	4	296.4
1.5	27	.796	.782	*	77	.763	.756	*	1.015	.79	.938	*	5	296.4
28	28	.802	.795	*	78	.764	.758	*	1.018	.80	.923	*		
29	29	.804	.804	*	79	.773	.758	*	1.022	.81	.910	*		
30	30	.805	.810	*	80	.769	.748	*	1.029	.82	.899	*		
31	31	.806	.808	*	81	.778	.744	*	1.033	.83	.890	*		
32	32	.804	.815	*	82	.783	.762	*	1.041	.84	.880	*		
33	33	.802	.812	*	83	.793	.779	*	1.045	.85	.871	*		
34	34	.799	.805	*	84	.804	.798	*	1.050	.86	.867	*		
35	35	.797	.801	*	85	.805	.809	*	1.056	.87	.859	*		
36	36	.797	.794	*	86	.800	.809	*	1.064	.88	.848	*		
37	37	.796	.785	*	87	.798	.801	*	1.055	.89	.838	*		
38	38	.795	.773	*	88	.796	.785	*	1.032	.90	.829	*		
39	39	.796	.763	*	89	.795	.764	*	1.006	.91	.833	*		
40	40	.792	.758	*	90	.788	.752	*	1.077	.92	.822	*		
41	41	.789	.752	*	91	.778	.749	*	.948	.93	.812	*		
42	42	.789	.749	*	92	.775	.752	*	.918	.94	.803	*		
43	43	.784	.745	*	93	.766	.757	*	.887	.95	.771	*		
44	44	.778	.745	*	94	.767	.757	*	.854	.96	.802	*		
45	45	.774	.745	*	95	.766	.750	*	.824	.97	.946	*		
46	46	.773	.748	*	96	.773	.750	*	.795	.98	.969	*		
47	47	.774	.752	*		*	*	47	.771	.99	1.048	*		
48	48	.772	.755	*		*	*	48	.751	100	.987	*		
49	49	.770	.757	*		*	*	49	.734	101	.791	*		
50	50	.766	.758	*		*	*	50	.722	102	.600	*		
51	51	.766	.757	*		*	*	51	.712	103	.461	*		
52	52	.767	.758	*	PRISES COL	*	*	52	.703					
53	53	.769	.761	*										
54	54	.769	.764	*		.837	1.205	*			REFERENCE PROFIL			
55	55	.770	.762	*		.876	.882	*			.763			
56	56	.768	.761	*		.929	.846	*			.765			
57	57	.770	.753	*		.975	.815	*			.763			
58	58	.769	.731	*		1.141	.786	*			.764			

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD271 NO(IT)= 5
19/3/85 16H10 M=.724 PI=1.7 TI=300 I=-0.25 (RM) AD271
DE AD250 4' ITER.

MACH DE REFERENCE= .7299 UINF= 239.417 M/S
TIV=296.2 K PIV= 1634 MB

I	MACH PAROIS						MACH PROFIL						T(K)	
	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.733	.724	*	PRISES DOUBLES		*	1	.079	.53	.869	*	1	291.7	
2	.730	.726	*			*	2	.166	.54	.566	*	2	290.9	
3	.730	.724	*	59	.728	.724	*	3	.274	.55	.568	*	3	291.9
4	.730	.726	*	60	.734	.728	*	4	.393	.56	.673	*	4	290.9
5	.729	.729	*	61	.731	.722	*	5	.470	.57	.678	*	5	290.8
6	.728	.728	*			*	6	.528	.58	.687	*	6	290.8	
7	.728	.726	*	PRISES LAT. GAUCHE	S*	*	7	.569	.59	.694	*	7	290.9	
8	.731	.726	*			*	8	.602	.60	.705	*	8	291.5	
9	.733	.731	*	62	.729	.728	*	9	.636	.61	.716	*	9	292.3
10	.731	.723	*	63	.730	.730	*	10	.671	.62	.730	*	10	292.1
11	.730	.726	*	64	.732	.722	*	11	.708	.63	.742	*	11	291.8
12	.727	.727	*	65	.735	.710	*	12	.748	.64	.755	*	12	291.6
13	.730	.723	*	66	.756	.714	*	13	.841	.65	.770	*	13	291.9
14	.727	.723	*	67	.769	.744	*	14	.935	.66	.796	*	14	292.2
15	.728	.724	*	68	.767	.753	*	15	.982	.67	.804	*	15	292.2
16	.729	.722	*	69	.764	.740	*	16	1.020	.68	.824	*	16	290.9
17	.732	.720	*	70	.759	.715	*	17	1.028	.69	.844	*	17	291.2
18	.737	.715	*	71	.737	.716	*	18	1.028	.70	.862	*	18	291.1
19	.734	.714	*	72	.733	.722	*	19	1.011	.71	.878	*	19	291.1
20	.732	.714	*	73	.737	.732	*	20	.995	.72	.889	*		
21	.743	.711	*			*	21	.991	.73	.894	*	I	TPG	
22	.741	.706	*	PRISES LAT. DROITES	S*	*	22	.995	.74	.897	*			
23	.748	.702	*			*	23	.984	.75	.892	*	1	296.1	
24	.751	.707	*	74	.730	.728	*	24	.978	.76	.886	*	2	296.1
25	.755	.716	*	75	.729	.726	*	25	.976	.77	.876	*	3	296.1
26	.759	.722	*	76	.730	.726	*	26	.973	.78	.865	*	4	296.1
27	.763	.729	*	77	.729	.723	*	27	.972	.79	.851	*	5	296.0
28	.766	.739	*	78	.732	.722	*	28	.973	.80	.838	*		
29	.767	.746	*	79	.741	.713	*	29	.973	.81	.827	*		
30	.767	.751	*	80	.738	.711	*	30	.974	.82	.817	*		
31	.768	.750	*	81	.749	.705	*	31	.974	.83	.808	*		
32	.767	.756	*	82	.754	.716	*	32	.975	.84	.797	*		
33	.765	.756	*	83	.761	.729	*	33	.977	.85	.788	*		
34	.763	.751	*	84	.767	.743	*	34	.977	.86	.783	*		
35	.762	.748	*	85	.768	.751	*	35	.979	.87	.773	*		
36	.762	.744	*	86	.765	.753	*	36	.979	.88	.760	*		
37	.761	.737	*	87	.763	.749	*	37	.976	.89	.749	*		
38	.761	.729	*	88	.763	.739	*	38	.966	.90	.738	*		
39	.763	.722	*	89	.763	.723	*	39	.952	.91	.734	*		
40	.760	.718	*	90	.757	.715	*	40	.930	.92	.727	*		
41	.757	.714	*	91	.747	.714	*	41	.906	.93	.720	*		
42	.757	.712	*	92	.739	.716	*	42	.879	.94	.718	*		
43	.752	.710	*	93	.733	.721	*	43	.852	.95	.719	*		
44	.745	.710	*	94	.734	.722	*	44	.822	.96	.720	*		
45	.741	.711	*	95	.731	.721	*	45	.793	.97	.733	*		
46	.739	.713	*	96	.736	.721	*	46	.766	.98	.779	*		
47	.738	.717	*			*	47	.741	.99	.839	*			
48	.737	.719	*			*	48	.721	100	.792	*			
49	.736	.720	*			*	49	.704	101	.635	*			
50	.734	.722	*			*	50	.690	102	.472	*			
51	.734	.721	*			*	51	.681	103	.340	*			
52	.733	.724	*	PRISES COL		*	52	.672						
53	.733	.725	*											
54	.733	.727	*		.799	1.181	*				REFERENCE PROFIL			
55	.733	.727	*		.842	.923	*				.730			
56	.732	.726	*		.901	.850	*				.730			
57	.733	.721	*		.951	.801	*				.730			
58	.733	.709	*		1.122	.761	*				.729			

***** FICHIER AD273 NO(IT)= 4
19/ 3/85 17H20 M=.721 PI=3.3 TI=300 I=-0.25 (RMP) AD273
DE AD272 5' ITER.

MACH DE REFERENCE= .7271 UINF= 239.455 M/S
TIV=298.3 K PIV= 3294 MB

***** FICHIER AD277 NO(IT)= 4
20/ 3/85 16H35 M=.730 PI=1.7 TI=TA I=-0.25 (RM) AD277
DE AD274 4' ITER.

MACH DE REFERENCE= .7358 UINF= 239.629 M/S
TIV=292.4 K PIV= 1638 MB

***** FICHIER AD279 N0(IT)= 4
 20/ 3/85 17H.722 PI=3.3 TI=240 I=-0.25 (RM T) AD279
 DE AD278 R.

MACH FERENCE= .7273 UINF= 214.723 M/S
 TIV=239.8 K PIV= 3292 MB

	ICH PAROIS			*	MACH PROFIL			*	T(K)			
I	HAUT	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR
1	.729	*	PRISES DOUBLES		*	1	.060	.53	.647	*	1	236.2
2	.725	*			*	2	.181	.54	.647	*	2	234.8
3	.726	*	.59	.722	.718	*	.294	.55	.651	*	3	234.9
4	.727	*	.60	.732	.725	*	.402	.56	.657	*	4	235.4
5	.728	*	.61	.731	.720	*	.490	.57	.664	*	5	235.2
6	.729	*			*	6	.543	.58	.672	*	6	235.1
7	.729	*	PRISES LAT. GAUCHE	S	*	7	.584	.59	.681	*	7	235.1
8	.727	*			*	8	.617	.60	.690	*	8	236.2
9	.729	*	.62	.725	.727	*	.648	.61	.702	*	9	237.6
10	.729	*	.63	.731	.728	*	.691	.62	.717	*	10	236.5
11	.728	*	.64	.729	.721	*	.722	.63	.728	*	11	236.1
12	.727	*	.65	.737	.706	*	.762	.64	.740	*	12	236.1
13	.724	*	.66	.752	.709	*	.853	.65	.755	*	13	236.3
14	.720	*	.67	.771	.737	*	.957	.66	.772	*	14	236.4
15	.720	*	.68	.769	.746	*	.994	.67	.790	*	15	236.7
16	.721	*	.69	.762	.731	*	1.034	.68	.809	*	16	236.9
17	.738	*	.70	.756	.710	*	1.046	.69	.828	*	17	235.1
18	.733	*	.71	.737	.710	*	1.042	.70	.845	*	18	235.3
19	.732	*	.72	.730	.719	*	1.019	.71	.861	*	19	237.5
20	.731	*	.73	.734	.731	*	.999	.72	.872	*		
21	.738	*			*	21	.994	.73	.875	*	I	TPG
22	.744	*	PRISES LAT. DROITES	S	22	1.003	.74	.878	*			
23	.749	*			*	23	.986	.75	.873	*	1	240.0
24	.741	*	.74	.725	.726	*	.980	.76	.868	*	2	240.4
25	.759	*	.75	.725	.721	*	.976	.77	.859	*	3	239.6
26	.755	*	.76	.727	.721	*	.972	.78	.848	*	4	239.3
27	.781	*	.77	.724	.719	*	.972	.79	.834	*	5	239.5
28	.762	*	.78	.729	.719	*	.972	.80	.823	*		
29	.789	*	.79	.739	.711	*	.974	.81	.812	*		
30	.784	*	.80	.736	.708	*	.975	.82	.803	*		
31	.782	*	.81	.748	.701	*	.975	.83	.794	*		
32	.768	*	.82	.751	.709	*	.978	.84	.784	*		
33	.787	*	.83	.759	.721	*	.978	.85	.779	*		
34	.782	*	.84	.768	.737	*	.980	.86	.774	*		
35	.789	*	.85	.770	.744	*	.982	.87	.762	*		
36	.785	*	.86	.766	.745	*	.985	.88	.747	*		
37	.729	*	.87	.763	.741	*	.982	.89	.733	*		
38	.722	*	.88	.760	.730	*	.976	.90	.721	*		
39	.745	*	.89	.759	.716	*	.960	.91	.735	*		
40	.713	*	.90	.753	.710	*	.939	.92	.714	*		
41	.708	*	.91	.745	.710	*	.915	.93	.703	*		
42	.706	*	.92	.739	.710	*	.890	.94	.699	*		
43	.705	*	.93	.731	.718	*	.865	.95	.694	*		
44	.706	*	.94	.732	.718	*	.835	.96	.704	*		
45	.707	*	.95	.729	.715	*	.806	.97	.712	*		
46	.708	*	.96	.732	.715	*	.776	.98	.758	*		
47	.711	*			*	47	.747	.99	.812	*		
48	.714	*			*	48	.722	100	.755	*		
49	.719	*			*	49	.699	101	.612	*		
50	.721	*			*	50	.679	102	.451	*		
51	.719	*			*	51	.663	103	.324	*		
52	.723	*	PRISES COL		*	52	.649					
53	.724	*										
54	.727	*		.798	1.176	*			REFERENCE PROFIL			
55	.727	*		.836	1.129	*			.724			
56	.728	*		.897	.886	*			.726			
57	.718	*		.949	.816	*			.723			
58	.701	*		1.126	.766	*			.724			

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD280 NO(IT)= 4
21/3/85 10H 0 M=.724 PI=2.5 TI=TA I=-0.25 (RMP) AD280
DE AD272 5' ITER.

MACH DE REFERENCE = .7297 UINF = 238.256 M/S
TIV = 293.4 K PIV = 2497 MB

***** FICHIER AD282 NO(IT)= 4
 21/3/85 11H45 M=.722 PI=1.7 TI=120K I=-0.25 (RM T) AD282
 DE AD276 4' ITER

MACH DE REFERENCE= .7302 UINF= 152.100 M/S
 TIV=119.4 K PIV= 1595 MB

*	T	MACH PAROIS						*	MACH PROFIL				*	T(K)		
*	I	I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
*	1	1	.731	.723	* PRISES DOUBLES			*	1	.146	53	.652	*	1	116.4	
*	2	2	.730	.729	*			*	2	.184	54	.652	*	2	116.1	
*	3	3	.730	.724	*	59	.728	.723	*	3	.290	55	.656	*	3	115.7
*	4	4	.729	.725	*	60	.734	.729	*	4	.398	56	.662	*	4	116.5
*	5	5	.726	.727	*	61	.731	.723	*	5	.486	57	.668	*	5	115.8
*	6	6	.726	.727	*			*	6	.541	58	.676	*	6	116.0	
*	7	7	.727	.725	* PRISES LAT. GAUCHE	S		*	7	.581	59	.685	*	7	115.9	
*	8	8	.729	.722	*			*	8	.615	60	.695	*	8	116.8	
*	9	9	.729	.728	*	62	.728	.729	*	9	.646	61	.707	*	9	117.4
*	10	10	.730	.722	*	63	.726	.731	*	10	.745	62	.720	*	10	116.6
*	11	11	.728	.729	*	64	.733	.724	*	11	.720	63	.732	*	11	116.1
*	12	12	.724	.729	*	65	.738	.707	*	12	.760	64	.746	*	12	116.4
*	13	13	.730	.723	*	66	.759	.712	*	13	.850	65	.762	*	13	116.5
*	14	14	.730	.722	*	67	.772	.741	*	14	.968	66	.778	*	14	116.6
*	15	15	.729	.724	*	68	.770	.751	*	15	.996	67	.796	*	15	116.2
*	16	16	.730	.722	*	69	.764	.737	*	16	1.040	68	.815	*	16	118.0
*	17	17	.735	.721	*	70	.760	.714	*	17	1.046	69	.834	*	17	116.2
*	18	18	.742	.716	*	71	.740	.713	*	18	1.045	70	.851	*	18	116.2
*	19	19	.734	.714	*	72	.732	.725	*	19	1.025	71	.867	*	19	119.5
*	20	20	.736	.713	*	73	.736	.731	*	20	1.004	72	.878	*		
*	I	21	.737	.710	*			*	21	1.000	73	.882	*	I	TPG	
*	22	.742	.707	* PRISES LAT. DROITES	S			*	22	1.002	74	.884	*			
*	1	23	.746	.701	*			*	23	.992	75	.880	*	1	119.5	
*	2	24	.750	.703	*	74	.727	.729	*	24	.987	76	.875	*	2	119.4
*	3	25	.757	.710	*	75	.731	.725	*	25	.982	77	.866	*	3	118.6
*	4	26	.761	.717	*	76	.728	.724	*	26	.979	78	.854	*	4	119.3
*	5	27	.765	.724	*	77	.726	.721	*	27	.979	79	.841	*	5	118.1
*	28	.768	.735	*	78	.732	.722	*	28	.979	80	.829	*			
*	29	.770	.741	*	79	.740	.714	*	29	.981	81	.818	*			
*	30	.770	.747	*	80	.734	.709	*	30	.982	82	.807	*			
*	31	.773	.745	*	81	.749	.704	*	31	.982	83	.798	*			
*	32	.770	.752	*	82	.758	.710	*	32	.985	84	.788	*			
*	33	.769	.751	*	83	.763	.724	*	33	.987	85	.778	*			
*	34	.765	.746	*	84	.770	.741	*	34	.989	86	.775	*			
*	35	.764	.744	*	85	.772	.747	*	35	.990	87	.763	*			
*	36	.764	.739	*	86	.768	.749	*	36	.993	88	.751	*			
*	37	.762	.733	*	87	.765	.745	*	37	.990	89	.738	*			
*	38	.763	.726	*	88	.763	.735	*	38	.982	90	.724	*			
*	39	.763	.719	*	99	.762	.720	*	39	.965	91	.723	*			
*	40	.759	.717	*	90	.756	.713	*	40	.944	92	.713	*			
*	41	.757	.712	*	91	.747	.712	*	41	.920	93	.702	*			
*	42	.758	.710	*	92	.742	.715	*	42	.894	94	.702	*			
*	43	.753	.708	*	93	.734	.723	*	43	.867	95	.698	*			
*	44	.748	.709	*	94	.735	.723	*	44	.838	96	.703	*			
*	45	.744	.710	*	95	.733	.728	*	45	.808	97	.695	*			
*	46	.742	.712	*	96	.734	.726	*	46	.778	98	.764	*			
*	47	.743	.716	*				*	47	.751	99	.818	*			
*	48	.741	.719	*				*	48	.726	100	.759	*			
*	49	.738	.724	*				*	49	.703	101	.617	*			
*	50	.734	.725	*				*	50	.684	102	.454	*			
*	51	.733	.725	*				*	51	.667	103	.316	*			
*	52	.733	.725	*					52	.654						
*	53	.735	.724	*												
*	54	.735	.726	*												
*	55	.736	.727	*												
*	56	.733	.728	*												
*	57	.734	.725	*												
*	58	.733	.723	*												

REFERENCE PROFIL

.726

.728

.726

.727

ORIGINAL PAGE IS
OF POOR QUALITY

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***** FICHIER AD283 NO(IT)= 4
22/ 3/85 9H25 M=.724 PI=1.7 TI=300K I=-0.25 (RM) AD283
DE AD281 4' ITER

MACH DE REFERENCE= .7265 UINF= 236.728 M/S
TIV=292.0 K PIV= 1621 MB

***** FICHIER AD284 NO(IT)= 4
22/ 3/85 9H50 M=.727 PI=2.9 TI=300K I=-0.25 (RMP) RD284
DE AD280 4' ITER

MACH DE REFERENCE= .7283 UINF= 238.878 M/S
TIV=296.0 K PIV= 2887 MB

***** FICHIER AD285 NO(IT)= 4
 22/ 3/85 11H10 M=.729 PI=2.5 TI=155K I=-0.25 (RMPT) AD285
 DE AD282 4' ITER

MACH DE REFERENCE= .7379 UINF= 174.634 M/S
 TIV=154.5 K PIV= 2484 MB

MACH PAROIS						MACH PROFIL						T(K)		
I	HAUT	BAS	I	HAUT	BAS	I	EXT	I	INT	*	I	TPR		
1	.738	.728	*	PRISES DOUBLES	*	*	.079	.53	.652	*	1	151.3		
2	.735	.733	*	*	*	2	.184	.54	.652	*	2	150.4		
3	.736	.730	*	59	.733	.727	*	3	.299	.53	.656	*	3	150.1
4	.736	.734	*	60	.741	.735	*	4	.404	.56	.662	*	4	151.0
5	.734	.736	*	61	.737	.739	*	5	.495	.57	.669	*	5	150.6
6	.733	.734	*	*	*	*	.546	.58	.677	*	6	150.4		
7	.733	.729	*	PRISES LAT. GAUCHES*	*	7	.587	.59	.686	*	7	150.5		
8	.736	.727	*	*	*	8	.624	.60	.696	*	8	151.4		
9	.738	.735	*	62	.734	.737	*	9	.653	.61	.708	*	9	152.8
10	.739	.728	*	63	.737	.738	*	10	.680	.62	.723	*	10	151.4
11	.736	.737	*	64	.739	.731	*	11	.731	.63	.735	*	11	150.9
12	.733	.738	*	65	.744	.712	*	12	.770	.64	.748	*	12	151.2
13	.738	.731	*	66	.767	.719	*	13	.863	.65	.763	*	13	151.3
14	.736	.729	*	67	.782	.749	*	14	.950	.66	.783	*	14	151.3
15	.735	.730	*	68	.785	.754	*	15	1.011	.67	.801	*	15	151.8
16	.736	.730	*	69	.779	.737	*	16	1.062	.68	.821	*	16	151.8
17	.741	.727	*	70	.766	.720	*	17	1.070	.69	.840	*	17	150.3
18	.748	.722	*	71	.747	.720	*	18	1.073	.70	.857	*	18	150.3
19	.739	.721	*	72	.738	.729	*	19	1.069	.71	.874	*	19	152.7
20	.742	.719	*	73	.745	.740	*	20	1.016	.72	.885	*	20	
21	.745	.716	*	*	*	*	21	1.019	.73	.890	*	I	TPG	
22	.754	.710	*	PRISES LAT. DROITES*	*	22	1.033	.74	.892	*	*	*	*	
23	.760	.706	*	*	*	23	1.013	.75	.887	*	1	154.7		
24	.761	.709	*	74	.734	.736	*	24	1.007	.76	.882	*	2	155.0
25	.766	.718	*	75	.736	.730	*	25	1.002	.77	.873	*	3	154.5
26	.769	.725	*	76	.737	.731	*	26	.997	.78	.861	*	4	153.5
27	.773	.733	*	77	.734	.730	*	27	.997	.79	.847	*	5	153.4
28	.777	.744	*	78	.739	.728	*	28	.998	.80	.835	*	*	
29	.779	.750	*	79	.745	.720	*	29	1.001	.81	.824	*	*	
30	.780	.756	*	80	.743	.715	*	30	1.001	.82	.813	*	*	
31	.785	.753	*	81	.761	.707	*	31	1.002	.83	.804	*	*	
32	.784	.758	*	82	.766	.718	*	32	1.005	.84	.794	*	*	
33	.784	.756	*	83	.773	.732	*	33	1.007	.85	.786	*	*	
34	.782	.749	*	84	.778	.749	*	34	1.009	.86	.784	*	*	
35	.780	.746	*	85	.781	.755	*	35	1.011	.87	.772	*	*	
36	.780	.740	*	86	.781	.753	*	36	1.015	.88	.757	*	*	
37	.777	.734	*	87	.781	.747	*	37	1.011	.89	.741	*	*	
38	.775	.728	*	88	.777	.736	*	38	1.002	.90	.729	*	*	
39	.773	.724	*	89	.773	.725	*	39	.984	.91	.728	*	*	
40	.768	.723	*	90	.763	.720	*	40	.960	.92	.726	*	*	
41	.765	.718	*	91	.754	.719	*	41	.934	.93	.710	*	*	
42	.765	.716	*	92	.748	.721	*	42	.907	.94	.707	*	*	
43	.761	.715	*	93	.741	.726	*	43	.880	.95	.703	*	*	
44	.755	.715	*	94	.740	.728	*	44	.849	.96	.709	*	*	
45	.751	.716	*	95	.738	.732	*	45	.818	.97	.703	*	*	
46	.749	.718	*	96	.742	.731	*	46	.787	.98	.767	*	*	
47	.749	.723	*	*	*	*	47	.758	.99	.820	*	*		
48	.748	.724	*	*	*	*	48	.732	.100	.763	*	*		
49	.744	.727	*	*	*	*	49	.708	.101	.615	*	*		
50	.748	.728	*	*	*	*	50	.686	.102	.451	*	*		
51	.739	.729	*	*	*	*	51	.668	.103	.326	*	*		
52	.739	.734	*	PRISES COL	*	52	.653	*	*	*	*	*		
53	.741	.734	*	*	*	*	*	*	*	*	*	*		
54	.739	.735	*	.802	1.183	*	*	REFERENCE PROFIL	*	*	*	*		
55	.742	.735	*	.848	1.242	*	*	733	*	*	*	*		
56	.740	.736	*	.906	.913	*	*	735	*	*	*	*		
57	.742	.731	*	.956	.837	*	*	732	*	*	*	*		
58	.742	.726	*	1.135	.790	*	*	733	*	*	*	*		

***** FICHIER AD286 NO(IT)= 4
22/ 3/85 16H10 M=.722 PI=3.3 TI=120K I=-0.25 (RMPT) AD286
DE AD276 4' ITER

MACH DE REFERENCE=.7279 UINF= 151.476 M/S
TIV=119.1 K PIYS= 3272 MB

***** FICHIER AD299 NO(IT)= 4
25/ 3/85 15H25 M=.722 PI=2.5 TI=120K I=-0.25 (RMPT) AD299
DE AD282 4' ITER

MACH DE REFERENCE= .7313 UINF= 152.434 M/S
TIV=119.6 K PIV= 2484 MB

***** FICHIER AD292 NO(IT)= 4
25/ 3/85 17H45 M=.754 PI=2.9 TI=300K I=+0.25 (RMP) AD292
DE AD291 S' ITER

MACH DE REFERENCE= .7594 UINF= 248.638 M/S
TIV=297.4 K PIV= 2896 MB

***** FICHIER AD294 NO(IT)= 4
 26/ 3/85 11H50 M=.754 PI=3.3 TI=300K I=+0.25 (RMP) AD294
 DE AD292 4' ITER

MACH DE REFERENCE= .7598 UINF= 248.336 M/S
 TIV=296.4 K PIV= 3290 MB

	MACH PAROIS						*	MACH PROFIL			*	T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.759	.748	*	PRISES DOUBLES		*	1	.039	53	.692	*	1	292.3	
2	.752	.748	*			*	2	.215	54	.680	*	2	290.2	
3	.755	.748	*	59	.751	.743	*	3	.332	55	.682	*	3	289.9
4	.761	.759	*	60	.761	.754	*	4	.443	56	.688	*	4	289.9
5	.762	.763	*	61	.766	.756	*	5	.535	57	.694	*	5	290.4
6	.754	.754	*			*	6	.587	58	.702	*	6	290.2	
7	.751	.745	*	PRISES LAT. GAUCHE*		*	7	.627	59	.710	*	7	290.5	
8	.759	.750	*			*	8	.659	60	.720	*	8	291.4	
9	.763	.761	*	62	.756	.758	*	9	.690	61	.732	*	9	292.7
10	.757	.747	*	63	.760	.756	*	10	.732	62	.740	*	10	292.4
11	.756	.755	*	64	.763	.749	*	11	.765	63	.760	*	11	292.8
12	.755	.761	*	65	.771	.730	*	12	.806	64	.772	*	12	291.7
13	.760	.753	*	66	.793	.734	*	13	.903	65	.789	*	13	292.1
14	.756	.748	*	67	.817	.765	*	14	1.029	66	.808	*	14	292.6
15	.757	.748	*	68	.816	.775	*	15	1.062	67	.827	*	15	292.7
16	.762	.750	*	69	.809	.760	*	16	1.117	68	.848	*	16	291.5
17	.765	.747	*	70	.797	.739	*	17	1.143	69	.869	*	17	290.9
18	.769	.741	*	71	.770	.740	*	18	1.155	70	.889	*	18	291.3
19	.764	.739	*	72	.763	.749	*	19	1.160	71	.906	*	19	291.6
20	.769	.736	*	73	.766	.761	*	20	1.161	72	.918	*		
21	.775	.732	*			*	21	1.162	73	.922	*	I	TPG	
22	.778	.728	*	PRISES LAT. DROITES*		*	22	1.175	74	.923	*			
23	.785	.724	*			*	23	1.165	75	.917	*	1	296.4	
24	.788	.725	*	74	.757	.757	*	24	1.164	76	.909	*	2	296.4
25	.795	.734	*	75	.753	.746	*	25	1.160	77	.897	*	3	296.4
26	.800	.740	*	76	.756	.750	*	26	1.155	78	.883	*	4	296.3
27	.807	.746	*	77	.755	.749	*	27	1.153	79	.867	*	5	296.3
28	.812	.759	*	78	.764	.747	*	28	1.145	80	.853	*		
29	.817	.767	*	79	.770	.737	*	29	1.059	81	.840	*		
30	.816	.774	*	80	.772	.731	*	30	1.000	82	.828	*		
31	.820	.772	*	81	.787	.727	*	31	1.007	83	.816	*		
32	.818	.779	*	82	.794	.733	*	32	1.025	84	.804	*		
33	.817	.778	*	83	.804	.746	*	33	1.040	85	.797	*		
34	.813	.772	*	84	.814	.765	*	34	1.055	86	.789	*		
35	.811	.769	*	85	.817	.774	*	35	1.068	87	.775	*		
36	.810	.764	*	86	.813	.775	*	36	1.081	88	.758	*		
37	.807	.757	*	87	.811	.770	*	37	1.071	89	.749	*		
38	.806	.749	*	88	.808	.759	*	38	1.032	90	.723	*		
39	.806	.743	*	89	.805	.745	*	39	1.008	91	.722	*		
40	.801	.741	*	90	.795	.740	*	40	.980	92	.712	*		
41	.798	.737	*	91	.778	.741	*	41	.950	93	.704	*		
42	.795	.736	*	92	.771	.741	*	42	.921	94	.699	*		
43	.786	.735	*	93	.765	.747	*	43	.891	95	.694	*		
44	.778	.737	*	94	.765	.748	*	44	.858	96	.697	*		
45	.772	.738	*	95	.761	.763	*	45	.828	97	.695	*		
46	.770	.739	*	96	.765	.762	*	46	.797	98	.728	*		
47	.772	.742	*			*	47	.769	99	.777	*			
48	.770	.743	*			*	48	.746	100	.714	*			
49	.769	.747	*			*	49	.727	101	.574	*			
50	.767	.751	*			*	50	.711	102	.412	*			
51	.764	.750	*			*	51	.698	103	.283	*			
52	.767	.759	*			*	52	.687						
53	.765	.756	*											
54	.761	.753	*											
55	.762	.757	*											
56	.762	.760	*											
57	.763	.759	*											
58	.762	.761	*											

PRISES COL

REFERENCE PROFIL

.755

.757

.754

.756

***** FICHIER AD295 NO(IT)= 4
 26/ 3/85 14H35 M=.754 PI=1.7 TI=120K I=+0.25 (RM T) AD295
 DE AD294 4' ITER

MACH DE REFERENCE= .7594 UINF= 157.630 M/S
 TIV=119.5 K PIV= 1645 MB

MACH PAROIS						MACH PROFIL						T(K)	
I	HAUT	BAS	I	HAUT	BAS	I	EXT	I	INT	*	I	TPR	
1	.764	.752	*	PRISES DOUBLES			*	1	.893	53	.676	*	1 116.4
2	.762	.759	*	*	*	*	2	.215	54	.674	*	2 115.9	
3	.762	.753	*	59	.759	.754	3	.333	55	.678	*	3 115.1	
4	.759	.753	*	60	.767	.759	4	.443	56	.684	*	4 115.9	
5	.756	.757	*	61	.760	.751	5	.538	57	.690	*	5 115.5	
6	.757	.758	*	*	*	*	6	.587	58	.699	*	6 115.7	
7	.760	.757	*	PRISES LAT. GAUCHE			*	.628	59	.707	*	7 115.7	
8	.761	.754	*	*	*	*	8	.660	60	.718	*	8 116.5	
9	.761	.759	*	62	.739	.759	9	.690	61	.731	*	9 117.3	
10	.764	.752	*	63	.737	.762	10	.740	62	.740	*	10 116.5	
11	.761	.758	*	64	.762	.752	11	.765	63	.758	*	11 116.0	
12	.756	.757	*	65	.770	.731	12	.806	64	.772	*	12 116.4	
13	.762	.751	*	66	.799	.731	13	.903	65	.798	*	13 116.5	
14	.760	.751	*	67	.815	.765	14	1.046	66	.808	*	14 116.5	
15	.759	.753	*	68	.817	.778	15	1.059	67	.828	*	15 116.1	
16	.759	.752	*	69	.809	.763	16	1.115	68	.849	*	16 117.8	
17	.763	.749	*	70	.793	.739	17	1.141	69	.869	*	17 115.7	
18	.772	.741	*	71	.768	.737	18	1.153	70	.889	*	18 116.1	
19	.764	.738	*	72	.763	.751	19	1.156	71	.906	*	19 119.2	
20	.767	.739	*	73	.762	.761	20	1.156	72	.918	*		
21	.769	.734	*	*	*	*	21	1.157	73	.922	*	I TPG	
22	.778	.725	*	PRISES LAT. DROITES			22	1.170	74	.924	*		
23	.785	.718	*	*	*	*	23	1.164	75	.917	*	1 119.5	
24	.790	.720	*	74	.759	.759	24	1.163	76	.909	*	2 119.4	
25	.797	.729	*	75	.763	.757	25	1.181	77	.896	*	3 119.2	
26	.802	.737	*	76	.762	.756	26	1.158	78	.883	*	4 118.9	
27	.807	.745	*	77	.758	.750	27	1.156	79	.866	*	5 118.2	
28	.812	.758	*	78	.761	.750	28	1.153	80	.851	*		
29	.815	.768	*	79	.761	.737	29	1.148	81	.837	*		
30	.815	.774	*	80	.770	.737	30	1.069	82	.825	*		
31	.822	.775	*	81	.787	.721	31	.993	83	.814	*		
32	.818	.792	*	82	.797	.729	32	1.005	84	.802	*		
33	.820	.781	*	83	.806	.745	33	1.022	85	.789	*		
34	.815	.774	*	84	.812	.765	34	1.042	86	.784	*		
35	.812	.771	*	85	.815	.774	35	1.060	87	.770	*		
36	.811	.787	*	86	.814	.775	36	1.079	88	.754	*		
37	.807	.759	*	87	.812	.772	37	1.090	89	.734	*		
38	.804	.751	*	88	.807	.761	38	1.058	90	.720	*		
39	.801	.744	*	89	.801	.745	39	1.009	91	.715	*		
40	.795	.741	*	90	.730	.738	40	.983	92	.711	*		
41	.792	.736	*	91	.772	.737	41	.954	93	.694	*		
42	.791	.734	*	92	.770	.740	42	.924	94	.689	*		
43	.786	.732	*	93	.763	.747	43	.894	95	.685	*		
44	.778	.733	*	94	.765	.750	44	.862	96	.696	*		
45	.773	.734	*	95	.761	.757	45	.831	97	.698	*		
46	.771	.736	*	96	.761	.756	46	.800	98	.724	*		
47	.770	.741	*	*	*	*	47	.772	99	.776	*		
48	.770	.743	*	*	*	*	48	.747	100	.711	*		
49	.767	.748	*	*	*	*	49	.725	101	.589	*		
50	.784	.750	*	*	*	*	50	.787	102	.498	*		
51	.784	.752	*	*	*	*	51	.692	103	.277	*		
52	.762	.754	*	*	*	*	52	.679	*	*	*		
53	.764	.754	*	*	*	*	*	*	*	*	*		
54	.763	.755	*	*	825	1.200	*	*	*	*	*		
55	.765	.756	*	*	888	.879	*	*	*	758	*		
56	.761	.756	*	*	922	.837	*	*	*	758	*		
57	.760	.754	*	*	968	.804	*	*	*	757	*		
58	.758	.754	*	*	1.144	.759	*	*	*	758	*		
PRISES COL										REFERENCE PROFIL			

***** FICHIER AD296 NO(IT)= 4
26/ 3/85 17H20 M=.753 PI=3.0 TI=120K I=+9.25 (RMPT) AD296
DE AD295 4' ITER

MACH DE REFERENCE= .7603 UINF= 157.390 M/S
TIV=119.7 K PIV= 2982 MB

***** FICHIER AD297 NO(IT)= 4
27/ 3/85 9H30 M=.755 PI=1.7 TI=TROK I=+0.25 (RM) AD297
DE AD293 4' ITER

MACH DE REFERENCE= .7567 UINF= 245.643 M/S
TIY=292.2 K PIY= 1674 MB

***** FICHIER AD298 NO(IT)= 4
27/ 3/85 10H 5 M=.755 PI=2.0 TI=155K I=+0.25 (RMPT) AD298
DE AD297 4' ITER

MACH DE REFERENCE= .7595 UINF= 179.120 M/S
TIV=154.3 K PIV= 1991 MB

***** FICHIER AD299 NO(IT)= 4
27/ 3/85 12H15 M=.754 PI=3 TI=155K I=+0.25 (RMPT) AD299
DE AD298 4ITER

MACH DE REFERENCE= .7589 UINF= 179.190 M/S
TIV=154.7 K PIY= 2983 MB

ORIGINAL PAGE IS
OF POOR QUALITY

72

FICHIER AD303 NO(IT)= 4
28/ 3/85 15H45 M=.757 PI=1.7 TI=TA I=+1.00 (RM) AD303
DE RD246 4ITER

MACH DE REFERENCE= .7608 UINF= 247.857 M/S
TIV=294.6 K PIV= 1689 MB

I	MACH PAROIS						MACH PROFIL						T(K)	
	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
* PRISES DOUBLES														
1	.765	.751	*			*	1	.072	53	.696	*	1	289.7	
2	.763	.755	*			*	2	.276	54	.691	*	2	288.3	
3	.763	.753	*	59	.760	.753	*	3	.393	55	.692	*	3	287.7
4	.761	.753	*	60	.765	.757	*	4	.505	56	.696	*	4	287.5
5	.759	.756	*	61	.763	.752	*	5	.597	57	.702	*	5	287.5
6	.759	.756	*			*	6	.649	58	.708	*	6	288.4	
7	.760	.754	*			*	7	.684	59	.716	*	7	288.6	
8	.761	.754	*			*	8	.712	60	.725	*	8	289.2	
9	.761	.758	*	62	.761	.756	*	9	.741	61	.736	*	9	290.5
10	.762	.751	*	63	.758	.759	*	10	.775	62	.749	*	10	290.2
11	.761	.754	*	64	.765	.749	*	11	.810	63	.763	*	11	289.9
12	.757	.754	*	65	.775	.729	*	12	.851	64	.775	*	12	289.8
13	.761	.750	*	66	.805	.722	*	13	.947	65	.790	*	13	290.1
14	.759	.751	*	67	.829	.756	*	14	1.020	66	.808	*	14	290.4
15	.761	.752	*	68	.827	.770	*	15	1.083	67	.827	*	15	290.3
16	.761	.751	*	69	.816	.759	*	16	1.155	68	.847	*	16	287.7
17	.766	.747	*	70	.803	.741	*	17	1.187	69	.866	*	17	287.9
18	.773	.739	*	71	.772	.738	*	18	1.204	70	.884	*	18	287.7
19	.769	.737	*	72	.767	.753	*	19	1.215	71	.901	*	19	287.3
20	.771	.736	*	73	.760	.761	*	20	1.220	72	.911	*		TPG
21	.776	.732	*			*	21	1.221	73	.913	*	I	TPG	
22	.783	.723	*			*	22	1.232	74	.912	*		1	294.7
23	.792	.716	*			*	23	1.228	75	.904	*		2	294.7
24	.798	.716	*	74	.762	.756	*	24	1.230	76	.895	*	3	294.7
25	.805	.723	*	75	.761	.754	*	25	1.230	77	.881	*	4	294.6
26	.812	.729	*	76	.761	.754	*	26	1.230	78	.866	*	5	294.6
27	.818	.736	*	77	.759	.749	*	27	1.230	79	.850	*		
28	.826	.749	*	78	.765	.748	*	28	1.231	80	.834	*		
29	.829	.758	*	79	.775	.735	*	29	1.232	81	.820	*		
30	.829	.765	*	80	.775	.731	*	30	1.237	82	.808	*		
31	.832	.765	*	81	.794	.719	*	31	1.240	83	.795	*		
32	.830	.772	*	82	.802	.723	*	32	1.248	84	.791	*		
33	.830	.772	*	83	.816	.736	*	33	1.232	85	.769	*		
34	.823	.768	*	84	.828	.755	*	34	1.057	86	.760	*		
35	.819	.765	*	85	.830	.766	*	35	.992	87	.745	*		
36	.818	.761	*	86	.824	.769	*	36	.977	88	.728	*		
37	.814	.754	*	87	.819	.765	*	37	.973	89	.708	*		
38	.813	.749	*	88	.816	.756	*	38	.969	90	.693	*		
39	.813	.743	*	89	.812	.745	*	39	.959	91	.683	*		
40	.807	.741	*	90	.801	.740	*	40	.942	92	.672	*		
41	.803	.737	*	91	.785	.740	*	41	.929	93	.662	*		
42	.801	.736	*	92	.774	.740	*	42	.895	94	.654	*		
43	.793	.736	*	93	.767	.748	*	43	.869	95	.646	*		
44	.784	.737	*	94	.769	.752	*	44	.841	96	.648	*		
45	.779	.737	*	95	.763	.764	*	45	.814	97	.639	*		
46	.775	.738	*	96	.760	.764	*	46	.789	98	.655	*		
47	.774	.740	*			*	47	.768	99	.680	*			
48	.771	.743	*			*	48	.750	100	.618	*			
49	.771	.748	*			*	49	.735	101	.487	*			
50	.768	.752	*			*	50	.724	102	.338	*			
51	.768	.753	*			*	51	.714	103	.209	*			
52	.764	.753	*			*	52	.705						
53	.766	.754	*			*								
54	.765	.756	*			*								
55	.765	.757	*			*								
56	.762	.757	*			*								
57	.759	.759	*			*								
58	.751	.764	*			*								

PRISES COL REFERENCE PROFIL

.825 1.202 * .759
.867 .874 * .760
.922 .938 * .758
.968 .907 * .759
1.138 .775 *

***** FICHIER AD304 NO(IT)= 4
 28/ 3/85 16H20 M=.696 PI=2.9 TI=TR I=+1.00 (RMP) AD304
 DE AD302 5' ITER

MACH DE REFERENCE= .6987 UINF= 230.508 M/S
 TIV=297.2 K PIV= 2888 MB

	MACH PAROIS						*	MACH PROFIL			*	T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.701	.690	*	PRISES DOUBLES		*	1	.114	53	.632	*	1	293.9	
2	.695	.689	*			*	2	.319	54	.629	*	2	291.8	
3	.697	.688	*	59	.693	.686	*	3	.432	55	.631	*	3	292.4
4	.701	.696	*	60	.702	.695	*	4	.543	56	.635	*	4	292.4
5	.702	.700	*	61	.704	.694	*	5	.633	57	.640	*	5	292.4
6	.696	.693	*			*	6	.677	58	.647	*	6	292.5	
7	.693	.688	*	PRISES LAT. GAUCHE*		*	7	.707	59	.653	*	7	292.7	
8	.700	.693	*			*	8	.731	60	.661	*	8	293.2	
9	.704	.702	*	62	.698	.696	*	9	.756	61	.671	*	9	294.4
10	.699	.689	*	63	.704	.696	*	10	.789	62	.682	*	10	294.3
11	.698	.693	*	64	.705	.692	*	11	.820	63	.693	*	11	293.9
12	.697	.697	*	65	.714	.671	*	12	.857	64	.703	*	12	293.8
13	.702	.690	*	66	.732	.666	*	13	.944	65	.716	*	13	294.1
14	.699	.688	*	67	.746	.690	*	14	1.010	66	.730	*	14	294.6
15	.700	.690	*	68	.745	.698	*	15	1.091	67	.745	*	15	294.9
16	.704	.693	*	69	.739	.690	*	16	1.124	68	.760	*	16	292.3
17	.706	.690	*	70	.729	.678	*	17	1.137	69	.775	*	17	292.9
18	.709	.683	*	71	.713	.681	*	18	1.128	70	.787	*	18	292.3
19	.706	.680	*	72	.701	.690	*	19	1.045	71	.798	*	19	292.2
20	.712	.676	*	73	.703	.697	*	20	.999	72	.805	*		TPG
21	.716	.673	*			*	21	.994	73	.806	*	I		
22	.719	.670	*	PRISES LAT. DROITES*		*	22	.996	74	.806	*			
23	.723	.664	*			*	23	.978	75	.800	*	1	297.3	
24	.726	.662	*	74	.699	.695	*	24	.969	76	.794	*	2	297.3
25	.731	.666	*	75	.694	.688	*	25	.961	77	.785	*	3	297.3
26	.734	.669	*	76	.698	.692	*	26	.955	78	.775	*	4	297.2
27	.738	.674	*	77	.698	.687	*	27	.952	79	.762	*	5	297.2
28	.743	.684	*	78	.705	.691	*	28	.950	80	.750	*		
29	.746	.691	*	79	.711	.679	*	29	.949	81	.739	*		
30	.745	.696	*	80	.715	.672	*	30	.946	82	.729	*		
31	.747	.695	*	81	.724	.667	*	31	.943	83	.719	*		
32	.745	.700	*	82	.731	.665	*	32	.943	84	.707	*		
33	.748	.700	*	83	.737	.674	*	33	.941	85	.700	*		
34	.741	.696	*	84	.744	.690	*	34	.940	86	.691	*		
35	.740	.695	*	85	.746	.698	*	35	.939	87	.677	*		
36	.740	.692	*	86	.743	.698	*	36	.938	88	.660	*		
37	.737	.688	*	87	.741	.696	*	37	.933	89	.640	*		
38	.736	.683	*	88	.739	.689	*	38	.925	90	.622	*		
39	.736	.680	*	89	.736	.681	*	39	.912	91	.616	*		
40	.732	.679	*	90	.728	.679	*	40	.893	92	.605	*		
41	.729	.677	*	91	.716	.681	*	41	.871	93	.595	*		
42	.728	.676	*	92	.715	.682	*	42	.848	94	.587	*		
43	.721	.675	*	93	.706	.688	*	43	.824	95	.577	*		
44	.716	.677	*	94	.703	.689	*	44	.797	96	.579	*		
45	.713	.678	*	95	.700	.706	*	45	.770	97	.566	*		
46	.712	.680	*	96	.703	.704	*	46	.742	98	.570	*		
47	.715	.683	*			*	47	.716	99	.583	*			
48	.712	.684	*			*	48	.694	100	.525	*			
49	.709	.688	*			*	49	.675	101	.487	*			
50	.705	.692	*			*	50	.660	102	.368	*			
51	.701	.690	*			*	51	.648	103	.145	*			
52	.705	.696	*	PRISES COL		*	52	.638						
53	.704	.693	*											
54	.701	.692	*			*								
55	.702	.696	*			*								
56	.703	.700	*			*								
57	.703	.701	*			*								
58	.700	.710	*			*								

REFERENCE PROFIL

.696

.699

.696

.697

**ORIGINAL PAGE IS
OF POOR QUALITY**

***** FICHIER AD305 N0(IT)= 4
28/ 3/85 16H55 M=.755 PI=2.9 TI=TR I=+1.00 (RMP) AD305
DE AD303 4'ITER

MACH DE REFERENCE= .7587 UINF= 248.382 M/S
TIV=297.3 K PIV= 2883 MB

***** FICHIER AD306 NO(IT)= 4
29/ 3/85 9H40 M=.758 PI=2.4 TI=TA I=+1.00 (RMP) AD306
DE AD305 4'ITER

MACH DE REFERENCE= .7645 UINF= 248.919 M/S
TIV=294.5 K PIY= 2402 MB

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD307 NO<IT>= 4
29/ 3/85 10H35 M=.696 PI=2.4 TI=TA I=+1.00 <RMP > AD307
DE AD304 4'ITER

MACH DE REFERENCE= .7020 UINF= 230.883 M/S
TIV=295.6 K PIV= 2398 MB

***** FICHIER AD308 N8(IT)= 4
 29/ 3/85 11H20 M=.694 PI=2. TI=155K I=+1.00 (RMP) AD308
 DE AD304 4'ITER

MACH DE REFERENCE= .7012 UINF= 166.615 M/S
 TIV=154.3 K PIV= 1995 MB

	MACH PAROIS						*	MACH PROFIL			*	T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.704	.692	*	PRISES DOUBLES		*	1	.119	53	.627	*	1	151.1	
2	.703	.696	*			*	2	.321	54	.625	*	2	150.0	
3	.702	.692	*	59	.700	.692	*	3	.440	55	.627	*	3	150.2
4	.702	.694	*	60	.705	.700	*	4	.551	56	.632	*	4	151.2
5	.700	.697	*	61	.704	.695	*	5	.641	57	.637	*	5	150.3
6	.699	.696	*			*	6	.680	58	.645	*	6	150.8	
7	.700	.695	*	PRISES LAT. GAUCHE*		*	7	.709	59	.651	*	7	150.8	
8	.701	.694	*			*	8	.735	60	.660	*	8	151.7	
9	.702	.701	*	62	.701	.698	*	9	.758	61	.670	*	9	152.6
10	.703	.694	*	63	.703	.702	*	10	.797	62	.681	*	10	151.6
11	.700	.700	*	64	.707	.692	*	11	.823	63	.693	*	11	151.3
12	.698	.700	*	65	.716	.674	*	12	.860	64	.703	*	12	151.5
13	.704	.694	*	66	.738	.668	*	13	.945	65	.716	*	13	151.7
14	.703	.692	*	67	.749	.691	*	14	1.010	66	.730	*	14	151.7
15	.703	.693	*	68	.747	.700	*	15	1.081	67	.745	*	15	151.4
16	.705	.692	*	69	.741	.691	*	16	1.133	68	.761	*	16	152.6
17	.708	.689	*	70	.735	.680	*	17	1.145	69	.775	*	17	150.5
18	.715	.683	*	71	.713	.693	*	18	1.146	70	.788	*	18	150.6
19	.709	.681	*	72	.705	.693	*	19	1.135	71	.799	*	19	154.1
20	.713	.680	*	73	.705	.702	*	20	1.003	72	.805	*		
21	.714	.678	*			*	21	.985	73	.807	*	I	TPG	
22	.722	.672	*	PRISES LAT. DROITES*		*	22	.997	74	.806	*			
23	.728	.665	*			*	23	.982	75	.800	*	1	154.2	
24	.731	.663	*	74	.701	.697	*	24	.976	76	.795	*	2	154.4
25	.737	.666	*	75	.702	.695	*	25	.968	77	.786	*	3	153.7
26	.740	.670	*	76	.701	.696	*	26	.961	78	.775	*	4	153.4
27	.743	.675	*	77	.700	.692	*	27	.959	79	.762	*	5	153.3
28	.746	.685	*	78	.706	.690	*	28	.957	80	.750	*		
29	.747	.692	*	79	.713	.679	*	29	.956	81	.739	*		
30	.746	.696	*	80	.713	.677	*	30	.954	82	.728	*		
31	.749	.696	*	81	.729	.667	*	31	.951	83	.718	*		
32	.747	.702	*	82	.738	.666	*	32	.953	84	.707	*		
33	.749	.700	*	83	.742	.676	*	33	.951	85	.697	*		
34	.742	.697	*	84	.746	.692	*	34	.950	86	.692	*		
35	.740	.696	*	85	.747	.699	*	35	.949	87	.677	*		
36	.741	.694	*	86	.744	.699	*	36	.949	88	.659	*		
37	.739	.689	*	87	.742	.698	*	37	.945	89	.639	*		
38	.739	.686	*	88	.740	.691	*	38	.936	90	.621	*		
39	.739	.683	*	89	.739	.683	*	39	.923	91	.617	*		
40	.735	.682	*	90	.732	.680	*	40	.904	92	.606	*		
41	.733	.679	*	91	.723	.680	*	41	.882	93	.595	*		
42	.733	.678	*	92	.715	.684	*	42	.859	94	.587	*		
43	.729	.677	*	93	.707	.689	*	43	.835	95	.577	*		
44	.723	.677	*	94	.707	.692	*	44	.807	96	.578	*		
45	.719	.678	*	95	.703	.701	*	45	.779	97	.588	*		
46	.716	.680	*	96	.704	.701	*	46	.750	98	.569	*		
47	.715	.685	*			*	47	.723	99	.582	*			
48	.714	.687	*			*	48	.699	100	.525	*			
49	.711	.690	*			*	49	.577	101	.410	*			
50	.707	.692	*			*	50	.558	102	.269	*			
51	.706	.694	*			*	51	.643	103	.148	*			
52	.705	.698	*	PRISES COL		*	52	.630		REFERENCE PROFIL				
53	.706	.697	*											
54	.705	.697	*		.760	1.153	*							
55	.706	.699	*		.811	.864	*							
56	.704	.700	*		.876	.811	*							
57	.703	.699	*		.931	.758	*							
58	.701	.703	*		1.110	.711	*							

***** FICHIER AD309 NO(IT)= 4
29/ 3/85 12H 3 M=.754 PI=2. TI=155K I=+1.00 (RMPT) AD309
DE AD308 4'ITER

MACH DE REFERENCE= .7603 UINF= 179.440 M/S
TIV=154.6 K PIV= 2002 MB

***** FICHIER AD310 NO(IT)= 4
29/ 3/85 14H60 M=.694 PI=2.5 TI=120K I=+1.00 (RMPT) AD310
DE AD308 4'ITER

MACH DE REFERENCE= .7033 UINF= 147.108 M/S
TIV=119.6 K PIV= 2496 MB

**ORIGINAL PAGE IS
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***** FICHIER AD311 NO(IT)= 4
29/ 3/85 15H45 M=.754 PI=2.5 TI=120K I=+1.00 (RMPT) AD311
DE AD309 4'ITER

MACH DE REFERENCE = .7638 UINF = 158.408 M/S
TIW=119.5 K PIV = 2496 MB

***** FICHIER AD312 NO(IT)= 5
1/ 4/85 14H40 M=.754 PI=1.7 TI=TA I=-2.00 (RM) AD312
DE AD253 4'ITER

MACH DE REFERENCE= .7625 VINF= 248.437 M/S
TIV=294.8 K PIV= 1689 MB

**ORIGINAL PAGE IS
OF POOR QUALITY**

***** FICHIER AD313 NO(IT)= 4
1/ 4/85 15H15 M=.761 PI=2.9 TI=TA I=-2.00 (RM) AD313
DE AD312 4'ITER

MACH DE REFERENCE= .7645 UINF= 250.200 M/S
TIV=297.6 K PIV= 2978 MB

***** FICHIER AD314 NO(IT)= 4
1/ 4/85 16H15 M=.762 PI=2.0 TI=155 I=-2.00 (RMPT) AD314
DE AD313 4'ITER

MACH DE REFERENCE= .7715 UINF= 182.836 M/S
TIV=156.3 K PIV= 1966 MB

***** FICHIER AD315 NO(IT)= 4
1/ 4/85 17H15 M=.757 PI=2.5 TI=120K I=-2.00 (RMPT) AD315
DE AD314 4'ITER

MACH DE REFERENCE= .7646 UINF= 158.809 M/S
TIV=113.9 K PIV= 2473 MB

***** FICHIER AD316 NO(IT)= 4
2/ 4/85 9H30 M=.761 PI=2.5 TI=300K I=+2.00 (RM) AD316
DE AD260 4'ITER

MACH DE REFERENCE= .7696 UINF= 250.489 M/S
TIV=294.7 K PIV= 2490 MB

MACH PAROIS						MACH PROFIL						T(K)	
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR
1	.773	.756	* PRISES DOUBLES			*	1	.126	53	.737	*	1	290.7
2	.773	.763	*			*	2	.343	54	.722	*	2	288.3
3	.773	.761	* 59	.767	.758	*	3	.463	55	.719	*	3	287.8
4	.769	.762	* 60	.774	.762	*	4	.577	56	.719	*	4	287.3
5	.765	.764	* 61	.773	.758	*	5	.672	57	.722	*	5	287.3
6	.766	.763	*			*	6	.729	58	.728	*	6	288.2
7	.767	.759	* PRISES LAT. GAUCHE			*	7	.750	59	.731	*	7	289.7
8	.768	.757	*			*	8	.774	60	.740	*	8	289.9
9	.768	.763	* 62	.770	.765	*	9	.800	61	.750	*	9	291.4
10	.770	.755	* 63	.770	.765	*	10	.832	62	.762	*	10	291.0
11	.768	.762	* 64	.773	.755	*	11	.864	63	.774	*	11	290.6
12	.763	.762	* 65	.798	.729	*	12	.903	64	.787	*	12	290.5
13	.769	.757	* 66	.821	.722	*	13	.992	65	.802	*	13	290.9
14	.767	.758	* 67	.854	.754	*	14	1.117	66	.816	*	14	291.5
15	.768	.758	* 68	.855	.773	*	15	1.205	67	.834	*	15	291.8
16	.768	.756	* 69	.838	.766	*	16	1.220	68	.853	*	16	289.7
17	.773	.752	* 70	.814	.748	*	17	1.253	69	.871	*	17	288.9
18	.782	.745	* 71	.786	.746	*	18	1.271	70	.888	*	18	289.4
19	.779	.741	* 72	.775	.760	*	19	1.274	71	.902	*	19	289.7
20	.783	.737	* 73	.758	.773	*	20	1.275	72	.911	*		TPG
21	.788	.731	*			*	21	1.276	73	.911	*	I	TPG
22	.798	.722	* PRISES LAT. DROITES			*	22	1.294	74	.908	*		
23	.807	.715	*			*	23	1.298	75	.898	*	1	294.7
24	.812	.715	* 74	.770	.764	*	24	1.295	76	.887	*	2	294.7
25	.821	.723	* 75	.769	.761	*	25	1.298	77	.872	*	3	294.8
26	.829	.728	* 76	.769	.759	*	26	1.300	78	.856	*	4	294.7
27	.842	.734	* 77	.766	.755	*	27	1.306	79	.838	*	5	294.7
28	.849	.746	* 78	.772	.753	*	28	1.310	80	.821	*		
29	.855	.756	* 79	.779	.740	*	29	1.317	81	.806	*		
30	.856	.763	* 80	.789	.731	*	30	1.321	82	.791	*		
31	.861	.764	* 81	.809	.717	*	31	1.323	83	.776	*		
32	.859	.774	* 82	.820	.723	*	32	1.329	84	.762	*		
33	.861	.775	* 83	.840	.734	*	33	1.273	85	.751	*		
34	.850	.772	* 84	.855	.754	*	34	1.097	86	.739	*		
35	.844	.771	* 85	.858	.766	*	35	1.031	87	.721	*		
36	.840	.769	* 86	.854	.772	*	36	1.004	88	.699	*		
37	.834	.764	* 87	.844	.771	*	37	.984	89	.675	*		
38	.829	.759	* 88	.836	.764	*	38	.965	90	.655	*		
39	.826	.754	* 89	.825	.753	*	39	.946	91	.645	*		
40	.818	.752	* 90	.813	.747	*	40	.926	92	.633	*		
41	.813	.748	* 91	.797	.745	*	41	.908	93	.619	*		
42	.811	.746	* 92	.789	.747	*	42	.889	94	.609	*		
43	.804	.742	* 93	.778	.756	*	43	.873	95	.598	*		
44	.796	.741	* 94	.778	.759	*	44	.858	96	.599	*		
45	.792	.741	* 95	.776	.752	*	45	.844	97	.584	*		
46	.789	.743	* 96	.760	.753	*	46	.829	98	.584	*		
47	.788	.747	*			*	47	.817	99	.592	*		
48	.785	.751	*			*	48	.807	100	.530	*		
49	.782	.756	*			*	49	.796	101	.405	*		
50	.777	.758	*			*	50	.784	102	.259	*		
51	.776	.759	*			*	51	.774	103	.130	*		
52	.774	.751	*	PRISES COL		*	52	.759					
53	.779	.764	*										
54	.780	.768	*	.840	1.211	*							
55	.779	.766	*	.877	1.234	*							
56	.773	.765	*	.931	1.040	*							
57	.763	.756	*	.977	.892	*							
58	.740	.737	*	1.146	.848	*							
													REFERENCE PROFIL

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***** FICHIER AD317 NO(IT)= 4
2/ 4/85 10H25 M=.756 PI=2.0 TI=155K I=+2 (RMPT) AD317
DE AD316 4'ITE

MACH DE REFERENCE= .7647 UINF= 180.428 M/S
TIV=154.7 K PIV= 1986 MB

	MACH PAROIS						*	MACH PROFIL				*	TPR	
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.769	.751	*	PRISES DOUBLES		*	1	.142	.53	.710	*	1	151.0	
2	.769	.760	*			*	2	.362	.54	.699	*	2	149.5	
3	.767	.754	*	.59	.763	.754	*	3	.482	.55	.697	*	3	148.8
4	.761	.753	*	.60	.769	.760	*	4	.593	.56	.699	*	4	149.6
5	.757	.755	*	.61	.766	.756	*	5	.691	.57	.703	*	5	149.0
6	.760	.757	*			*	6	.729	.58	.709	*	6	149.2	
7	.762	.756	*	PRISES LAT. GAUCHE*		*	7	.760	.59	.713	*	7	150.4	
8	.762	.752	*			*	8	.784	.60	.722	*	8	151.2	
9	.761	.758	*	.62	.763	.759	*	9	.807	.61	.733	*	9	152.5
10	.766	.753	*	.63	.762	.764	*	10	.943	.62	.746	*	10	151.4
11	.764	.759	*	.64	.769	.750	*	11	.872	.63	.758	*	11	151.1
12	.759	.757	*	.65	.784	.724	*	12	.911	.64	.770	*	12	151.3
13	.766	.750	*	.66	.821	.715	*	13	.994	.65	.785	*	13	151.5
14	.765	.751	*	.67	.847	.748	*	14	1.128	.66	.799	*	14	151.5
15	.765	.753	*	.68	.851	.764	*	15	1.219	.67	.818	*	15	151.2
16	.764	.750	*	.69	.838	.755	*	16	1.240	.68	.838	*	16	151.4
17	.770	.746	*	.70	.816	.743	*	17	1.264	.69	.856	*	17	149.0
18	.779	.739	*	.71	.781	.742	*	18	1.278	.70	.872	*	18	149.2
19	.773	.735	*	.72	.773	.756	*	19	1.281	.71	.887	*	19	152.7
20	.777	.732	*	.73	.764	.768	*	20	1.279	.72	.894	*		
21	.780	.726	*			*	21	1.281	.73	.893	*	I	TPG	
22	.792	.717	*	PRISES LAT. DROITES*		*	22	1.302	.74	.889	*			
23	.802	.710	*			*	23	1.293	.75	.890	*	1	154.6	
24	.809	.707	*	.74	.763	.760	*	24	1.297	.76	.870	*	2	154.9
25	.821	.713	*	.75	.766	.758	*	25	1.299	.77	.856	*	3	154.1
26	.828	.719	*	.76	.765	.756	*	26	1.301	.78	.840	*	4	153.8
27	.839	.726	*	.77	.763	.750	*	27	1.308	.79	.823	*	5	153.6
28	.844	.739	*	.78	.768	.747	*	28	1.311	.80	.807	*		
29	.848	.749	*	.79	.774	.734	*	29	1.316	.81	.792	*		
30	.849	.757	*	.80	.781	.726	*	30	1.322	.82	.778	*		
31	.955	.756	*	.81	.805	.712	*	31	1.325	.83	.763	*		
32	.854	.765	*	.82	.821	.714	*	32	1.332	.84	.750	*		
33	.858	.763	*	.83	.839	.725	*	33	1.337	.85	.735	*		
34	.848	.759	*	.84	.848	.747	*	34	1.335	.86	.729	*		
35	.943	.758	*	.85	.851	.758	*	35	1.164	.87	.710	*		
36	.841	.755	*	.86	.850	.760	*	36	1.049	.88	.688	*		
37	.836	.751	*	.87	.843	.758	*	37	1.012	.89	.663	*		
38	.831	.746	*	.88	.836	.751	*	38	.986	.90	.643	*		
39	.827	.743	*	.89	.828	.743	*	39	.963	.91	.632	*		
40	.820	.741	*	.90	.812	.741	*	40	.938	.92	.626	*		
41	.814	.738	*	.91	.795	.741	*	41	.914	.93	.610	*		
42	.813	.737	*	.92	.783	.744	*	42	.892	.94	.601	*		
43	.803	.735	*	.93	.774	.750	*	43	.871	.95	.587	*		
44	.793	.737	*	.94	.775	.754	*	44	.851	.96	.588	*		
45	.788	.738	*	.95	.769	.761	*	45	.832	.97	.587	*		
46	.784	.740	*	.96	.784	.760	*	46	.814	.98	.570	*		
47	.782	.744	*				*	47	.798	.99	.575	*		
48	.781	.746	*				*	48	.780	.100	.511	*		
49	.778	.750	*				*	49	.766	.101	.389	*		
50	.774	.752	*				*	50	.752	.102	.244	*		
51	.773	.756	*				*	51	.736	.103	.115	*		
52	.768	.758	*		PRISES COL		*	52	.725					
53	.772	.760	*											
54	.772	.762	*		.838	1.208	*							
55	.772	.761	*		.880	.876	*							
56	.767	.761	*		.934	.842	*							
57	.763	.759	*		.979	.815	*							
58	.755	.758	*		1.155	.781	*							
										REFERENCE PROFIL				

***** FICHIER AD318 NO(IT)= 4
 2/ 4/85 12H 0 M=.757 PI=1.7 TI=155K I=+2 (RM T) AD318
 DE AD317 4'ITE

MACH DE REFERENCE= .7630 UINF= 179.976 M/S
 TIV=154.5 K PIV= 1673 MB

	MACH PAROIS						*	MACH PROFIL				*	T(K)	
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.769	.752	*	PRISES DOUBLES		*	1	.163	.53	.707	*	1	150.9	
2	.769	.760	*			*	2	.360	.54	.696	*	2	149.7	
3	.767	.755	*	59	.763	.755	*	3	.482	.55	.695	*	3	148.9
4	.762	.753	*	60	.768	.759	*	4	.594	.56	.697	*	4	149.3
5	.759	.757	*	61	.766	.753	*	5	.689	.57	.702	*	5	148.9
6	.761	.759	*			*	6	.731	.58	.707	*	6	149.1	
7	.763	.757	*	PRISES LAT. GAUCHE	S	*	7	.761	.59	.713	*	7	150.2	
8	.762	.752	*			*	8	.784	.60	.721	*	8	150.6	
9	.762	.758	*	62	.763	.760	*	9	.807	.61	.733	*	9	151.7
10	.765	.752	*	63	.758	.762	*	10	.842	.62	.745	*	10	151.2
11	.763	.759	*	64	.771	.751	*	11	.873	.63	.758	*	11	150.8
12	.759	.758	*	65	.784	.725	*	12	.912	.64	.770	*	12	151.0
13	.765	.752	*	66	.820	.712	*	13	.997	.65	.784	*	13	151.3
14	.766	.754	*	67	.846	.745	*	14	1.139	.66	.802	*	14	151.4
15	.768	.755	*	68	.851	.765	*	15	1.212	.67	.820	*	15	151.2
16	.767	.752	*	69	.837	.757	*	16	1.231	.68	.837	*	16	151.5
17	.771	.747	*	70	.811	.739	*	17	1.259	.69	.855	*	17	149.3
18	.777	.738	*	71	.781	.742	*	18	1.275	.70	.871	*	18	149.6
19	.772	.734	*	72	.772	.755	*	19	1.279	.71	.884	*	19	152.7
20	.777	.733	*	73	.765	.765	*	20	1.278	.72	.892	*		
21	.781	.727	*			*	21	1.279	.73	.892	*	I	TPG	
22	.793	.716	*	PRISES LAT. DROITES	S	22	1.300	.74	.888	*				
23	.802	.707	*			*	23	1.294	.75	.879	*	1	154.5	
24	.809	.705	*	74	.764	.760	*	24	1.294	.76	.869	*	2	154.6
25	.819	.712	*	75	.766	.757	*	25	1.297	.77	.855	*	3	154.3
26	.827	.716	*	76	.764	.755	*	26	1.299	.78	.839	*	4	153.9
27	.837	.723	*	77	.763	.752	*	27	1.304	.79	.822	*	5	153.7
28	.842	.736	*	78	.770	.749	*	28	1.309	.80	.806	*		
29	.846	.745	*	79	.773	.734	*	29	1.314	.81	.791	*		
30	.847	.754	*	80	.783	.727	*	30	1.320	.82	.777	*		
31	.854	.754	*	81	.805	.710	*	31	1.324	.83	.762	*		
32	.854	.765	*	82	.819	.712	*	32	1.330	.84	.749	*		
33	.858	.766	*	83	.837	.723	*	33	1.336	.85	.734	*		
34	.849	.761	*	84	.847	.743	*	34	1.336	.86	.727	*		
35	.844	.761	*	85	.851	.755	*	35	1.151	.87	.709	*		
36	.841	.757	*	86	.850	.761	*	36	1.045	.88	.687	*		
37	.834	.752	*	87	.844	.760	*	37	1.011	.89	.661	*		
38	.829	.746	*	88	.837	.752	*	38	.985	.90	.642	*		
39	.823	.740	*	89	.825	.741	*	39	.961	.91	.632	*		
40	.816	.738	*	90	.808	.736	*	40	.936	.92	.624	*		
41	.810	.733	*	91	.792	.736	*	41	.912	.93	.607	*		
42	.808	.732	*	92	.782	.743	*	42	.889	.94	.597	*		
43	.800	.731	*	93	.773	.751	*	43	.866	.95	.585	*		
44	.791	.732	*	94	.774	.753	*	44	.845	.96	.587	*		
45	.786	.733	*	95	.769	.762	*	45	.825	.97	.586	*		
46	.783	.738	*	96	.764	.761	*	46	.808	.98	.567	*		
47	.782	.744	*			*	47	.790	.99	.573	*			
48	.780	.748	*			*	48	.775	100	.510	*			
49	.777	.752	*			*	49	.760	101	.389	*			
50	.773	.753	*			*	50	.747	102	.248	*			
51	.772	.755	*			*	51	.735	103	.126	*			
52	.768	.756	*			*	52	.721						
53	.771	.756	*											
54	.771	.758	*											
55	.771	.758	*											
56	.766	.758	*											
57	.763	.758	*											
58	.755	.760	*											

PRISES COL REFERENCE PROFIL

.836	1.180	*
.875	.868	*
.929	.934	*
.974	.811	*
1.148	.775	*

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD320 NO(IT)= 4
 2/ 4/95 16H35 M=.756 PI=2.5 TI=120 I=+2 (RMPT) AD320
 DE AD317 4'ITE

MACH DE REFERENCE= .7669 UINF= 159.342 M/S
 TIV=120.0 K PIV= 2487 MB

I	MACH PAROIS				MACH PROFIL				T(K)		
	HAUT	BAS	I	HAUT	BAS	I	EXT	I	INT	I	TPR
1	.772	.753	*	PRISES DOUBLES	*	*	1	.184	53	.719	*
2	.772	.764	*		*	2	.345	54	.704	*	2
3	.769	.758	*	59	.767	.759	*	3	.467	55	.701
4	.763	.758	*	60	.773	.762	*	4	.587	56	.704
5	.759	.760	*	61	.771	.757	*	5	.681	57	.706
6	.762	.761	*			*	6	.722	58	.712	*
7	.767	.760	*	PRISES LAT. GAUCHE	*	7	.753	59	.716	*	7
8	.767	.754	*		*	8	.777	60	.726	*	8
9	.766	.761	*	62	.764	.764	*	9	.797	61	.737
10	.770	.754	*	63	.765	.765	*	10	.846	62	.748
11	.764	.762	*	64	.771	.753	*	11	.865	63	.761
12	.758	.761	*	65	.787	.727	*	12	.900	64	.772
13	.766	.754	*	66	.825	.718	*	13	.986	65	.788
14	.768	.753	*	67	.854	.751	*	14	1.129	66	.801
15	.767	.756	*	68	.855	.769	*	15	1.210	67	.819
16	.768	.753	*	69	.838	.757	*	16	1.239	68	.838
17	.772	.749	*	70	.817	.743	*	17	1.259	69	.856
18	.780	.741	*	71	.782	.744	*	18	1.274	70	.872
19	.772	.738	*	72	.775	.758	*	19	1.279	71	.886
20	.780	.737	*	73	.765	.772	*	20	1.279	72	.894
21	.782	.731	*			*	21	1.279	73	.893	*
22	.796	.719	*	PRISES LAT. DROITES	*	22	1.296	74	.891	*	I
23	.805	.711	*		*	23	1.292	75	.882	*	1
24	.811	.709	*	74	.764	.764	*	24	1.296	76	.871
25	.824	.715	*	75	.770	.761	*	25	1.299	77	.858
26	.832	.721	*	76	.768	.758	*	26	1.300	78	.842
27	.844	.728	*	77	.762	.753	*	27	1.306	79	.824
28	.849	.741	*	78	.770	.750	*	28	1.310	80	.808
29	.855	.751	*	79	.773	.737	*	29	1.315	81	.793
30	.855	.759	*	80	.782	.730	*	30	1.321	82	.779
31	.861	.759	*	81	.808	.712	*	31	1.324	83	.764
32	.859	.768	*	82	.824	.715	*	32	1.332	84	.750
33	.861	.767	*	83	.844	.729	*	33	1.335	85	.739
34	.849	.763	*	84	.854	.751	*	34	1.290	86	.726
35	.843	.761	*	85	.857	.762	*	35	1.163	87	.707
36	.840	.757	*	86	.854	.764	*	36	1.049	88	.685
37	.835	.752	*	87	.843	.762	*	37	1.000	89	.662
38	.831	.748	*	88	.836	.754	*	38	.979	90	.641
39	.827	.744	*	89	.829	.745	*	39	.952	91	.635
40	.820	.743	*	90	.813	.741	*	40	.930	92	.630
41	.815	.738	*	91	.795	.741	*	41	.909	93	.612
42	.814	.737	*	92	.784	.747	*	42	.887	94	.602
43	.805	.736	*	93	.774	.753	*	43	.867	95	.589
44	.795	.737	*	94	.777	.756	*	44	.849	96	.589
45	.789	.738	*	95	.774	.762	*	45	.832	97	.593
46	.785	.742	*	96	.763	.760	*	46	.816	98	.571
47	.784	.748	*			*	47	.798	99	.580	*
48	.782	.751	*			*	48	.793	100	.517	*
49	.778	.754	*			*	49	.771	101	.391	*
50	.775	.754	*			*	50	.758	102	.242	*
51	.776	.758	*			*	51	.743	103	.111	*
52	.774	.762	*	PRISES COL	*	52	.732				
53	.778	.764	*								REFERENCE PROFIL
54	.777	.767	*		.833	1.194	*				.759
55	.777	.766	*		.861	.867	*				.762
56	.770	.765	*		.818	.833	*				.760
57	.765	.760	*		.973	.810	*				.758
58	.756	.757	*		1.150	.778	*				

***** FICHIER AD321 NO(IT)= 4
 3/ 4/85 11H60 M=.760 PI=1.7 TI=TA I=+.25 (RM) AD321
 DE AD297 4' ITE

MACH DE REFERENCE= .7619 UINF= 247.486 M/S
 TIV=292.9 K PIV= 1779 MB

MACH PAROIS						*	MACH PROFIL				*	I	T(K)	
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.764	.754	*	PRISES DOUBLES		*	1	.058	53	.699	*	1	289.3	
2	.764	.759	*			*	2	.200	54	.695	*	2	287.9	
3	.764	.756	*	59	.759	.755	*	3	.319	55	.696	*	3	287.8
4	.762	.756	*	60	.766	.758	*	4	.426	56	.701	*	4	287.9
5	.761	.759	*	61	.765	.753	*	5	.518	57	.707	*	5	288.0
6	.760	.759	*				*	6	.574	58	.714	*	6	288.0
7	.759	.756	*	PRISES LAT. GAUCHES*		*	7	.614	59	.721	*	7	288.3	
8	.760	.754	*			*	8	.647	60	.732	*	8	289.0	
9	.761	.759	*	62	.763	.760	*	9	.679	61	.743	*	9	290.1
10	.763	.753	*	63	.760	.760	*	10	.717	62	.757	*	10	289.7
11	.762	.757	*	64	.763	.752	*	11	.752	63	.771	*	11	289.2
12	.759	.757	*	65	.773	.733	*	12	.795	64	.795	*	12	289.0
13	.763	.753	*	66	.793	.736	*	13	.893	65	.801	*	13	289.3
14	.760	.753	*	67	.818	.772	*	14	1.006	66	.818	*	14	289.3
15	.761	.754	*	68	.814	.782	*	15	1.052	67	.840	*	15	290.0
16	.761	.753	*	69	.804	.768	*	16	1.103	68	.860	*	16	289.3
17	.764	.750	*	70	.796	.744	*	17	1.130	69	.883	*	17	288.5
18	.768	.745	*	71	.769	.742	*	18	1.142	70	.905	*	18	288.9
19	.765	.743	*	72	.767	.755	*	19	1.149	71	.924	*	19	289.2
20	.769	.739	*	73	.765	.763	*	20	1.150	72	.938	*		
21	.773	.735	*				*	21	1.150	73	.943	*	I	TPG
22	.779	.731	*	PRISES LAT. DROITES*		*	22	1.158	74	.944	*			
23	.786	.727	*			*	23	1.156	75	.938	*	1	293.0	
24	.789	.729	*	74	.762	.759	*	24	1.154	76	.929	*	2	293.1
25	.794	.738	*	75	.761	.757	*	25	1.149	77	.914	*	3	293.0
26	.800	.744	*	76	.761	.755	*	26	1.145	78	.899	*	4	293.0
27	.809	.753	*	77	.760	.752	*	27	1.141	79	.881	*	5	293.0
28	.814	.766	*	78	.762	.751	*	28	1.123	80	.865	*		
29	.818	.776	*	79	.766	.741	*	29	1.029	81	.851	*		
30	.817	.782	*	80	.774	.735	*	30	1.006	82	.839	*		
31	.818	.781	*	81	.786	.728	*	31	1.016	83	.827	*		
32	.816	.789	*	82	.791	.736	*	32	1.035	84	.814	*		
33	.816	.787	*	83	.806	.752	*	33	1.050	85	.803	*		
34	.808	.780	*	84	.818	.770	*	34	1.062	86	.796	*		
35	.806	.778	*	85	.817	.781	*	35	1.071	87	.783	*		
36	.805	.773	*	86	.812	.782	*	36	1.071	88	.767	*		
37	.803	.766	*	87	.806	.778	*	37	1.041	89	.750	*		
38	.803	.759	*	88	.804	.767	*	38	1.023	90	.738	*		
39	.804	.752	*	89	.803	.753	*	39	.998	91	.733	*		
40	.800	.749	*	90	.795	.745	*	40	.969	92	.725	*		
41	.797	.744	*	91	.780	.742	*	41	.939	93	.716	*		
42	.796	.742	*	92	.772	.744	*	42	.909	94	.714	*		
43	.789	.740	*	93	.765	.751	*	43	.878	95	.708	*		
44	.781	.740	*	94	.768	.754	*	44	.846	96	.714	*		
45	.776	.739	*	95	.765	.758	*	45	.817	97	.713	*		
46	.773	.740	*	96	.766	.758	*	46	.790	98	.753	*		
47	.771	.744	*				*	47	.767	99	.802	*		
48	.769	.747	*				*	48	.749	100	.743	*		
49	.768	.751	*				*	49	.735	101	.594	*		
50	.766	.755	*				*	50	.724	102	.433	*		
51	.767	.755	*				*	51	.715	103	.298	*		
52	.766	.754	*	PRISES COL		*	52	.707						
53	.769	.756	*											
54	.767	.758	*		.832	.953	*							
55	.767	.758	*		.872	.849	*							
56	.765	.759	*		.924	.818	*							
57	.763	.756	*		.970	.739	*							
58	.760	.752	*		1.135	.759	*							

REFERENCE PROFIL

***** FICHIER AD322 NO(IT)= 4
3/ 4/85 13H50 M=.77 PI=1.7 TI=TA I=+.25 (RM) AD322
DE AD321 4'ITE

MACH DE REFERENCE= .7729 UINR= 251.372 M/S
TIV=294.6 K PIY= 1716 MB

***** FICHIER AD323 NO(IT)= 4
3/ 4/85 14H10 M=.78 PI=1.7 TI=TA I=+.25 (RM) AD323
DE AD322 4'ITE

MACH DE REFERENCE=.7843 UINR= 255.169 M/S
TIV=295.7 K PIV= 1731 MB

***** FICHIER AD324 NO(IT)= 4
3/4/85 14H30 M=.785 PI=1.7 TI=TA I=+.25 (RM) AD324
DE AD323 4'ITE

MACH DE REFERENCE= .7904 UINF= 257.186 M/S
TIV=296.3 K PIV= 1741 MB

***** FICHIER AD325 NO(IT)= 4
3/4/85 14H50 M=.738 PI=1.7 TI=TA I=+.25 (RM) AD325
DE AD321 4'ITE

MACH DE REFERENCE= .7416 UINF= 243.107 M/S
TIV=296.7 K PIV= 1662 MB

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OF POOR QUALITY

***** FICHIER AD326 NO(IT)= 4
3/ 4/85 15H 5 M=.716 PI=1.7 TI=TA I=+.25 (RM) AD326
DE AD325 4'ITE

MACH DE REFERENCE= .7183 UINF= 236.281 M/S
TIY=296.9 K PIV= 1629 MB

***** FICHIER AD327 NO(IT)= 4
3/ 4/85 16H10 M=.756 PI=2.5 TI=TA I=+.25 (RMP) AD327
DE AD321 4'ITE

MACH DE REFERENCE= .7625 UINFL= 249.950 M/S
TIV=298.4 K PIV= 2495 MB

ORIGINAL PAGE IS
OF POOR QUALITY

***** FICHIER AD328 NO(IT)= 4
4/4/95 9H30 M=.698 PI=1.7 TI=TA I=+.25 (RM) AD328
DE AD326 4'ITE

MACH DE REFERENCE= .7003 UINF= 229.601 M/S
TIV=293.6 K PIV= 1596 MB

MACH PAROIS						MACH PROFIL						T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.702	.692	*	PRISES DOUBLES	*	*	1	.044	53	.641	*	1	291.1	
2	.700	.696	*			*	2	.223	54	.639	*	2	290.1	
3	.700	.695	*	59	.699	.694	*	3	.335	55	.640	*	3	290.6
4	.701	.698	*	60	.705	.698	*	4	.441	56	.645	*	4	290.6
5	.699	.700	*	61	.702	.693	*	5	.527	57	.649	*	5	290.5
6	.699	.698	*			*	6	.579	58	.656	*	6	290.6	
7	.699	.695	*	PRISES LAT. GAUCHE	*	*	7	.615	59	.663	*	7	290.7	
8	.702	.695	*			*	8	.645	60	.673	*	8	291.1	
9	.704	.700	*	62	.699	.699	*	9	.674	61	.682	*	9	292.0
10	.702	.692	*	63	.701	.699	*	10	.707	62	.694	*	10	291.6
11	.700	.697	*	64	.704	.693	*	11	.741	63	.705	*	11	291.3
12	.697	.698	*	65	.710	.677	*	12	.779	64	.717	*	12	291.1
13	.700	.695	*	66	.723	.679	*	13	.870	65	.730	*	13	291.4
14	.698	.694	*	67	.738	.704	*	14	.960	66	.745	*	14	291.7
15	.699	.694	*	68	.735	.712	*	15	.993	67	.761	*	15	292.1
16	.701	.693	*	69	.731	.702	*	16	1.017	68	.778	*	16	292.1
17	.705	.692	*	70	.726	.684	*	17	1.015	69	.793	*	17	291.6
18	.710	.688	*	71	.709	.685	*	18	1.003	70	.808	*	18	292.0
19	.706	.686	*	72	.702	.692	*	19	.982	71	.820	*	19	292.0
20	.708	.683	*	73	.702	.699	*	20	.964	72	.829	*		
21	.710	.679	*			*	21	.959	73	.832	*	I	TPG	
22	.716	.675	*	PRISES LAT. DROITES	*	22	.957	74	.832	*				
23	.720	.671	*			*	23	.946	75	.828	*	1	293.6	
24	.728	.673	*	74	.700	.698	*	24	.942	76	.822	*	2	293.7
25	.724	.680	*	75	.700	.695	*	25	.935	77	.813	*	3	293.6
26	.727	.685	*	76	.701	.695	*	26	.931	78	.802	*	4	293.5
27	.732	.691	*	77	.698	.693	*	27	.929	79	.791	*	5	293.6
28	.736	.700	*	78	.703	.692	*	28	.928	80	.779	*		
29	.739	.707	*	79	.706	.683	*	29	.928	81	.769	*		
30	.738	.711	*	80	.710	.679	*	30	.927	82	.759	*		
31	.740	.710	*	81	.720	.672	*	31	.926	83	.749	*		
32	.737	.715	*	82	.722	.679	*	32	.927	84	.740	*		
33	.748	.715	*	83	.731	.690	*	33	.926	85	.733	*		
34	.734	.712	*	84	.739	.704	*	34	.926	86	.724	*		
35	.732	.710	*	85	.738	.711	*	35	.926	87	.713	*		
36	.732	.707	*	86	.736	.713	*	36	.926	88	.699	*		
37	.731	.701	*	87	.731	.709	*	37	.922	89	.685	*		
38	.731	.695	*	88	.731	.701	*	38	.915	90	.673	*		
39	.732	.690	*	89	.730	.689	*	39	.903	91	.671	*		
40	.729	.686	*	90	.725	.684	*	40	.889	92	.663	*		
41	.728	.684	*	91	.714	.685	*	41	.868	93	.655	*		
42	.726	.682	*	92	.710	.687	*	42	.844	94	.650	*		
43	.720	.682	*	93	.704	.691	*	43	.820	95	.645	*		
44	.715	.683	*	94	.703	.692	*	44	.792	96	.648	*		
45	.712	.683	*	95	.701	.699	*	45	.765	97	.645	*		
46	.710	.684	*	96	.701	.693	*	46	.739	98	.672	*		
47	.711	.687	*			*	47	.715	99	.709	*			
48	.709	.689	*			*	48	.694	100	.655	*			
49	.707	.691	*			*	49	.677	101	.527	*			
50	.704	.693	*			*	50	.665	102	.379	*			
51	.703	.693	*			*	51	.654	103	.253	*			
52	.703	.694	*	PRISES COL	*	52	.645							
53	.704	.694	*											
54	.702	.695	*		.768	1.160	*							
55	.702	.695	*		.815	.960	*							
56	.701	.696	*		.880	.853	*							
57	.700	.697	*		.936	.790	*							
58	.700	.699	*		1.109	.742	*							
								REFERENCE PROFIL						

***** FICHIER AD331 NO(IT)= 4
 5/4/85 9H25 M=.728 PI=1.7 TI=TA I=+0.25 (RM) AD 331
 DE AD326 4'ITE

MACH DE REFERENCE= .7288 UINF= 237.893 M/S
 TIY=293.2 K PIV= 1614 MB

MACH PAROIS						MACH PROFIL						T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.731	.722	*	PRISES DOUBLES	*	*	1	.040	.53	.668	*	1	289.3	
2	.730	.726	*			*	2	.213	.54	.564	*	2	288.2	
3	.730	.722	*	.59	.727	.722	*	3	.325	.55	.666	*	3	288.6
4	.729	.723	*	.60	.732	.727	*	4	.435	.56	.671	*	4	288.6
5	.728	.726	*	.61	.731	.722	*	5	.524	.57	.676	*	5	288.6
6	.727	.725	*			*	6	.578	.58	.682	*	6	288.6	
7	.727	.725	*	PRISES LAT. GAUCHE*	*	*	7	.616	.59	.690	*	7	288.7	
8	.729	.725	*			*	8	.648	.60	.699	*	8	289.3	
9	.729	.730	*	.62	.729	.725	*	9	.679	.61	.710	*	9	290.3
10	.729	.722	*	.63	.727	.729	*	10	.713	.62	.723	*	10	290.0
11	.729	.725	*	.64	.732	.721	*	11	.749	.63	.735	*	11	289.6
12	.726	.724	*	.65	.738	.704	*	12	.799	.64	.748	*	12	289.4
13	.730	.720	*	.66	.757	.707	*	13	.885	.65	.762	*	13	289.7
14	.728	.721	*	.67	.770	.734	*	14	.989	.66	.779	*	14	289.9
15	.730	.722	*	.68	.771	.742	*	15	1.030	.67	.797	*	15	290.0
16	.731	.721	*	.69	.767	.732	*	16	1.073	.68	.815	*	16	289.2
17	.733	.719	*	.70	.754	.713	*	17	1.084	.69	.834	*	17	289.1
18	.737	.715	*	.71	.738	.713	*	18	1.087	.70	.851	*	18	289.3
19	.732	.712	*	.72	.731	.720	*	19	1.078	.71	.866	*	19	289.5
20	.735	.710	*	.73	.731	.731	*	20	1.017	.72	.876	*		
21	.738	.706	*			*	21	1.016	.73	.880	*	I	TPG	
22	.745	.701	*	PRISES LAT. DROITES*	*	*	22	1.018	.74	.881	*			
23	.750	.697	*			*	23	1.006	.75	.875	*	1	293.1	
24	.753	.701	*	.74	.729	.725	*	24	1.000	.76	.863	*	2	293.1
25	.757	.709	*	.75	.729	.724	*	25	.992	.77	.858	*	3	293.1
26	.760	.714	*	.76	.727	.723	*	26	.987	.78	.845	*	4	293.0
27	.764	.720	*	.77	.727	.719	*	27	.986	.79	.833	*	5	293.0
28	.768	.730	*	.78	.731	.720	*	28	.985	.80	.818	*		
29	.769	.737	*	.79	.733	.710	*	29	.985	.81	.807	*		
30	.769	.742	*	.80	.739	.705	*	30	.984	.82	.796	*		
31	.772	.741	*	.81	.752	.699	*	31	.982	.83	.786	*		
32	.772	.747	*	.82	.756	.708	*	32	.984	.84	.775	*		
33	.775	.746	*	.83	.764	.720	*	33	.983	.85	.767	*		
34	.779	.741	*	.84	.770	.734	*	34	.982	.86	.757	*		
35	.769	.739	*	.85	.771	.742	*	35	.983	.87	.747	*		
36	.769	.736	*	.86	.770	.743	*	36	.982	.88	.732	*		
37	.766	.730	*	.87	.769	.739	*	37	.976	.89	.716	*		
38	.764	.725	*	.88	.767	.730	*	38	.966	.90	.705	*		
39	.762	.720	*	.89	.761	.720	*	39	.949	.91	.700	*		
40	.758	.717	*	.90	.754	.714	*	40	.928	.92	.691	*		
41	.755	.714	*	.91	.745	.709	*	41	.902	.93	.683	*		
42	.755	.711	*	.92	.740	.714	*	42	.876	.94	.679	*		
43	.750	.708	*	.93	.732	.718	*	43	.848	.95	.675	*		
44	.745	.707	*	.94	.734	.720	*	44	.818	.96	.676	*		
45	.741	.707	*	.95	.732	.728	*	45	.789	.97	.676	*		
46	.740	.709	*	.96	.730	.728	*	46	.761	.98	.708	*		
47	.739	.715	*			*	47	.738	.99	.751	*			
48	.738	.713	*			*	48	.719	100	.693	*			
49	.738	.719	*			*	49	.703	101	.557	*			
50	.732	.720	*			*	50	.691	102	.403	*			
51	.732	.721	*			*	51	.682	103	.272	*			
52	.732	.722	*			PRISES COL	*	52	.691					
53	.733	.724	*											
54	.732	.725	*		.792	1.179	*				REFERENCE PROFIL			
55	.732	.726	*		.836	.905	*				.728			
56	.731	.727	*		.898	.840	*				.728			
57	.729	.726	*		.949	.794	*				.727			
58	.726	.727	*		1.121	.755	*				.727			

***** FICHIER AD332 NO(IT)= 4
5/4/95 10H35 M=.763 PI=3.0 TI=120K I=+0.25 (RMPT) AD 332
DE AD330 4'ITE

MACH DE REFERENCE= .7661 UINF= 159.591 M/S
TIV=120.6 K PIV= 2984 MB

***** FICHIER AD333 NO(IT)= 4
5/4/85 11H60 M=.775 PI=3.0 TI=120K I=+0.25 (RMPT) AD 333
DE AD332 4'ITE

MACH DE REFERENCE= .7774 UINF= 161.465 M/S
TIV=120.3 K PIY= 2987 MB

***** FICHIER AD334 NO(IT)= 4
 9/4/85 10H45 M=.75 PI=1.7 TI=TA I=+0.25 (RM) AD 334
 DE AD325 4'ITE

MACH DE REFERENCE= .7496 UINF= 244.380 M/S
 TIV=294.1 K PIV= 1647 MB

MACH PAROIS						*	MACH PROFIL				*	T(K)		
I	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT	*	I	TPR	
1	.753	.744	*	PRISES DOUBLES		*	1	.041	.53	.692	*	1	290.6	
2	.752	.748	*			*	2	.202	.54	.688	*	2	289.2	
3	.752	.745	*	59	.748	.744	*	.317	.55	.689	*	3	289.5	
4	.751	.746	*	60	.754	.747	*	.427	.56	.693	*	4	289.6	
5	.750	.748	*	61	.753	.742	*	.517	.57	.700	*	5	289.5	
6	.749	.748	*			*	6	.574	.58	.706	*	6	289.6	
7	.748	.745	*	PRISES LAT. GAUCHE	S	*	7	.612	.59	.713	*	7	289.3	
8	.750	.744	*			*	8	.645	.60	.723	*	8	290.5	
9	.750	.749	*	62	.751	.749	*	.678	.61	.733	*	9	291.4	
10	.750	.742	*	63	.747	.749	*	10	.714	.62	.746	*	10	291.1
11	.750	.746	*	64	.754	.742	*	11	.751	.63	.760	*	11	290.6
12	.747	.747	*	65	.761	.727	*	12	.792	.64	.773	*	12	290.4
13	.751	.743	*	66	.782	.725	*	13	.891	.65	.789	*	13	290.7
14	.749	.744	*	67	.801	.759	*	14	.999	.66	.804	*	14	291.1
15	.751	.745	*	68	.798	.768	*	15	1.045	.67	.825	*	15	291.3
16	.752	.744	*	69	.791	.756	*	16	1.093	.68	.844	*	16	290.9
17	.755	.740	*	70	.780	.733	*	17	1.116	.69	.865	*	17	290.5
18	.758	.733	*	71	.758	.735	*	18	1.127	.70	.885	*	18	290.8
19	.754	.731	*	72	.754	.741	*	19	1.130	.71	.902	*	19	290.9
20	.758	.733	*	73	.753	.752	*	20	1.130	.72	.914	*	I	TPG
21	.760	.729	*			*	21	1.127	.73	.919	*			
22	.765	.721	*	PRISES LAT. DROITES	S	*	22	1.132	.74	.920	*			
23	.771	.715	*			*	23	1.117	.75	.914	*	1	294.1	
24	.776	.718	*	74	.751	.747	*	24	1.071	.76	.906	*	2	294.1
25	.781	.722	*	75	.749	.746	*	25	1.006	.77	.893	*	3	294.1
26	.786	.733	*	76	.749	.744	*	26	1.011	.78	.880	*	4	294.1
27	.793	.741	*	77	.749	.742	*	27	1.019	.79	.864	*	5	294.1
28	.798	.753	*	78	.753	.741	*	28	1.025	.80	.848	*		
29	.800	.762	*	79	.755	.729	*	29	1.030	.81	.836	*		
30	.800	.767	*	80	.762	.728	*	30	1.033	.82	.824	*		
31	.801	.766	*	81	.772	.717	*	31	1.034	.83	.812	*		
32	.799	.773	*	82	.780	.726	*	32	1.036	.84	.801	*		
33	.800	.772	*	83	.792	.741	*	33	1.034	.85	.792	*		
34	.794	.766	*	84	.802	.758	*	34	1.034	.86	.783	*		
35	.792	.764	*	85	.801	.767	*	35	1.033	.87	.771	*		
36	.791	.760	*	86	.797	.769	*	36	1.031	.88	.756	*		
37	.789	.753	*	87	.792	.764	*	37	1.020	.89	.740	*		
38	.798	.747	*	88	.790	.754	*	38	1.004	.90	.728	*		
39	.788	.740	*	89	.787	.741	*	39	.982	.91	.724	*		
40	.783	.736	*	90	.780	.734	*	40	.955	.92	.713	*		
41	.781	.732	*	91	.770	.731	*	41	.926	.93	.705	*		
42	.780	.730	*	92	.760	.736	*	42	.897	.94	.701	*		
43	.774	.728	*	93	.755	.740	*	43	.867	.95	.698	*		
44	.767	.727	*	94	.757	.741	*	44	.836	.96	.701	*		
45	.763	.727	*	95	.753	.746	*	45	.807	.97	.701	*		
46	.761	.731	*	96	.754	.746	*	46	.780	.98	.737	*		
47	.759	.737	*			*	47	.757	.99	.785	*			
48	.759	.739	*			*	48	.739	.100	.725	*			
49	.757	.740	*			*	49	.725	.101	.592	*			
50	.755	.741	*			*	50	.714	.102	.422	*			
51	.755	.741	*			*	51	.707	.103	.290	*			
52	.754	.743	*	PRISES COL		*	52	.699						
53	.755	.746	*											
54	.754	.747	*											
55	.754	.748	*											
56	.753	.748	*											
57	.752	.745	*											
58	.749	.739	*											

REFERENCE PROFIL

.749

.749

.750

.749

***** FICHIER RD335 NO(IT)= 4
9/4/85 15H50 M=.786 PI=3.0 TI=120K I=+0.25 (RMPT) RD 335
DE RD333 4'ITE

MACH DE REFERENCE= .7396 UINF= 163.556 M/S
TIY=120.0 K PIV= 2989 MB

***** FICHIER AD336 NO(IT)= 4
 9/ 4/85 17H 5 M=.725 PI=3.0 TI=120K I=+0.25 (RMPT) AD 336
 DE RD330 4'ITE

MACH DE REFERENCE= .7291 UINF= 152.193 M/S
 TIY=119.9 K PIV= 2982 MB

I	MACH PAROIS			MACH PROFIL			T(K)			*	I	TPR		
	HAUT	BAS	I	HAUT	BAS	*	I	EXT	I	INT				
1	.731	.722	*	PRISES DOUBLES			*	1	.371	53	.655	*	1	116.8
2	.728	.727	*	*	*	*	2	.228	54	.654	*	2	115.6	
3	.729	.722	*	59	.723	.718	*	3	.342	55	.657	*	3	115.7
4	.731	.726	*	60	.732	.727	*	4	.457	56	.663	*	4	117.0
5	.728	.728	*	61	.731	.722	*	5	.546	57	.669	*	5	116.9
6	.725	.724	*	*	*	*	6	.593	58	.676	*	6	116.8	
7	.724	.720	*	PRISES LAT. GAUCHES*			7	.631	59	.685	*	7	116.8	
8	.727	.721	*	*	*	*	8	.663	60	.694	*	8	118.0	
9	.730	.732	*	62	.728	.730	*	9	.691	61	.705	*	9	119.6
10	.729	.721	*	63	.729	.730	*	10	.720	62	.717	*	10	117.6
11	.727	.729	*	64	.732	.723	*	11	.764	63	.730	*	11	117.2
12	.725	.731	*	65	.744	.704	*	12	.797	64	.742	*	12	117.3
13	.732	.722	*	66	.764	.705	*	13	.891	65	.757	*	13	117.2
14	.731	.719	*	67	.777	.742	*	14	1.013	66	.763	*	14	116.9
15	.729	.721	*	68	.777	.729	*	15	1.045	67	.780	*	15	116.5
16	.731	.722	*	69	.772	.729	*	16	1.089	68	.799	*	16	117.7
17	.733	.719	*	70	.761	.708	*	17	1.105	69	.816	*	17	115.8
18	.739	.712	*	71	.740	.712	*	18	1.108	70	.832	*	18	115.8
19	.732	.711	*	72	.731	.719	*	19	1.107	71	.847	*	19	117.7
20	.740	.710	*	73	.735	.730	*	20	1.091	72	.856	*	I	TPG
21	.737	.707	*	PRISES LAT. DROITES*			21	1.009	73	.858	*			
22	.748	.701	*	PRISES LAT. DROITES*			22	1.021	74	.859	*			
23	.752	.696	*	*	*	*	23	1.012	75	.854	*	1	119.1	
24	.754	.696	*	74	.728	.728	*	24	1.006	76	.847	*	2	119.4
25	.762	.703	*	75	.727	.722	*	25	1.000	77	.838	*	3	119.5
26	.764	.707	*	76	.728	.724	*	26	.994	78	.826	*	4	118.6
27	.769	.712	*	77	.727	.720	*	27	.993	79	.813	*	5	119.7
28	.772	.722	*	78	.730	.720	*	28	.992	80	.800	*		
29	.775	.729	*	79	.731	.711	*	29	.993	81	.789	*		
30	.774	.735	*	80	.739	.706	*	30	.993	82	.778	*		
31	.778	.735	*	81	.753	.697	*	31	.992	83	.763	*		
32	.777	.743	*	82	.762	.702	*	32	.994	84	.757	*		
33	.781	.742	*	83	.770	.712	*	33	.994	85	.746	*		
34	.773	.737	*	84	.776	.729	*	34	.993	86	.741	*		
35	.771	.736	*	85	.777	.738	*	35	.994	87	.727	*		
36	.771	.732	*	86	.776	.740	*	36	.995	88	.713	*		
37	.769	.726	*	87	.772	.739	*	37	.991	89	.694	*		
38	.769	.718	*	88	.769	.728	*	38	.981	90	.680	*		
39	.768	.712	*	89	.768	.714	*	39	.965	91	.684	*		
40	.762	.711	*	90	.760	.709	*	40	.948	92	.673	*		
41	.760	.705	*	91	.745	.712	*	41	.923	93	.659	*		
42	.759	.705	*	92	.741	.713	*	42	.896	94	.656	*		
43	.752	.705	*	93	.733	.718	*	43	.869	95	.652	*		
44	.746	.708	*	94	.733	.718	*	44	.840	96	.656	*		
45	.741	.709	*	95	.732	.732	*	45	.811	97	.663	*		
46	.739	.711	*	96	.731	.731	*	46	.781	98	.674	*		
47	.741	.715	*	*	*	*	*	47	.754	99	.723	*		
48	.741	.715	*	*	*	*	*	48	.728	100	.666	*		
49	.737	.719	*	*	*	*	*	49	.706	101	.530	*		
50	.734	.721	*	*	*	*	*	50	.687	102	.372	*		
51	.732	.720	*	*	*	*	*	51	.670	103	.238	*		
52	.733	.726	*	PRISES COL			*	52	.657					
53	.735	.724	*											
54	.733	.725	*											
55	.736	.728	*											
56	.734	.731	*											
57	.733	.729	*											
58	.733	.733	*											

REFERENCE PROFIL